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**Low Speed Wind Tunnel Tests on a  
Series of Rectangular Wings of Varying  
Aspect Ratio and Aerofoil Section**

*by*

*G. G. Brebner, L. A. Wyatt and Gladys P. Hott*

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LOW SPEED WIND TUNNEL TESTS ON A SERIES OF RECTANGULAR WINGS OF  
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G. G. Brebner

L. A. Wyatt

Gladys P. Ilott

SUMMARY

To provide experimental evidence on the loading and pressure distribution of low aspect ratio wings and on the variation of aerofoil section characteristics with aspect ratio, wind tunnel tests were done on a series of rectangular wings with aspect ratios varying from 4.0 to 0.5 and three different aerofoil sections. Two of the sections were cambered and all had the RAE 101 thickness distribution,  $t/c = 0.10$ . The tests comprised balance measurements of lift, drag and pitching moment, pressure measurements at the centre section (which have been integrated to obtain local forces and moments) and boundary layer transition observations.

A limited analysis has been done of the local and total forces and moments, comparisons being made with the methods of Küchemann and Weber for calculating load and pressure distribution. The experimental pressure distributions offer scope for considerably more analysis.



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## 1 INTRODUCTION

This report presents the results of a series of wind tunnel tests on rectangular wings with different aspect ratios and aerofoil sections. The purpose of the tests was to provide experimental evidence about some aspects of wing loading calculation methods, particularly about the effect of reducing the aspect ratio on the characteristics of symmetrical and cambered profiles. One aim was to study the effect of aspect ratio on the pressure distribution associated with the wing thickness distribution. Therefore an uncambered aerofoil section was chosen (RAE 101, thickness/chord ratio = 0.10) for which detailed experimental results in two dimensions were available<sup>6</sup>.

Again, there are theoretical indications<sup>4</sup> that the loading on cambered wings behaves differently from that on uncambered wings as the aspect ratio is reduced, and another aim of these tests was to provide an experimental basis for further theoretical work.

Rectangular wings were chosen in order to avoid complicating the analysis with taper and sweep effects, but any conclusions drawn about sectional\* aerofoil characteristics or spanwise load distribution would be relevant to wings of more general planform.

The experimental results are presented in tabular form to facilitate subsequent analysis. Most of the tests were done at two Reynolds Numbers,  $1.6 \times 10^6$  and  $3.2 \times 10^6$ . To keep the number of tables as small as possible, pressure plotting results are included at the higher Reynolds Number only, except in those cases where only the lower Reynolds Number was tested. However, for anyone who wishes to study or analyse them, the results at  $R = 1.6 \times 10^6$  are available from the authors.

Only a small amount of comparison between theory and experiment is included, and the conclusions are of a tentative nature. The theoretical methods used were those of Küchemann<sup>1</sup> and Weber<sup>2,3,4</sup> for calculating the loading and pressure distribution on wings of moderate and small aspect ratio, and that of Brebner<sup>5</sup> for cambered wings. Since this work was done the increased availability of electronic computers has reduced the interest in developing accurate methods simple enough for desk computation. Nevertheless it is hoped that this limited analysis will be relevant to the continuing search for physically meaningful mathematical models.

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\* "Sectional" properties (e.g. sectional lift slope,  $\partial C_L / \partial \alpha_0$ ) are associated with bound vorticity only and not with trailing vorticity. This does not mean they are independent of aspect ratio, since the distribution of bound vorticity changes with aspect ratio.

The wings with symmetrical profiles are discussed separately from those with cambered profiles. In Section 2 all the models and tests are described and the results and analysis of the symmetrical section wings are given in Section 3. Some cambered wing results are briefly analysed in Section 4.

## 2 DESCRIPTION OF MODELS AND TESTS

Three different streamwise profiles were included in the set of wings tested, the thickness distribution of each being RAE 101, thickness/chord ratio = 0.10. The mean lines were a straight line and two camber lines of the family derived in Ref.5, those designated by  $m = 0.5$  and  $m = 0.8$ , where  $m$  is a parameter related to the chordwise position of the maximum ordinate. The wings with symmetrical profile are designated by the letter A, those with the  $m = 0.5$  and  $0.8$  camber lines by the letters B and C respectively. Section B had 2% camber and section C had 1% camber.

Each series of finite wings comprised five different aspect ratios, 4.0, 2.5, 1.4, 1.0 and 0.5. There were three series of balance models (one each of Sections A, B and C) on which lift, drag and pitching moment were measured; and two series of pressure-plotting models (one each of Sections A and B), on which the pressure distribution on the centre line was measured. The balance models were denoted by the letter F and the pressure-plotting models by the letter P. The aspect ratios were numbered in sequence from 1 ( $A = 4.0$ ) to 5 ( $A = 0.5$ ). This facilitates concise reference to any wing, e.g. BP/3. In addition results for a two-dimensional wing with Section A are available in Ref.6, and wing BP/1 was fitted with faired extensions and measured as a two-dimensional wing spanning the tunnel vertically. These wings are designated AP/0 and BP/0. The complete series of wings is set out in Table 1.

All the models were made of laminated teak and, except for BP/0, were suspended on wires, the balance models from an overhead balance, the pressure models from the tunnel roof. The largest aspect ratio of each series was progressively cut down to the other four aspect ratios. A sketch of the planforms is given in Fig.1, showing the suspension points. On the three smallest aspect ratios the main suspension points were at the ends of steel bars running through the wings at their maximum thickness positions. The wings had rounded tips. The area used in calculating the force and moment coefficients is that of the rectangle defined by span  $\times$  centre line chord. The pressure models had 29 flush holes at the centre section, equally distributed on both surfaces. The chordwise positions of the holes are given in Fig.1. The pressure tubes ( $1/32$ " inside diameter at the surface) were taken out of the wing at two positions, 4 inches on either side of the centre line, towards the rear of the wing. This was to simplify the work of cutting

down the wings to the next smaller aspect ratio. Each group of tubes was arranged in a flat sheet parallel to the stream direction to minimise their effect on the flow. On the cambered wings of the BP series the tubes were led out of the "flatter" surface which is conventionally regarded as the lower surface of a cambered wing. This served to define the "lower surface" on the AP series as the surface from which the pressure tubes emerged.

Each model, both balance and pressure plotting, was tested in two attitudes, called "normal attitude" and "inverted attitude". (Exceptions are noted in Table 1.) In the normal attitude the "upper surface" was lowermost in the tunnel, as is normal with models suspended on a wire rig. In the inverted attitude the "upper surface" was uppermost in the tunnel. The reason for doing both cases was to eliminate any pitch angle in the tunnel flow by comparing the two sets of results. In the case of the symmetrical wings it was also possible to eliminate any error due to model asymmetry or inaccurate positioning of the incidence datum line. This was not possible for the cambered wings since the zero lift angle was not known beforehand. These corrections to the incidence are shown diagrammatically in Fig.2. The incidence sign convention is such that, in the normal attitude in the tunnel, positive incidence is nose down and in the inverted attitude positive incidence is nose up. With some balance models the incidences tested in the normal and inverted attitudes were the same, or nearly so, and mean values of the forces and moments in the two attitudes are quoted for those incidences. With the pressure plotting models the results for normal and inverted attitudes are presented separately.

The tests were done between 1953 and 1957 in the No.2  $11\frac{1}{2}$  ft  $\times$   $8\frac{1}{2}$  ft wind tunnel at R.A.E. Farnborough and the 13 ft  $\times$  9 ft tunnel at R.A.E. Bedford. The wind speeds were 125 ft/sec and 250 ft/sec, giving Reynolds numbers of  $1.6 \times 10^6$  and  $3.2 \times 10^6$  based on the 24 inch chord of the wings. Relevant corrections were applied to incidence, lift, drag, pitching moment and pressure coefficient to take account of tunnel constraint, blockage, streamwise pressure gradient, asymmetry in pitch of the tunnel flow, and rig drag and pitching moment.

In addition to the balance and pressure measurements, some observations were made of the movement of the transition position on the balance models, using the simple paraffin evaporation technique.

#### Acknowledgement

The authors are indebted to many colleagues at Farnborough and Bedford for their assistance in experimental work and computing during the series of tests.

### 3 RESULTS AND DISCUSSION: WINGS WITH SYMMETRICAL SECTION

The pressure measurements at the centre section of the wings of the AP series are tabulated in Tables 2 to 6, and the local force and moment coefficients obtained by integration in Tables 7 to 11. Some of the pressure holes suffered either temporarily or permanently from blockages and leaks and these readings are omitted from the tables. The lift, drag and pitching moment coefficients from the measurements on the balance models of the AP series are tabulated in Tables 12 to 16, and the transition observations in Table 17.

For comparison with the experimental data the pressure distributions at the centre section of these wings have been computed by the method of Weber<sup>3</sup> for several values of the effective incidence  $\alpha_e$ , and these calculated values are given in Tables 45 to 49, along with the local normal force coefficient,  $C_N$ , obtained by integration.

#### 3.1 Pressure measurements at zero lift

The pressure measurements at the centre sections of the AP wings are directly comparable with the results calculated by Weber's method<sup>3</sup>, and the comparisons are shown in Fig.3. The experimental points plotted are the mean values of the pressure coefficient,  $C_p$ , on both sides of the wing at both attitudes at both Reynolds Numbers (where available). (Interpolation is necessary where zero incidence was not actually measured.) For wing AP/3 of aspect ratio 1.4 further data was available from the results of Peckham<sup>7</sup> on a similar planform with 12% RAE 101 section: the velocity increments have been scaled down linearly for comparison with the present results.

It is clear from Fig.3 that the theory of Ref.3 correctly predicts the qualitative reduction in peak suction and its forward movement as the aspect ratio is decreased, but that quantitatively the amount of this reduction is slightly underestimated. This discrepancy is due to the linearising assumption of the theory whereby the boundary conditions are satisfied on the chordline instead of on the wing surface. Fig.13 of Ref.3 shows that, for low aspect ratio ellipsoids with  $t/c = 0.10$ , the ratio of the exact theoretical velocity increment (and hence  $C_p$ ) at the midpoint of the centre section to the linearised theory value is the same as the ratio of experimental to calculated peak suction for wings AP/4 and AP/5.

#### 3.2 Balance measurements

To obtain a theoretical comparison for the total lift and pitching moment results on the AP series of wings, it is necessary to calculate the spanwise load distribution and then integrate over the span. If the total lift and spanwise load distribution are calculated for a given incidence, the "effective incidence"

$\alpha_e = \alpha - \alpha_1$  is known everywhere and thus the chordwise pressure distribution at the centre section can be calculated. Therefore, to be able to calculate accurately the pressure distribution ab initio, it is necessary to have an accurate method for estimating the spanwise load distribution. In practice the calculation of the chordwise pressure distribution may be related to the local normal force or lift coefficient rather than to  $\alpha_e$  (i.e.  $\alpha_e$  has to be chosen to give the required  $C_N$  or  $C_L$  on integrating the pressures) and this means that it is the shape of the spanwise load distribution rather than the actual calculated values of  $C_L/\alpha$  which is important.

As the aspect ratio is reduced, non-linear effects become more prominent in the aerodynamic characteristics. This is due to the effect of the tip vortex sheet which induces lift near the tips, mainly towards the rear of the wing. On small aspect ratio wings this non-linear lift becomes apparent at low incidences. Therefore in these cases loading calculations by linear theories such as that of Küchemann<sup>1</sup> or Multhopp<sup>8</sup> are directly applicable only for predicting the lift slope near zero incidence. The non-linear effects can be estimated by using the tip end plate methods of Mangler and Rotta<sup>9</sup> and Küchemann and Kettle<sup>10</sup>, and this is done in the present analysis.

As no experimental spanwise load distributions are available for the present wings, comparisons with linear theory can only be done through the total lift slope  $\bar{C}_L/\alpha$ , pitching moment  $\bar{C}_m$  and drag  $\bar{C}_D$ . For further consideration, Fig.4(a) shows some unpublished electrolytic tank results by Redshaw and Temple for the spanwise  $C_L$  distribution on a thin rectangular wing of aspect ratio 6. Although a large number of pivotal points is represented in this method, its accuracy is not necessarily assured because the singularities around the edges cannot be properly allowed for. These results are compared with a calculation by the Küchemann method<sup>1</sup> which appears to overestimate  $C_L/\alpha$ , particularly near the tip. A modification to the Küchemann method has been introduced here to take account of the known fact that towards the tip of a rectangular wing the chordwise loading changes shape slightly, the load being concentrated rather nearer the leading edge (excluding non-linear tip vortex effects). The details of this modification are given in Appendix A, and the plotted curve in Fig.4(a) shows better agreement with the tank results. In Fig.4(b) the shape of the spanwise loading curve from the tank tests is compared with a calculation by the Multhopp method<sup>8</sup> and the agreement is good when 4 chordwise points are taken. On this evidence the modified Küchemann method is tentatively accepted as sufficiently accurate for moderate aspect ratios, but this opinion may be modified in the light of the present tests. The Küchemann method has the advantage over the Multhopp

method that corrections to take account of wing thickness and boundary layer can be incorporated without difficulty. Figs.5(a) and 5(b) show calculated spanwise load distributions for the two extreme aspect ratios, 4.0 and 0.5, of the present series, using the modified and original Kuchemann methods and the Multhopp method with 4 chordwise points. The wing is assumed to be thin.

Table 18 compares the experimental lift curve slopes at zero lift of two of the AF series of wings with calculations by the original and modified Kuchemann methods, with and without a correction to take account the loss of lift due to the boundary layer. The latter took the form of a factor  $k = 0.92$  applied to the sectional lift slopes  $a = \partial C_L / \partial \alpha_e$ , the numerical value 0.92 having been previously found to be appropriate both to a  $45^\circ$  sweptback wing with 12% RAE 101 section<sup>11</sup> and a two-dimensional wing with 10% RAE 101 section<sup>6</sup> (wing AP/0). The wing thickness is allowed for in all cases by a factor  $(1 + 0.8 \times t/c)$  applied to the sectional lift slopes. It is, of course, not known whether it is permissible to allow for the boundary layer on a wing of finite span in the same way as on a two-dimensional aerofoil section. Nevertheless, one would expect the values obtained with  $k = 0.92$  to be more realistic than those with  $k = 1.0$ .

The lift curves for these wings, AF/1 and AF/5, are plotted in Figs.6 and 7 and estimates of the non-linear lift increment from the tip vortex effect are also shown. The main difficulty in this estimation is to calculate the height of the vortex sheet,  $h$ , in terms of the span  $b$ , and three approximations are given for this in Ref.1. These are quoted in Appendix B. The simplest approximation gives the best agreement with the present tests, which is gratifying in that the other two approximations require some knowledge of the shape of the lift curve and are therefore not suitable for an ab initio calculation.

The non-linear lift acts towards the rear of the section and therefore causes a nose-down pitching moment. Figs.8 and 9 show the pitching moment results for wings AF/1 and AF/5 along with the calculations by linear theory. The pitching moment due to the non-linear lift is estimated assuming this lift to act at 75% chord as suggested in Ref.1. The linear estimate is simply based on the parameter  $n$  (see Ref.1) at the centre section of the wing and takes no account of boundary layer and thickness effects. These tend to counteract each other and this simple thin wing estimate is in quite good agreement with the linear part of the  $\bar{C}_m$  v  $\bar{C}_L$  curve for both wings. The choice of approximation 1 (see Appendix B) in calculating the non-linear lift implies that the latter starts as soon as the incidence is non-zero and this is clearly wrong. However this approximation plus the assumption that the non-linear lift acts at 75% chord

gives a reasonable picture of the general behaviour of the pitching moment, although this aspect of the problem requires far more work.

From the spanwise loading, the induced drag or vortex drag,  $\bar{C}_{Di}$ , can be calculated. At any spanwise position the local vortex drag  $C_{Di} = C_L \times \alpha_{i0}$  where  $\alpha_{i0}$  is half the downwash induced far downstream by the trailing vortex system.  $\alpha_{i0}$  is related to the downwash angle  $\alpha_i$  at the wing by the factor  $\omega = \frac{\alpha_i}{\alpha_{i0}}$ . If the effect of the viscous boundary layer is omitted from the calculation ( $k = 1.0$ ),

$$\alpha_e = \alpha - \alpha_i .$$

If the boundary layer is assumed to reduce the incidence by an amount  $\alpha_B$ , thereby causing a loss of lift,

$$\alpha_e = \alpha' - \alpha_i - \alpha_B ,$$

$\alpha'$  being different from  $\alpha$  above. For the same  $C_L$  in the two cases  $\alpha_e$  is the same and the shape of the spanwise loading does not depend much on  $k$  so that  $\alpha_i$  is the same. Therefore  $\alpha = \alpha' - \alpha_B$  i.e.

$$\frac{\alpha_B}{\alpha'} = 1 - \frac{\alpha}{\alpha'} ;$$

$\frac{\alpha}{\alpha'}$  is the ratio of the local lift slopes; with (in this case)  $k = 0.92$  and  $k = 1.0$ ,  $\alpha_B$  can be found. The boundary layer drag  $C_{DB} = C_L \times \alpha_B$ , analogous to the vortex drag can then be added to  $C_{Di}$ . By integration over the span the total lift-dependent drag can be calculated.

The comparisons between calculation and experiment for wings AF/1 and AF/5 are shown in Figs.10 and 11. For wing AF/1 the values of  $\bar{C}_D - \bar{C}_{D0} = \bar{C}_{Di} + \bar{C}_{DB}$  given by the two calculation methods (original and modified) are very similar, though in fact the spanwise distribution of  $C_{Di}$  is very different in the two calculations. The agreement with experiment is not very good for wing AF/1, the actual drag being higher than the estimated drag. For wing AF/5 the two calculation methods give the same answer, the spanwise distribution of  $C_{Di}$  being similar in both. The agreement with experiment is good. All that this indicates, however, is that with small aspect ratio wings the near-elliptic spanwise loading is not sensitive to quite large changes in the calculation method.

In Figs.12 and 13 the total tangential force  $\bar{C}_T$  is plotted against  $\bar{C}_N^2$ , the square of the total normal force, for the same two wings AF/1 and AF/5. The experimental  $\bar{C}_T$  v  $\bar{C}_N^2$  curve does not pass through the origin because of the

effect of viscosity on the zero lift pressure distribution. Thus only the experimental and calculated slopes near zero lift are comparable. As shown in Ref.1  $C_T/C_N^2 = -\frac{1}{a}$  where these are local values at any spanwise position, and so the ratio  $\bar{C}_T/\bar{C}_N^2$  should define an average value of  $a$  for the whole wing. In the original Küchemann loading method  $a$  is constant over the wing and the  $C_T$  v  $C_N^2$  line corresponding to this theoretical value is drawn in Figs.12 and 13. In the modified method,  $a$  varies over the span and  $\frac{1}{a}$  lies in the range indicated by the shaded area.

The comparisons of Figs.10-13 show that the main trend in the initial slopes is correctly represented; they favour the original version of the calculation method rather than the modified version, so that despite the evidence of Table 18 and Fig.4 their relative merits are by no means established. Further analysis would seem desirable, especially of the non-linear effects.

### 3.3 Pressure measurements with lift

This section deals only with local force and moment coefficients obtained by integrating the pressure distributions at the centre sections of wings of the AP series. No analysis has so far been undertaken of the detailed pressure distributions except at zero lift as described in Section 3.1. Figs.14-21 for wings AP/1 and AP/5 correspond to Figs.6-13 for the AF series. The two lift slopes in Figs.14 and 15 differ less than the total lift slopes in Figs.6 and 7, since the two spanwise loading curves are most nearly the same at the centre section. Agreement with experiment over the linear range is good. Although it has not been done in the analysis so far, it is possible to estimate the spanwise distribution of non-linear lift as described in Ref.1.

The local pitching moments are plotted in Figs.16 and 17. The experimental scatter for wing AP/1 is considerable and points have been plotted for both attitudes. The calculated curve is in fair agreement with the mean experimental points. For AP/5, however, agreement between experiment and calculation is less good. As far as the centre section pitching moment is concerned there is no difference between the original and modified calculation methods.

The local drag due to lift and boundary layer in Figs.18 and 19 shows greater differences between the two calculation methods than the total coefficient shown in Figs.10 and 11. In both cases the original method gives better agreement with experiment. In contrast with the total force measurements, however, the agreement is better for the higher aspect ratio than for the lower one.

Finally in this section, the local values of  $C_T$  and  $C_N^2$  are plotted against each other in Figs.20 and 21, and the theoretical estimates of the slope



(the same by both methods) are in fair agreement with the linear part of the experimental curve.

#### 4 RESULTS AND DISCUSSION: WINGS WITH CAMBERED SECTIONS

The pressure measurements at the centre section of the wings of the BP series are tabulated in Tables 19 to 24, and the local force and moment coefficients in Tables 25 to 30. The lift, drag and pitching moment coefficients from the measurements on the balance models of the BF and CF series are given in Tables 31 to 40, and the transition observations in Tables 41 and 42.

No analysis has been done of the pressure plotting results for the BP series other than finding the local zero lift angle at the centre line, and this section contains only a very brief discussion of the balance measurements of the two cambered series. In Figs. 22 and 23 the total lift coefficient  $\bar{C}_L$  is plotted over a small range of incidence for all 10 wings in order to determine the zero lift angle. Experimental scatter makes this derivation rather uncertain. Assuming that the value of the parameter  $n$  at the centre section of a wing of given aspect ratio does not depend on the camber, and that this value represents the behaviour of the whole wing, the zero-lift angle of each wing can be estimated from the charts of Ref. 5\*. This estimate must be regarded as highly tentative, as there is no self-evident connection between the two problems considered. Table 43 gives the calculated and experimental values of the zero lift angle,  $\alpha_0$ , for the wings of the BF and CF series. The agreement is good for the higher aspect ratios, but whereas the theory predicts a steady increase in the magnitude of  $\alpha_0$  as the aspect ratio decreases the experiments show the opposite tendency.

Similarly in Fig. 24 the local normal force coefficients at the centre sections of the BP series are plotted against  $\alpha$  and the experimental and calculated zero lift angles are shown in Table 44.

There is a more rigorous treatment of thin cambered wings of small aspect ratio by Weber<sup>4</sup>. This has as yet not been applied to the present shapes of camber line. The variation with aspect ratio of the zero lift angles is less than would be expected from the results quoted by Weber<sup>4</sup> for other camber lines.

Finally, in Figs. 25-28 the total pitching moment coefficients are shown for the extreme aspect ratios of the BF and CF series. The calculated variation of  $\bar{C}_m$  with  $\bar{C}_L$  is also plotted, again on the assumption that  $n$  has the same value

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\*In these charts the parameter  $\lambda\phi$  is related to  $n$  by the equation

$$n = \frac{1}{2} \left( 1 - \frac{\lambda\phi}{\pi/2} \right)$$

as on an uncambered wing. In all cases  $\bar{C}_{mo}$  is overestimated, but the slopes  $\partial\bar{C}_m/\partial\bar{C}_L$  are in good agreement over the linear range.

5 FURTHER WORK

Considerable analysis of the pressure distributions is possible, particularly as regards the verification for small aspect ratios of approximations which are justifiable in calculations of high aspect ratio wings, and the methods of combining incidence thickness and camber terms in the formulae. Non-linear effects also require further consideration.

The modification to the Kuechemann method for calculating the spanwise load distribution, which appears justified by comparison with electrolytic tank results, is by no means justified by the results of the present series of tests and further evidence on this point is needed.

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Appendix A  
MODIFICATION TO KÜCHEMANN LOADING METHOD

In the original Küchemann method for calculating spanwise load distribution the aspect ratio is reflected in a parameter  $n$  which governs the shape of the chordwise load distribution, and  $n$  is assumed to be constant over the whole span for an unswept wing. It is defined by

$$n = 1 - \frac{1}{2 \left[ 1 + \left( \frac{a_0}{\pi A} \right)^2 \right]^{1/4}},$$

where  $a_0$  is the two-dimensional lift slope of the section and  $A$  is the aspect ratio.

In the modified method,  $n$  at any spanwise position is obtained as the mean value of two parameters  $n'$  and  $n''$  which are based on the proximity of the section to the two tips. For example, on a rectangular wing of aspect ratio 4 the section half-way out along the span is assumed to behave in relation to the nearer tip as though it were the centre section of a wing of aspect ratio 2: and in relation to the further tip as though it were the centre section of a wing of aspect ratio 6. These two aspect ratios define  $n'$  and  $n''$  and the resultant  $n = \frac{n' + n''}{2}$ .

This modification causes  $n$  to increase towards the tips which is in qualitative agreement with observed effects in the absence of a marked tip vortex sheet. The sectional lift slope will also vary over the span of a rectangular wing. The value of  $n$  at the centre section remains as in the original method.

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Appendix BAPPROXIMATIONS FOR THE HEIGHT OF A TIP VORTEX SHEET

$$\text{Approximation 1:- } \frac{h}{b} = \frac{\alpha}{2} \frac{c_T}{\bar{c}} \frac{1}{\Lambda}$$

$$\text{Approximation 2:- } \frac{h}{b} = \frac{\alpha - \alpha_s}{2} \frac{c_T}{\bar{c}} \frac{1}{\Lambda}$$

$$\text{Approximation 3:- } \frac{h}{b} = \alpha \frac{\alpha - \alpha_s}{\alpha_m - \alpha_s} \frac{c_T}{\bar{c}} \frac{1}{\Lambda}$$

where  $h$  = height of vortex sheet

$b$  = span

$c_T$  = tip chord

$\bar{c}$  = mean chord

$\alpha$  = incidence

$\alpha_s$  = incidence at which separation starts from the tip

$\alpha_m$  = incidence at which separation starts from the leading edge.

$\frac{h}{b}$  is related to a factor  $k$  (see Ref.9) which then enables the non-linear lift to be determined from equation (39) of Ref.1.

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Table 1  
SUMMARY OF WINGS TESTED

| Aspect ratio | Balance models      |                              |                              | Pressure models     |                              |
|--------------|---------------------|------------------------------|------------------------------|---------------------|------------------------------|
|              | Symmetrical section | m = 0.5 mean line, 2% camber | m = 0.8 mean line, 1% camber | Symmetrical section | m = 0.5 mean line, 2% camber |
| $\infty$     | -                   | -                            | -                            | AP/0<br>(Ref.6)     | BP/0                         |
| 4.0          | AF/1                | BF/1*                        | CF/1                         | AP/1 $\phi$         | BP/1                         |
| 2.5          | AF/2                | BF/2 <sup>+</sup>            | CF/2                         | AP/2 $\phi$         | BP/2 <sup>+</sup>            |
| 1.4          | AF/3                | BF/3                         | CF/3                         | AP/3                | BP/3                         |
| 1.0          | AF/4                | BF/4                         | CF/4                         | AP/4                | BP/4                         |
| 0.5          | AF/5                | BF/5                         | CF/5                         | AP/5                | BP/5                         |

\* Tested only at  $R = 1.6 \times 10^6$ , normal attitude.

+ Tested only in normal attitude.

‡ No test at  $R = 3.2 \times 10^6$ , inverted attitude.

$\phi$  Tested only at  $R = 1.6 \times 10^6$ .



Table 2 (contd)

Wing AP/1, inverted attitude

$C_p$

$V = 125 \text{ ft/sec}, R = 1.6 \times 10^6$

| $\alpha$<br>X/C | 4.7°   | 2.5°   | 1.45°  | 0.35°  | -0.75° | -1.85° | -4.0°  | -6.2°  | -8.4°  | -10.55° | -11.65° | -12.75° | -13.4° | -14.5° | -14.85° |
|-----------------|--------|--------|--------|--------|--------|--------|--------|--------|--------|---------|---------|---------|--------|--------|---------|
| Upper Surface   |        |        |        |        |        |        |        |        |        |         |         |         |        |        |         |
| 0               | 0.331  | 0.830  | 0.964  | 0.995  | 0.962  | 0.851  | 0.190  | -0.550 | -1.845 | -3.576  | -4.696  | -5.476  | -6.261 | -0.483 | -0.249  |
| 0.005           | -1.127 | -0.383 | -0.035 | 0.253  | 0.485  | 0.675  | 0.925  | 0.995  | 0.942  | 0.749   | 0.552   | 0.416   | 0.284  | 0.968  | 0.978   |
| 0.015           | -1.040 | -0.508 | -0.246 | -0.023 | 0.176  | 0.361  | 0.653  | 0.854  | 0.969  | 1.001   | 0.977   | 0.957   | 0.939  | 0.970  | 0.956   |
| 0.030           | -0.954 | -0.556 | -0.323 | -0.170 | -0.006 | 0.145  | 0.420  | 0.627  | 0.799  | 0.909   | 0.953   | 0.969   | 0.993  | 0.839  | 0.822   |
| 0.050           | -0.843 | -0.540 | -0.381 | -0.229 | -0.099 | 0.023  | 0.253  | 0.369  | 0.623  | 0.761   | 0.822   | 0.863   | 0.893  | 0.699  | 0.679   |
| 0.075           | -0.759 | -0.517 | -0.390 | -0.268 | -0.162 | -0.055 | 0.148  | 0.320  | 0.481  | 0.617   | 0.690   | 0.733   | 0.762  | 0.574  | 0.559   |
| 0.100           | -0.688 | -0.501 | -0.390 | -0.287 | -0.191 | -0.100 | 0.084  | 0.236  | 0.382  | 0.517   | 0.585   | 0.631   | 0.660  | 0.484  | 0.473   |
| 0.200           | -0.576 | -0.457 | -0.384 | -0.314 | -0.247 | -0.194 | -0.061 | 0.050  | 0.167  | 0.278   | 0.337   | 0.377   | 0.405  | 0.261  | 0.247   |
| 0.300           | -0.514 | -0.431 | -0.379 | -0.321 | -0.277 | -0.230 | -0.131 | -0.051 | 0.048  | 0.141   | 0.191   | 0.233   | 0.256  | 0.116  | 0.101   |
| 0.400           | -0.375 | -0.339 | -0.294 | -0.255 | -0.221 | -0.194 | -0.108 | -0.048 | 0.033  | 0.103   | 0.146   | 0.178   | 0.195  | 0.064  | 0.050   |
| 0.500           | -0.289 | -0.234 | -0.237 | -0.201 | -0.172 | -0.150 | -0.085 | -0.036 | 0.024  | 0.079   | 0.121   | 0.142   | 0.158  | 0.031  | 0.007   |
| 0.650           | -      | -      | -      | -      | -      | -      | -      | -      | -      | -       | -       | -       | -      | -      | -       |
| 0.750           | -0.085 | -0.066 | -0.049 | -0.038 | -0.022 | -0.009 | 0      | 0.019  | 0.059  | 0.087   | 0.096   | 0.121   | 0.127  | -0.036 | -0.077  |
| 0.850           | -0.027 | -0.016 | -0.006 | 0.001  | 0.008  | 0.017  | 0.047  | 0.031  | 0.059  | 0.081   | 0.095   | 0.106   | 0.107  | -0.087 | -0.142  |
| 0.950           | -      | -      | -      | -      | -      | -      | -      | -      | -      | -       | -       | -       | -      | -      | -       |
| Lower Surface   |        |        |        |        |        |        |        |        |        |         |         |         |        |        |         |
| 0.005           | 0.935  | 0.699  | 0.503  | 0.258  | -0.021 | -0.363 | -1.133 | -2.096 | -3.124 | -4.580  | -5.741  | -6.570  | -7.395 | -0.771 | -0.504  |
| 0.015           | 0.656  | 0.381  | 0.193  | -0.020 | -0.236 | -0.498 | -1.035 | -1.676 | -2.750 | -2.890  | -3.458  | -3.778  | -4.112 | -0.713 | -0.508  |
| 0.030           | 0.408  | 0.148  | -0.016 | -0.186 | -0.360 | -0.563 | -0.963 | -1.442 | -1.834 | -2.415  | -2.679  | -2.885  | -3.100 | -0.693 | -0.501  |
| 0.050           | 0.258  | 0.040  | -0.095 | -0.232 | -0.375 | -0.532 | -0.829 | -1.140 | -1.510 | -1.870  | -2.088  | -2.223  | -2.344 | -0.678 | -0.480  |
| 0.075           | 0.145  | -0.047 | -0.157 | -0.268 | -0.382 | -0.512 | -0.745 | -0.981 | -1.267 | -1.540  | -1.701  | -1.794  | -1.886 | -0.664 | -0.480  |
| 0.100           | 0.071  | -0.094 | -0.194 | -0.292 | -0.390 | -0.498 | -0.693 | -0.905 | -1.126 | -1.351  | -1.474  | -1.554  | -1.630 | -0.664 | -0.482  |
| 0.200           | -0.049 | -0.167 | -0.229 | -0.294 | -0.359 | -0.435 | -0.523 | -0.670 | -0.801 | -0.928  | -1.080  | -1.016  | -1.083 | -0.682 | -0.498  |
| 0.300           | -0.116 | -0.208 | -0.251 | -0.299 | -0.353 | -0.403 | -0.476 | -0.581 | -0.672 | -0.751  | -0.871  | -0.808  | -0.840 | -0.689 | -0.504  |
| 0.400           | -0.095 | -0.162 | -0.198 | -0.237 | -0.267 | -0.315 | -0.349 | -0.429 | -0.487 | -0.548  | -0.572  | -0.587  | -0.583 | -0.687 | -0.504  |
| 0.500           | -0.099 | -0.147 | -0.174 | -0.205 | -0.231 | -0.225 | -0.274 | -0.319 | -0.351 | -0.373  | -0.382  | -0.386  | -0.390 | -0.635 | -0.504  |
| 0.650           | 0.002  | -0.030 | -0.023 | -0.045 | -0.066 | -0.089 | -0.114 | -0.150 | -0.178 | -0.200  | -0.209  | -0.211  | -0.221 | -0.588 | -0.508  |
| 0.750           | 0.043  | 0.035  | 0.021  | 0.001  | -0.008 | -0.026 | -0.038 | -0.072 | -0.090 | -0.104  | -0.107  | -0.110  | -0.119 | -0.529 | -0.511  |
| 0.850           | 0.038  | 0.021  | 0.008  | -0.001 | -0.006 | -0.019 | -0.024 | -0.045 | -0.052 | -0.059  | -0.055  | -0.054  | -0.059 | -0.473 | -0.505  |
| 0.950           | 0.047  | 0.045  | 0.040  | 0.038  | 0.032  | 0.032  | 0.035  | 0.024  | 0.021  | 0.022   | 0.024   | 0.021   | 0.015  | -0.397 | -0.459  |





Wing AP/2, normal attitude

$\zeta$

$V = 125 \text{ ft/sec}, R = 1.6 \times 10^6$

Table 3

| $\alpha$ | X/C   | Upper Surface |        |        |        |        |        |        |        |        |        |        |        | Lower Surface |        |        |        |        |        |        |        |        |        |        |        |        |        |
|----------|-------|---------------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|---------------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| 4.1°     | 0.561 | 0.904         | 1.000  | 0.897  | 0.593  | 0.042  | -0.801 | -1.729 | -3.041 | -4.320 | -4.836 | -0.275 | -0.216 | 0.005         | 0.561  | 0.904  | 1.000  | 0.897  | 0.593  | 0.042  | -0.801 | -1.729 | -3.041 | -4.320 | -4.836 | -0.275 | -0.216 |
|          | 0.005 | 0.863         | 0.614  | 0.271  | -0.225 | -0.765 | -1.427 | -2.285 | -3.236 | -4.789 | -6.222 | -6.736 | -0.492 | 0.005         | 0.863  | 0.614  | 0.271  | -0.225 | -0.765 | -1.427 | -2.285 | -3.236 | -4.789 | -6.222 | -6.736 | -0.492 | 0.005  |
|          | 0.015 | 0.573         | 0.302  | 0      | -0.391 | -0.777 | -1.226 | -1.808 | -2.069 | -2.726 | -3.280 | -3.765 | -0.484 | 0.015         | 0.573  | 0.302  | 0      | -0.391 | -0.777 | -1.226 | -1.808 | -2.069 | -2.726 | -3.280 | -3.765 | -0.484 | 0.015  |
|          | 0.030 | -0.811        | -0.477 | -0.180 | -0.082 | -0.745 | -1.080 | -1.522 | -1.753 | -2.170 | -2.542 | -2.691 | -0.475 | 0.030         | -0.811 | -0.477 | -0.180 | -0.082 | -0.745 | -1.080 | -1.522 | -1.753 | -2.170 | -2.542 | -2.691 | -0.475 | 0.030  |
|          | 0.050 | -0.716        | -0.460 | -0.226 | -0.020 | -0.620 | -0.976 | -1.214 | -1.388 | -1.444 | -1.472 | -1.480 | -0.487 | 0.050         | -0.716 | -0.460 | -0.226 | -0.020 | -0.620 | -0.976 | -1.214 | -1.388 | -1.444 | -1.472 | -1.480 | -0.487 | 0.050  |
|          | 0.075 | -0.651        | -0.453 | -0.259 | -0.094 | -0.569 | -0.882 | -1.099 | -1.203 | -1.253 | -1.272 | -1.279 | -0.480 | 0.075         | -0.651 | -0.453 | -0.259 | -0.094 | -0.569 | -0.882 | -1.099 | -1.203 | -1.253 | -1.272 | -1.279 | -0.480 | 0.075  |
|          | 0.100 | -0.618        | -0.451 | -0.280 | -0.140 | -0.548 | -0.822 | -1.039 | -1.147 | -1.214 | -1.253 | -1.259 | -0.480 | 0.100         | -0.618 | -0.451 | -0.280 | -0.140 | -0.548 | -0.822 | -1.039 | -1.147 | -1.214 | -1.253 | -1.259 | -0.480 | 0.100  |
|          | 0.200 | -0.498        | -0.393 | -0.288 | -0.198 | -0.439 | -0.678 | -0.855 | -0.968 | -1.034 | -1.077 | -1.084 | -0.480 | 0.200         | -0.498 | -0.393 | -0.288 | -0.198 | -0.439 | -0.678 | -0.855 | -0.968 | -1.034 | -1.077 | -1.084 | -0.480 | 0.200  |
|          | 0.300 | -0.440        | -0.271 | -0.295 | -0.234 | -0.361 | -0.512 | -0.609 | -0.681 | -0.726 | -0.753 | -0.759 | -0.480 | 0.300         | -0.440 | -0.271 | -0.295 | -0.234 | -0.361 | -0.512 | -0.609 | -0.681 | -0.726 | -0.753 | -0.759 | -0.480 | 0.300  |
|          | 0.400 | -0.314        | -0.287 | -0.228 | -0.188 | -0.277 | -0.357 | -0.426 | -0.477 | -0.507 | -0.519 | -0.522 | -0.480 | 0.400         | -0.314 | -0.287 | -0.228 | -0.188 | -0.277 | -0.357 | -0.426 | -0.477 | -0.507 | -0.519 | -0.522 | -0.480 | 0.400  |
|          | 0.500 | -             | -      | -      | -      | -      | -      | -      | -      | -      | -      | -      | -      | 0.500         | -      | -      | -      | -      | -      | -      | -      | -      | -      | -      | -      | -      | 0.500  |
|          | 0.650 | -0.090        | -0.069 | -0.036 | -0.019 | -0.011 | 0.041  | 0.073  | 0.108  | 0.135  | 0.141  | 0.142  | 0.029  | 0.650         | -0.090 | -0.069 | -0.036 | -0.019 | -0.011 | 0.041  | 0.073  | 0.108  | 0.135  | 0.141  | 0.142  | 0.029  | 0.650  |
|          | 0.750 | -0.014        | -0.006 | 0.019  | 0.030  | 0.058  | 0.047  | 0.066  | 0.083  | 0.125  | 0.138  | 0.146  | 0.009  | 0.750         | -0.014 | -0.006 | 0.019  | 0.030  | 0.058  | 0.047  | 0.066  | 0.083  | 0.125  | 0.138  | 0.146  | 0.009  | 0.750  |
|          | 0.850 | 0             | 0.015  | 0.026  | 0.030  | 0.051  | 0.068  | 0.059  | 0.078  | 0.098  | 0.106  | 0.107  | -0.044 | 0.850         | 0      | 0.015  | 0.026  | 0.030  | 0.051  | 0.068  | 0.059  | 0.078  | 0.098  | 0.106  | 0.107  | -0.044 | 0.850  |
|          | 0.950 | 0.068         | 0.068  | 0.074  | 0.066  | 0.080  | 0.083  | 0.088  | 0.087  | 0.094  | 0.086  | 0.079  | -0.194 | 0.950         | 0.068  | 0.068  | 0.074  | 0.066  | 0.080  | 0.083  | 0.088  | 0.087  | 0.094  | 0.086  | 0.079  | -0.194 | 0.950  |

Table 3 (Contd)

Wing AP/2, Inverted attitude

C<sub>D</sub>

V = 125 ft/sec, R = 1.6 x 10<sup>6</sup>

| $\alpha$<br>x/c | 4.55°         | 2.45°  | 0.35°  | -1.7°  | -3.8°  | -5.9°  | -8.0°  | -10.05° | -12.15° | -14.2° | -15.25° | -16.1° | -17.45° |
|-----------------|---------------|--------|--------|--------|--------|--------|--------|---------|---------|--------|---------|--------|---------|
|                 | Upper Surface |        |        |        |        |        |        |         |         |        |         |        |         |
| 0               | 0.577         | 0.907  | 1.027  | 0.905  | 0.577  | 0.045  | -0.891 | -2.032  | -3.515  | -5.068 | -5.960  | -0.406 | -0.256  |
| 0.005           | -0.805        | -0.213 | 0.273  | 0.613  | 0.868  | 0.988  | 1.000  | 0.919   | 0.746   | 0.475  | 0.306   | 0.960  | 0.972   |
| 0.015           | -0.821        | -0.401 | -0.014 | 0.284  | 0.558  | 0.760  | 0.904  | 0.978   | 1.000   | 0.978  | 0.946   | 0.972  | 0.975   |
| 0.030           | -0.761        | -0.449 | -0.140 | 0.104  | 0.345  | 0.517  | 0.700  | 0.824   | 0.915   | 0.978  | 0.993   | 0.895  | 0.855   |
| 0.050           | -0.690        | -0.452 | -0.205 | -0.013 | 0.192  | 0.362  | 0.521  | 0.649   | 0.763   | 0.857  | 0.889   | 0.702  | 0.712   |
| 0.075           | -0.630        | -0.452 | -0.250 | -0.085 | 0.087  | 0.241  | 0.378  | 0.504   | 0.618   | 0.718  | 0.760   | 0.582  | 0.591   |
| 0.100           | -0.579        | -0.435 | -0.255 | -0.117 | 0.030  | 0.160  | 0.293  | 0.413   | 0.519   | 0.621  | 0.663   | 0.494  | 0.509   |
| 0.200           | -0.489        | -0.406 | -0.291 | -0.205 | -0.100 | 0.009  | 0.091  | 0.184   | 0.272   | 0.355  | 0.396   | 0.271  | 0.278   |
| 0.300           | -0.457        | -0.387 | -0.305 | -0.246 | -0.169 | -0.090 | -0.025 | 0.050   | 0.124   | 0.198  | 0.229   | 0.124  | 0.129   |
| 0.400           | -0.422        | -0.303 | -0.240 | -0.203 | -0.145 | -0.097 | -0.036 | 0.021   | 0.103   | 0.138  | 0.162   | 0.060  | 0.061   |
| 0.500           | -0.243        | -0.225 | -0.181 | -0.147 | -0.105 | -0.065 | -0.024 | 0.025   | 0.113   | 0.119  | 0.137   | 0.040  | 0.031   |
| 0.650           | -             | -      | -      | -      | -      | -      | -      | -       | -       | -      | -       | -      | -       |
| 0.750           | -0.035        | -0.040 | -0.011 | 0.004  | 0      | 0.014  | 0.041  | 0.064   | 0.098   | 0.112  | 0.120   | -0.005 | -0.033  |
| 0.850           | 0.017         | 0.010  | 0.029  | 0.032  | 0.048  | 0.035  | 0.046  | 0.068   | 0.098   | 0.097  | 0.101   | -0.052 | -0.089  |
| 0.950           | -             | -      | -      | -      | -      | -      | -      | -       | -       | -      | -       | -      | -       |
|                 | Lower Surface |        |        |        |        |        |        |         |         |        |         |        |         |
| 0.005           | 0.885         | 0.625  | 0.273  | -0.222 | -0.827 | -1.575 | -2.374 | -3.228  | -4.442  | -6.174 | -7.024  | -0.639 | -0.438  |
| 0.015           | 0.585         | 0.304  | -0.003 | -0.388 | -0.822 | -1.321 | -1.874 | -2.637  | -2.843  | -3.572 | -3.920  | -0.594 | -0.436  |
| 0.030           | 0.337         | 0.084  | -0.169 | -0.472 | -0.798 | -1.171 | -1.596 | -1.869  | -2.302  | -2.712 | -2.916  | -0.581 | -0.434  |
| 0.050           | 0.205         | -0.016 | -0.212 | -0.455 | -0.705 | -0.984 | -1.191 | -1.513  | -1.803  | -2.107 | -2.239  | -0.570 | -0.427  |
| 0.075           | 0.096         | -0.088 | -0.250 | -0.448 | -0.638 | -0.856 | -1.034 | -1.259  | -1.471  | -1.691 | -1.791  | -0.573 | -0.431  |
| 0.100           | 0.032         | -0.131 | -0.274 | -0.446 | -0.604 | -0.756 | -0.935 | -1.108  | -1.276  | -1.454 | -1.534  | -0.592 | -0.436  |
| 0.200           | -0.075        | -0.188 | -0.274 | -0.386 | -0.485 | -0.557 | -0.658 | -0.766  | -0.856  | -0.947 | -0.991  | -0.611 | -0.471  |
| 0.300           | -0.128        | -0.220 | -0.276 | -0.365 | -0.425 | -0.497 | -0.557 | -0.619  | -0.678  | -0.731 | -0.754  | -0.668 | -0.504  |
| 0.400           | -0.100        | -0.174 | -0.214 | -0.279 | -0.298 | -0.363 | -0.404 | -0.443  | -0.483  | -0.517 | -0.526  | -0.664 | -0.532  |
| 0.500           | -0.061        | -0.119 | -0.152 | -0.171 | -0.210 | -0.247 | -0.278 | -0.311  | -0.337  | -0.354 | -0.359  | -0.629 | -0.550  |
| 0.650           | 0.007         | -0.021 | -0.028 | -0.064 | -0.081 | -0.107 | -0.124 | -0.145  | -0.154  | -0.164 | -0.168  | -0.559 | -0.553  |
| 0.750           | 0.076         | 0.041  | 0.029  | 0.005  | -0.009 | -0.030 | -0.043 | -0.054  | -0.063  | -0.070 | -0.078  | -0.492 | -0.529  |
| 0.850           | 0.064         | 0.027  | 0.029  | 0.007  | 0      | -0.008 | -0.012 | -0.027  | -0.027  | -0.026 | -0.033  | -0.424 | -0.497  |
| 0.950           | 0.089         | 0.070  | 0.069  | 0.059  | 0.060  | 0.059  | 0.055  | 0.047   | 0.045   | 0.046  | 0.030   | -0.316 | -0.395  |

Table 3 (Contd)

Wing AP/2, normal attitude

$\Delta C_p$

V = 125 ft/sec, R = 1.6 x 10<sup>6</sup>

| $\alpha$<br>x/c | -4.1° | -2.05° | 0.05°  | 2.15°  | 4.0°   | 6.05°  | 8.15°  | 10.25° | 12.35° | 14.4°  | 15.1°  | 16.5°  | 17.65° |
|-----------------|-------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| 0               | 0     | 0      | 0      | 0      | 0      | 0      | 0      | 0      | 0      | 0      | 0      | 0      | 0      |
| 0.005           | 1.710 | 0.827  | 0.009  | -0.852 | -1.623 | -2.396 | -3.280 | -4.152 | -5.498 | -6.649 | -7.045 | -1.555 | -1.466 |
| 0.015           | 1.410 | 0.685  | 0.027  | -0.699 | -1.331 | -1.968 | -2.712 | -3.043 | -3.731 | -4.251 | -4.718 | -1.558 | -1.470 |
| 0.030           | 1.152 | 0.576  | 0.038  | -0.543 | -1.054 | -1.580 | -2.204 | -2.550 | -3.085 | -3.511 | -3.676 | -1.424 | -1.332 |
| 0.050           | 0.909 | 0.459  | 0.017  | -0.438 | -0.848 | -1.265 | -1.664 | -2.054 | -2.504 | -2.870 | -3.004 | -1.284 | -1.195 |
| 0.075           | 0.742 | 0.371  | 0.017  | -0.357 | -0.689 | -1.024 | -1.376 | -1.686 | -2.061 | -2.363 | -2.462 | -1.167 | -1.081 |
| 0.100           | 0.655 | 0.336  | 0.031  | -0.294 | -0.572 | -0.813 | -1.130 | -1.405 | -1.720 | -1.992 | -2.075 | -1.078 | -0.988 |
| 0.200           | 0.408 | 0.201  | 0.009  | -0.201 | -0.384 | -0.565 | -0.773 | -0.946 | -1.152 | -1.316 | -1.374 | -0.919 | -0.799 |
| 0.300           | 0.288 | 0.143  | 0.008  | -0.144 | -0.278 | -0.403 | -0.557 | -0.672 | -0.824 | -0.937 | -0.973 | -0.801 | -0.701 |
| 0.400           | 0.193 | 0.107  | 0.005  | -0.104 | -0.163 | -0.269 | -0.379 | -0.472 | -0.580 | -0.664 | -0.686 | -0.759 | -0.675 |
| 0.500           | -     | -      | -      | -      | -      | -      | -      | -      | -      | -      | -      | -      | -      |
| 0.650           | -     | -      | -      | -      | -      | -      | -      | -      | -      | -      | -      | -      | -      |
| 0.750           | 0.034 | 0.019  | -0.022 | -0.059 | -0.094 | -0.093 | -0.124 | -0.146 | -0.194 | -0.217 | -0.223 | -0.528 | -0.541 |
| 0.850           | 0.061 | 0.031  | 0.014  | -0.046 | -0.031 | -0.056 | -0.059 | -0.079 | -0.096 | -0.111 | -0.117 | -0.370 | -0.390 |
| 0.950           | -     | -      | -      | -      | -      | -      | -      | -      | -      | -      | -      | -      | -      |

Wing AP/2, inverted attitude

$\Delta C_p$

V = 125 ft/sec, R = 1.6 x 10<sup>6</sup>

| $\alpha$<br>x/c | 4.55° | 2.45° | 0.35°  | -1.7°  | -3.8°  | -5.9°  | -8.0°  | -9.05° | -12.15° | -14.2° | -15.25° | -16.1° | -17.45° |
|-----------------|-------|-------|--------|--------|--------|--------|--------|--------|---------|--------|---------|--------|---------|
| 0               | 0     | 0     | 0      | 0      | 0      | 0      | 0      | 0      | 0       | 0      | 0       | 0      | 0       |
| 0.005           | 1.690 | 0.838 | 0      | -0.835 | -1.695 | -2.563 | -3.374 | -4.147 | -5.188  | -6.649 | -7.330  | -1.599 | -1.410  |
| 0.015           | 1.406 | 0.705 | 0.011  | -0.672 | -1.380 | -2.081 | -2.778 | -3.615 | -3.843  | -4.550 | -4.866  | -1.566 | -1.411  |
| 0.030           | 1.098 | 0.533 | -0.019 | -0.576 | -1.143 | -1.688 | -2.296 | -2.693 | -3.217  | -3.690 | -3.909  | -1.476 | -1.289  |
| 0.050           | 0.895 | 0.436 | -0.007 | -0.442 | -0.897 | -1.346 | -1.712 | -2.162 | -2.566  | -2.958 | -3.128  | -1.272 | -1.139  |
| 0.075           | 0.726 | 0.364 | 0      | -0.363 | -0.725 | -1.097 | -1.412 | -1.763 | -2.089  | -2.409 | -2.551  | -1.155 | -1.022  |
| 0.100           | 0.611 | 0.304 | -0.009 | -0.329 | -0.634 | -0.916 | -1.228 | -1.521 | -1.795  | -2.075 | -2.197  | -1.086 | -0.945  |
| 0.200           | 0.414 | 0.218 | 0.017  | -0.181 | -0.385 | -0.566 | -0.749 | -0.950 | -1.128  | -1.302 | -1.387  | -0.882 | -0.749  |
| 0.300           | 0.329 | 0.167 | 0.029  | -0.119 | -0.256 | -0.409 | -0.532 | -0.669 | -0.802  | -0.929 | -0.983  | -0.792 | -0.633  |
| 0.400           | 0.322 | 0.129 | 0.026  | -0.066 | -0.153 | -0.266 | -0.368 | -0.464 | -0.586  | -0.655 | -0.688  | -0.724 | -0.593  |
| 0.500           | 0.182 | 0.106 | 0.029  | -0.024 | -0.105 | -0.182 | -0.254 | -0.336 | -0.450  | -0.473 | -0.496  | -0.669 | -0.581  |
| 0.650           | -     | -     | -      | -      | -      | -      | -      | -      | -       | -      | -       | -      | -       |
| 0.750           | 0.111 | 0.081 | 0.040  | 0.001  | -0.009 | -0.044 | -0.084 | -0.118 | -0.161  | -0.182 | -0.198  | -0.487 | -0.496  |
| 0.850           | 0.047 | 0.017 | 0      | -0.025 | -0.048 | -0.043 | -0.058 | -0.095 | -0.125  | -0.117 | -0.134  | -0.372 | -0.407  |
| 0.950           | -     | -     | -      | -      | -      | -      | -      | -      | -       | -      | -       | -      | -       |

Table 4

Wing AP/3, normal attitude

C<sub>p</sub>

V = 250 ft/sec; R = 3.2 x 10<sup>6</sup>

| $\alpha$<br>I/C | -3.75° | -2.7°  | -1.7°  | -0.7°  | 0.3°   | 1.35°  | 2.35°  | 3.35°  | 4.35°  | 6.4°   | 8.4°   | 10.45° | 12.5°  | 14.5°  | 16.5°  | 17.55° |
|-----------------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| Upper surface   |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |
| 0               | 0.781  | 0.890  | 0.959  | 0.994  | 1.000  | 1.000  | 0.963  | 0.886  | 0.760  | 0.409  | -0.075 | -0.678 | -1.530 | -2.440 | -3.478 | -4.022 |
| 0.005           | 0.773  | 0.672  | 0.556  | 0.420  | 0.269  | 0.107  | -0.089 | -0.291 | -0.535 | -1.075 | -1.612 | -      | -      | -      | -      | -      |
| 0.015           | 0.466  | 0.362  | 0.254  | 0.139  | 0.011  | -0.120 | -0.271 | -0.420 | -0.595 | -0.958 | -1.332 | -1.625 | -2.070 | -2.512 | -2.982 | -3.219 |
| 0.030           | 0.228  | 0.139  | 0.048  | -0.046 | -0.149 | -0.253 | -0.367 | -0.481 | -0.611 | -0.873 | -1.158 | -1.396 | -1.709 | -2.008 | -2.309 | -2.457 |
| 0.050           | 0.102  | 0.026  | -0.050 | -0.126 | -0.208 | -0.274 | -0.380 | -0.466 | -0.565 | -0.762 | -0.893 | -1.103 | -1.324 | -1.531 | -1.740 | -1.846 |
| 0.075           | 0.006  | -0.054 | -0.118 | -0.179 | -0.247 | -0.311 | -0.384 | -0.449 | -0.528 | -0.651 | -0.797 | -0.942 | -1.108 | -1.259 | -1.411 | -1.487 |
| 0.100           | -0.050 | -0.101 | -0.157 | -0.202 | -0.264 | -0.319 | -0.377 | -0.432 | -0.496 | -0.618 | -0.753 | -0.851 | -0.979 | -1.098 | -1.218 | -1.272 |
| 0.200           | -0.151 | -0.185 | -0.220 | -0.251 | -0.284 | -0.318 | -0.350 | -0.382 | -0.426 | -0.491 | -0.553 | -0.615 | -0.681 | -0.740 | -0.798 | -0.826 |
| 0.300           | -0.203 | -0.220 | -0.245 | -0.262 | -0.288 | -0.311 | -0.332 | -0.349 | -0.341 | -0.309 | -0.426 | -0.465 | -0.502 | -0.545 | -0.570 | -0.586 |
| 0.400           | -0.161 | -0.177 | -0.198 | -0.206 | -0.227 | -0.244 | -0.218 | -0.234 | -0.254 | -0.284 | -0.307 | -0.330 | -0.354 | -0.377 | -0.396 | -0.404 |
| 0.500           | -0.124 | -0.131 | -0.134 | -0.144 | -0.149 | -0.162 | -0.171 | -0.179 | -0.191 | -0.207 | -0.221 | -0.234 | -0.246 | -0.259 | -0.270 | -0.274 |
| 0.650           | -      | -      | -      | -      | -      | -      | -      | -      | -      | -      | -      | -      | -      | -      | -      | -      |
| 0.750           | 0.006  | 0.001  | -0.006 | -0.003 | -0.008 | -0.012 | -0.011 | -0.013 | -0.017 | -0.020 | -0.022 | -0.026 | -0.029 | -0.033 | -0.035 | -0.036 |
| 0.850           | 0.034  | 0.034  | 0.030  | 0.034  | 0.031  | 0.030  | 0.030  | 0.031  | 0.030  | 0.030  | 0.032  | 0.031  | 0.031  | 0.032  | 0.032  | 0.031  |
| 0.950           | -      | -      | -      | -      | -      | -      | -      | -      | -      | -      | -      | -      | -      | -      | -      | -      |
| Lower surface   |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |
| 0.005           | -      | -      | -      | -      | -      | -      | -      | -      | -      | -      | -      | 1.009  | 0.952  | 0.835  | 0.656  | 0.547  |
| 0.015           | -0.585 | -0.437 | -0.294 | -0.154 | -0.019 | 0.101  | 0.195  | 0.345  | 0.453  | 0.642  | 0.773  | 0.903  | 0.978  | 1.011  | 1.010  | 1.005  |
| 0.030           | -0.615 | -0.505 | -0.395 | -0.280 | -0.178 | -0.081 | 0.024  | 0.123  | 0.218  | 0.395  | 0.531  | 0.678  | 0.793  | 0.879  | 0.944  | 0.967  |
| 0.050           | -      | -      | -      | -      | -      | -      | -      | -      | -      | -      | -      | -      | -      | -      | -      | -      |
| 0.075           | -0.519 | -0.453 | -0.393 | -0.324 | -0.261 | -0.212 | -0.130 | -0.066 | 0.002  | 0.129  | 0.231  | 0.353  | 0.465  | 0.559  | 0.647  | 0.686  |
| 0.100           | -0.502 | -0.447 | -0.393 | -0.334 | -0.282 | -0.229 | -0.171 | -0.116 | -0.057 | 0.055  | 0.148  | 0.255  | 0.358  | 0.440  | 0.533  | 0.580  |
| 0.200           | -0.394 | -0.361 | -0.339 | -0.313 | -0.281 | -0.250 | -0.213 | -0.165 | -0.140 | -0.067 | 0.002  | 0.072  | 0.147  | 0.287  | 0.285  | 0.319  |
| 0.300           | -0.306 | -0.283 | -0.266 | -0.296 | -0.283 | -0.262 | -0.235 | -0.156 | -0.187 | -0.134 | -0.082 | -0.029 | 0.032  | 0.088  | 0.145  | 0.175  |
| 0.400           | -0.252 | -0.241 | -0.229 | -0.212 | -0.205 | -0.193 | -0.176 | -0.157 | -0.144 | -0.112 | -0.076 | -0.038 | 0.007  | 0.049  | 0.095  | 0.118  |
| 0.500           | -0.156 | -0.148 | -0.139 | -0.124 | -0.115 | -0.108 | -0.097 | -0.092 | -0.077 | -0.051 | -0.025 | 0.003  | 0.031  | 0.048  | 0.080  | 0.099  |
| 0.650           | -0.048 | -0.043 | -0.043 | -0.035 | -0.032 | -0.029 | -0.022 | -0.016 | -0.009 | 0.005  | 0.022  | 0.039  | 0.061  | 0.078  | 0.098  | 0.112  |
| 0.750           | 0.019  | 0.022  | 0.021  | 0.027  | 0.029  | 0.030  | 0.035  | 0.039  | 0.043  | 0.054  | 0.065  | 0.080  | 0.096  | 0.110  | 0.119  | 0.129  |
| 0.850           | 0.041  | 0.043  | 0.041  | 0.047  | 0.047  | 0.049  | 0.052  | 0.056  | 0.057  | 0.063  | 0.072  | 0.082  | 0.094  | 0.107  | 0.120  | 0.129  |
| 0.950           | 0.093  | 0.096  | 0.092  | 0.098  | 0.097  | 0.169  | 0.099  | 0.101  | 0.101  | 0.101  | 0.106  | 0.110  | 0.115  | 0.121  | 0.131  | 0.128  |

Table 4 (Contd)

Wing AP/3, inverted attitude

C<sub>p</sub>

V = 250 ft/sec; R = 3.2 x 10<sup>6</sup>

| $\alpha$<br>X/C | 5.15°  | 4.15°  | 3.15°  | 2.1°   | 1.15°  | 0.1°   | -0.9°  | -1.95° | -2.95° | -5.0°  | -7.0°  | -9.05° | -11.05° | -13.1° | -15.1° | -16.1° |
|-----------------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|---------|--------|--------|--------|
| Upper surface   |        |        |        |        |        |        |        |        |        |        |        |        |         |        |        |        |
| 0               | 0.706  | 0.839  | 0.933  | 0.985  | 0.882  | 0.997  | 0.975  | 0.925  | 0.821  | 0.498  | 0.022  | -0.616 | -1.414  | -2.395 | -3.494 | -4.201 |
| 0.005           | -0.615 | -0.385 | -0.175 | 0.008  | 0.197  | 0.347  | 0.497  | 0.623  | 0.738  | 0.902  | 0.992  | 1.013  | 0.985   | 0.898  | 0.750  | 0.644  |
| 0.015           | -0.667 | -0.500 | -0.346 | -0.209 | -0.061 | 0.064  | 0.193  | 0.308  | 0.420  | 0.610  | 0.763  | 0.877  | 0.959   | 1.004  | 1.013  | 1.005  |
| 0.030           | -0.659 | -0.533 | -0.418 | -0.313 | -0.199 | -0.099 | 0.005  | 0.102  | 0.199  | 0.372  | 0.523  | 0.652  | 0.769   | 0.861  | 0.929  | 0.957  |
| 0.050           | -0.604 | -0.512 | -0.423 | -0.343 | -0.255 | -0.175 | -0.090 | -0.011 | 0.071  | 0.220  | 0.354  | 0.477  | 0.593   | 0.695  | 0.781  | 0.820  |
| 0.075           | -0.560 | -0.489 | -0.419 | -0.364 | -0.287 | -0.222 | -0.153 | -0.088 | -0.021 | 0.106  | 0.225  | 0.335  | 0.443   | 0.543  | 0.631  | 0.675  |
| 0.100           | -0.525 | -0.466 | -0.408 | -0.365 | -0.300 | -0.245 | -0.187 | -0.132 | -0.076 | 0.035  | 0.139  | 0.238  | 0.338   | 0.431  | 0.516  | 0.560  |
| 0.200           | -0.447 | -0.415 | -0.373 | -0.346 | -0.312 | -0.279 | -0.243 | -0.208 | -0.171 | -0.099 | -0.029 | 0.043  | 0.118   | 0.190  | 0.260  | 0.297  |
| 0.300           | -0.366 | -0.344 | -0.339 | -0.310 | -0.280 | -0.261 | -0.239 | -0.216 | -0.194 | -0.148 | -0.103 | -0.054 | 0.003   | 0.061  | 0.118  | 0.149  |
| 0.400           | -0.275 | -0.259 | -0.241 | -0.238 | -0.223 | -0.210 | -0.194 | -0.179 | -0.161 | -0.124 | -0.087 | -0.047 | -0.009  | 0.026  | 0.071  | 0.095  |
| 0.500           | -0.209 | -0.201 | -0.191 | -0.187 | -0.184 | -0.170 | -0.159 | -0.151 | -0.137 | -0.111 | -0.085 | -0.055 | -0.018  | 0.014  | 0.050  | 0.068  |
| 0.650           | -      | -      | -      | -      | -      | -      | -      | -      | -      | -      | -      | -      | -       | -      | -      | -      |
| 0.750           | -0.036 | -0.036 | -0.033 | -0.034 | -0.031 | -0.029 | -0.025 | -0.021 | -0.016 | -0.006 | 0.004  | 0.016  | 0.035   | 0.046  | 0.066  | 0.075  |
| 0.850           | 0.009  | 0.008  | 0.007  | 0.005  | 0.006  | 0.005  | 0.005  | 0.006  | 0.006  | 0.007  | 0.006  | 0.006  | 0.009   | 0.007  | 0.006  | 0.008  |
| 0.950           | -      | -      | -      | -      | -      | -      | -      | -      | -      | -      | -      | -      | -       | -      | -      | -      |
| Lower surface   |        |        |        |        |        |        |        |        |        |        |        |        |         |        |        |        |
| 0.005           | -      | -      | -      | -      | -      | -      | -      | -      | -      | -      | -      | -      | -       | -      | -      | -      |
| 0.015           | 0.490  | 0.389  | 0.292  | 0.183  | -0.076 | -0.085 | -0.229 | -0.373 | -0.528 | -0.876 | -1.251 | -1.649 | -2.059  | -2.503 | -2.963 | -3.264 |
| 0.030           | 0.248  | 0.159  | 0.077  | -0.016 | -0.107 | -0.227 | -0.339 | -0.456 | -0.573 | -0.823 | -1.097 | -1.360 | -1.646  | -1.950 | -2.229 | -2.434 |
| 0.050           | -      | -      | -      | -      | -      | -      | -      | -      | -      | -      | -      | -      | -       | -      | -      | -      |
| 0.075           | 0.022  | -0.040 | -0.096 | -0.156 | -0.228 | -0.280 | -0.357 | -0.415 | -0.493 | -0.638 | -0.775 | -0.921 | -1.080  | -1.232 | -1.388 | -1.471 |
| 0.100           | -0.039 | -0.096 | -0.143 | -0.194 | -0.254 | -0.306 | -0.363 | -0.421 | -0.481 | -0.597 | -0.771 | -0.827 | -0.954  | -1.071 | -1.193 | -1.256 |
| 0.200           | -0.124 | -0.146 | -0.192 | -0.227 | -0.263 | -0.297 | -0.311 | -0.343 | -0.375 | -0.437 | -0.506 | -0.567 | -0.627  | -0.689 | -0.747 | -0.780 |
| 0.300           | -0.166 | -0.152 | -0.222 | -0.247 | -0.271 | -0.294 | -0.262 | -0.283 | -0.300 | -0.344 | -0.386 | -0.427 | -0.459  | -0.497 | -0.533 | -0.553 |
| 0.400           | -0.131 | -0.147 | -0.173 | -0.192 | -0.208 | -0.219 | -0.222 | -0.233 | -0.242 | -0.271 | -0.297 | -0.321 | -0.344  | -0.360 | -0.381 | -0.393 |
| 0.500           | -0.090 | -0.088 | -0.114 | -0.103 | -0.105 | -0.122 | -0.139 | -0.148 | -0.156 | -0.173 | -0.189 | -0.205 | -0.213  | -0.228 | -0.242 | -0.252 |
| 0.650           | -0.003 | -0.008 | -0.009 | -0.018 | -0.026 | -0.033 | -0.038 | -0.043 | -0.045 | -0.056 | -0.064 | -0.072 | -0.074  | -0.082 | -0.091 | -0.098 |
| 0.750           | 0.051  | 0.044  | 0.044  | 0.037  | 0.030  | 0.026  | 0.023  | 0.018  | 0.019  | 0.011  | 0.005  | -0.002 | -0.003  | -0.009 | -0.017 | -0.025 |
| 0.850           | 0.058  | 0.053  | 0.051  | 0.046  | 0.042  | 0.040  | 0.038  | 0.036  | 0.037  | 0.033  | 0.028  | 0.026  | 0.026   | 0.022  | 0.018  | 0.011  |
| 0.950           | 0.087  | 0.079  | 0.082  | 0.077  | 0.076  | 0.074  | 0.076  | 0.073  | 0.077  | 0.075  | 0.073  | 0.073  | 0.073   | 0.072  | 0.066  | 0.058  |



Table 5

Wing AP/4, normal attitude

$C_p$

$V = 250 \text{ ft/sec}, R = 3.2 \times 10^6$

| $\alpha$<br>X/C | $-5.75^\circ$ | $-3.75^\circ$ | $-2.75^\circ$ | $-1.75^\circ$ | $-0.75^\circ$ | $0.3^\circ$ | $1.3^\circ$ | $2.3^\circ$ | $3.3^\circ$ | $4.3^\circ$ | $6.35^\circ$ | $10.35^\circ$ | $14.4^\circ$ | $18.4^\circ$ | $20.45^\circ$ | $21.45^\circ$ |
|-----------------|---------------|---------------|---------------|---------------|---------------|-------------|-------------|-------------|-------------|-------------|--------------|---------------|--------------|--------------|---------------|---------------|
| Upper Surface   |               |               |               |               |               |             |             |             |             |             |              |               |              |              |               |               |
| 0               | 0.583         | 0.833         | 0.915         | 0.971         | 1.002         | 1.011       | 1.007       | 0.980       | 0.927       | 0.849       | 0.614        | -0.185        | -1.387       | -3.032       | -4.029        | -4.566        |
| 0.005           | 0.817         | 0.732         | 0.642         | 0.539         | 0.418         | 0.285       | 0.144       | -0.009      | -0.179      | -0.358      | -0.757       | -1.713        | -3.022       | -4.702       | -4.810        | -5.161        |
| 0.015           | 0.581         | 0.419         | 0.329         | 0.234         | 0.129         | 0.019       | -0.094      | -0.217      | -0.342      | -0.472      | -0.754       | -1.386        | -1.936       | -2.714       | -3.131        | -3.335        |
| 0.030           | 0.342         | 0.199         | 0.120         | 0.044         | -0.044        | -0.133      | -0.220      | -0.312      | -0.410      | -0.506      | -0.713       | -1.151        | -1.535       | -2.207       | -2.288        | -2.414        |
| 0.050           | 0.193         | 0.071         | 0.006         | -0.056        | -0.125        | -0.197      | -0.264      | -0.334      | -0.408      | -0.480      | -0.632       | -0.889        | -1.210       | -1.546       | -1.725        | -1.814        |
| 0.075           | 0.084         | -0.017        | -0.070        | -0.120        | -0.179        | -0.233      | -0.286      | -0.341      | -0.398      | -0.453      | -0.571       | -0.775        | -1.004       | -1.242       | -1.371        | -1.436        |
| 0.100           | 0.017         | -0.069        | -0.114        | -0.155        | -0.203        | -0.248      | -0.293      | -0.339      | -0.383      | -0.427      | -0.517       | -0.694        | -0.869       | -1.049       | -1.145        | -1.195        |
| 0.200           | -0.106        | -0.159        | -0.187        | -0.212        | -0.239        | -0.265      | -0.291      | -0.314      | -0.340      | -0.357      | -0.403       | -0.496        | -0.577       | -0.662       | -0.709        | -0.740        |
| 0.300           | -0.168        | -0.202        | -0.222        | -0.236        | -0.256        | -0.270      | -0.286      | -0.302      | -0.310      | -0.298      | -0.327       | -0.378        | -0.417       | -0.459       | -0.527        | -0.502        |
| 0.400           | -0.141        | -0.164        | -0.179        | -0.187        | -0.201        | -0.212      | -0.223      | -0.205      | -0.203      | -0.212      | -0.233       | -0.264        | -0.282       | -0.310       | -0.333        | -0.341        |
| 0.500           | -0.108        | -0.125        | -0.135        | -0.142        | -0.131        | -0.126      | -0.135      | -0.142      | -0.148      | -0.152      | -0.165       | -0.180        | -0.189       | -0.206       | -0.228        | -0.234        |
| 0.650           | -             | -             | -             | -             | -             | -           | -           | -           | -           | -           | -            | -             | -            | -            | -             | -             |
| 0.750           | 0.005         | 0             | -0.002        | -0.002        | -0.006        | -0.005      | -0.006      | -0.006      | -0.006      | -0.006      | -0.009       | -0.011        | -0.014       | -0.028       | -0.048        | -0.054        |
| 0.850           | 0.036         | 0.035         | 0.033         | 0.036         | 0.034         | 0.037       | 0.036       | 0.036       | 0.037       | 0.037       | 0.037        | 0.037         | 0.038        | 0.027        | 0.009         | 0.005         |
| 0.950           | -             | -             | -             | -             | -             | -           | -           | -           | -           | -           | -            | -             | -            | -            | -             | -             |
| Lower Surface   |               |               |               |               |               |             |             |             |             |             |              |               |              |              |               |               |
| 0.005           | -0.808        | -0.385        | -0.199        | -0.023        | 0.139         | 0.291       | 0.420       | 0.541       | 0.646       | 0.738       | 0.878        | 1.010         | 0.958        | 0.721        | 0.520         | 0.411         |
| 0.015           | -0.799        | -0.511        | -0.378        | -0.247        | -0.125        | -0.005      | 0.103       | 0.209       | 0.308       | 0.401       | 0.565        | 0.826         | 0.975        | 1.014        | 0.996         | 0.974         |
| 0.030           | -0.766        | -0.556        | -0.457        | -0.359        | -0.265        | -0.170      | -0.084      | 0.004       | 0.085       | 0.167       | 0.314        | 0.581         | 0.789        | 0.930        | 0.975         | 0.990         |
| 0.050           | -             | -             | -             | -             | -             | -           | -           | -           | -           | -           | -            | -             | -            | -            | -             | -             |
| 0.075           | -0.573        | -0.476        | -0.420        | -0.361        | -0.308        | -0.251      | -0.199      | -0.143      | -0.088      | -0.035      | 0.066        | 0.270         | 0.460        | 0.626        | 0.700         | 0.732         |
| 0.100           | -0.536        | -0.444        | -0.407        | -0.361        | -0.315        | -0.268      | -0.227      | -0.178      | -0.135      | -0.088      | -0.001       | 0.180         | 0.356        | 0.512        | 0.587         | 0.621         |
| 0.200           | -0.392        | -0.350        | -0.327        | -0.316        | -0.293        | -0.267      | -0.242      | -0.216      | -0.191      | -0.156      | -0.108       | 0.013         | 0.141        | 0.266        | 0.328         | 0.356         |
| 0.300           | -0.323        | -0.294        | -0.283        | -0.268        | -0.284        | -0.269      | -0.256      | -0.238      | -0.220      | -0.182      | -0.167       | -0.079        | 0.024        | 0.126        | 0.178         | 0.204         |
| 0.400           | -0.233        | -0.217        | -0.210        | -0.201        | -0.207        | -0.206      | -0.197      | -0.185      | -0.173      | -0.150      | -0.138       | -0.075        | 0.005        | 0.015        | 0.127         | 0.147         |
| 0.500           | -0.153        | -0.144        | -0.140        | -0.134        | -0.128        | -0.119      | -0.114      | -0.120      | -0.125      | -0.106      | -0.101       | -0.055        | 0.007        | 0.003        | 0.107         | 0.123         |
| 0.650           | -0.039        | -0.034        | -0.034        | -0.030        | -0.030        | -0.027      | -0.025      | -0.021      | -0.022      | -0.020      | -0.005       | 0.009         | 0.048        | 0.096        | 0.121         | 0.132         |
| 0.750           | 0.022         | 0.026         | 0.026         | 0.029         | 0.026         | 0.029       | 0.029       | 0.032       | 0.032       | 0.032       | 0.040        | 0.063         | 0.089        | 0.118        | 0.138         | 0.146         |
| 0.850           | 0.042         | 0.044         | 0.044         | 0.045         | 0.044         | 0.044       | 0.044       | 0.045       | 0.045       | 0.045       | 0.047        | 0.048         | 0.062        | 0.092        | 0.118         | 0.137         |
| 0.950           | 0.093         | 0.093         | 0.091         | 0.093         | 0.090         | 0.092       | 0.091       | 0.091       | 0.090       | 0.091       | 0.087        | 0.092         | 0.107        | 0.119        | 0.114         | 0.115         |

Table 5-(Contd)-

Wing AP/4, Inverted attitude

C<sub>p</sub>

V = 250 ft/sec; R = 3.2 x 10<sup>6</sup>

| $\alpha$<br>X/C | 6.85°  | 4.85°  | 3.85°  | 2.85°  | 1.85°  | 0.85°  | -0.2°  | -1.2°  | -2.2°  | -3.2°  | -5.2°  | -9.25° | -13.3° | -17.3° | -19.35° | -21.35° | -23.35° | -24.4° | -25.4° |
|-----------------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|---------|---------|---------|--------|--------|
| Upper surface   |        |        |        |        |        |        |        |        |        |        |        |        |        |        |         |         |         |        |        |
| 0               | 0.547  | 0.813  | 0.902  | 0.962  | 1.000  | 1.011  | 1.008  | 0.988  | 0.938  | 0.863  | 0.633  | -0.194 | -1.514 | -3.342 | -4.448  | -5.634  | -7.033  | -7.608 | -5.754 |
| 0.005           | -0.853 | -0.427 | -0.243 | -0.080 | 0.083  | 0.237  | 0.379  | 0.489  | 0.602  | 0.702  | 0.856  | 1.008  | 0.977  | 0.774  | 0.594   | 0.371   | 0.098   | -0.014 | -0.174 |
| 0.015           | -0.817 | -0.524 | -0.390 | -0.270 | -0.146 | -0.023 | 0.093  | 0.187  | 0.293  | 0.388  | 0.556  | 0.816  | 0.967  | 1.012  | 0.997   | 0.955   | 0.884   | 0.846  | 0.799  |
| 0.030           | -0.760 | -0.546 | -0.446 | -0.358 | -0.262 | -0.168 | -0.075 | 0.004  | 0.089  | 0.169  | 0.320  | 0.581  | 0.783  | 0.922  | 0.967   | 0.998   | 1.011   | 1.011  | 1.010  |
| 0.050           | -0.667 | -0.512 | -0.438 | -0.371 | -0.297 | -0.225 | -0.151 | -0.091 | -0.022 | 0.045  | 0.173  | 0.405  | 0.607  | 0.839  | 0.835   | 0.893   | 0.940   | 0.955  | 0.971  |
| 0.075           | -0.596 | -0.479 | -0.423 | -0.371 | -0.315 | -0.256 | -0.198 | -0.149 | -0.094 | -0.040 | 0.067  | 0.269  | 0.455  | 0.618  | 0.689   | 0.758   | 0.817   | 0.842  | 0.866  |
| 0.100           | -0.535 | -0.449 | -0.403 | -0.362 | -0.317 | -0.269 | -0.222 | -0.175 | -0.134 | -0.089 | 0.001  | 0.179  | 0.348  | 0.504  | 0.575   | 0.715   | 0.710   | 0.737  | 0.763  |
| 0.200           | -0.413 | -0.371 | -0.354 | -0.333 | -0.307 | -0.280 | -0.253 | -0.229 | -0.204 | -0.175 | -0.118 | 0.001  | 0.109  | 0.248  | 0.311   | 0.373   | 0.434   | 0.463  | 0.489  |
| 0.300           | -0.333 | -0.307 | -0.295 | -0.312 | -0.299 | -0.284 | -0.265 | -0.252 | -0.235 | -0.217 | -0.176 | -0.090 | 0.004  | 0.104  | 0.158   | 0.204   | 0.253   | 0.295  | 0.318  |
| 0.400           | -0.236 | -0.223 | -0.212 | -0.204 | -0.233 | -0.220 | -0.210 | -0.199 | -0.190 | -0.176 | -0.149 | -0.088 | -0.019 | 0.060  | 0.105   | 0.148   | 0.196   | 0.219  | 0.239  |
| 0.500           | -0.164 | -0.160 | -0.084 | -0.149 | -0.142 | -0.133 | -0.132 | -0.148 | -0.146 | -0.135 | -0.116 | -0.071 | -0.019 | 0.044  | 0.082   | 0.118   | 0.158   | 0.180  | 0.194  |
| 0.650           | -      | -      | -      | -      | -      | -      | -      | -      | -      | -      | -      | -      | -      | -      | -       | -       | -       | -      | -      |
| 0.750           | -0.001 | -0.005 | -0.005 | -0.006 | -0.006 | -0.007 | -0.008 | -0.007 | -0.007 | -0.005 | 0.001  | 0.023  | 0.031  | 0.066  | 0.089   | 0.112   | 0.136   | 0.151  | 0.157  |
| 0.850           | 0.046  | 0.042  | 0.041  | 0.038  | 0.037  | 0.035  | 0.031  | 0.031  | 0.029  | 0.030  | 0.032  | 0.042  | 0.058  | 0.075  | 0.091   | 0.107   | 0.124   | 0.135  | 0.136  |
| 0.950           | -      | -      | -      | -      | -      | -      | -      | -      | -      | -      | -      | -      | -      | -      | -       | -       | -       | -      | -      |
| Lower surface   |        |        |        |        |        |        |        |        |        |        |        |        |        |        |         |         |         |        |        |
| 0.005           | 0.904  | 0.766  | 0.677  | 0.585  | 0.469  | 0.336  | 0.187  | 0.044  | -0.133 | -0.318 | -0.729 | -1.718 | -4.100 | -4.576 | -4.939  | -5.148  | -5.942  | -6.242 | -6.591 |
| 0.015           | 0.601  | 0.432  | 0.338  | 0.251  | 0.144  | 0.033  | -0.088 | -0.198 | -0.331 | -0.463 | -0.745 | -1.388 | -1.940 | -2.841 | -3.243  | -3.638  | -4.094  | -4.244 | -4.379 |
| 0.030           | 0.349  | 0.193  | 0.113  | 0.037  | -0.050 | -0.141 | -0.235 | -0.321 | -0.422 | -0.520 | -0.727 | -1.204 | -1.605 | -2.137 | -2.374  | -2.608  | -2.890  | -2.969 | -3.022 |
| 0.050           | -      | -      | -      | -      | -      | -      | -      | -      | -      | -      | -      | -      | -      | -      | -       | -       | -       | -      | -      |
| 0.075           | 0.093  | -0.016 | -0.071 | -0.120 | -0.176 | -0.233 | -0.289 | -0.340 | -0.398 | -0.453 | -0.552 | -0.785 | -1.014 | -1.257 | -1.376  | -1.471  | -1.617  | -1.656 | -1.688 |
| 0.100           | 0.022  | -0.071 | -0.118 | -0.162 | -0.206 | -0.255 | -0.303 | -0.344 | -0.390 | -0.426 | -0.517 | -0.698 | -0.876 | -1.062 | -1.149  | -1.215  | -1.333  | -1.365 | -1.406 |
| 0.200           | -0.090 | -0.142 | -0.176 | -0.205 | -0.230 | -0.257 | -0.284 | -0.305 | -0.320 | -0.340 | -0.382 | -0.479 | -0.561 | -0.647 | -0.683  | -0.702  | -0.773  | -0.795 | -0.827 |
| 0.300           | -0.151 | -0.177 | -0.189 | -0.229 | -0.247 | -0.264 | -0.280 | -0.283 | -0.276 | -0.290 | -0.316 | -0.370 | -0.416 | -0.464 | -0.485  | -0.510  | -0.531  | -0.533 | -0.551 |
| 0.400           | -0.126 | -0.145 | -0.155 | -0.173 | -0.191 | -0.202 | -0.214 | -0.198 | -0.207 | -0.212 | -0.227 | -0.260 | -0.282 | -0.312 | -0.328  | -0.354  | -0.363  | -0.366 | -0.383 |
| 0.500           | -0.091 | -0.102 | -0.108 | -0.119 | -0.113 | -0.119 | -0.124 | -0.133 | -0.138 | -0.140 | -0.148 | -0.167 | -0.180 | -0.204 | -0.215  | -0.233  | -0.249  | -0.253 | -0.269 |
| 0.650           | 0.004  | -0.017 | -0.022 | -0.023 | -0.027 | -0.028 | -0.030 | -0.033 | -0.035 | -0.034 | -0.038 | -0.047 | -0.054 | -0.077 | -0.090  | -0.107  | -0.127  | -0.131 | -0.147 |
| 0.750           | 0.047  | 0.034  | 0.030  | 0.029  | 0.029  | 0.026  | 0.025  | 0.024  | 0.023  | 0.024  | 0.023  | 0.014  | 0.007  | -0.016 | -0.030  | -0.045  | -0.064  | -0.068 | -0.085 |
| 0.850           | 0.056  | 0.049  | 0.046  | 0.044  | 0.044  | 0.043  | 0.042  | 0.043  | 0.042  | 0.042  | 0.041  | 0.037  | 0.031  | 0.015  | 0.005   | -0.006  | -0.019  | -0.022 | -0.036 |
| 0.950           | 0.103  | 0.101  | 0.100  | 0.098  | 0.099  | 0.098  | 0.096  | 0.096  | 0.095  | 0.096  | 0.096  | 0.094  | 0.085  | 0.072  | 0.061   | 0.052   | 0.039   | 0.035  | 0.016  |





Table 6

Wing AP/5, normal attitude

C<sub>p</sub>

V = 250 ft/sec; R = 3.2 x 10<sup>6</sup>

| α<br>X/C | Upper surface |        |        |        |        |        |        |        |        |        |        |        | Lower surface |        |        |        |        |        |  |  |  |  |  |  |
|----------|---------------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|---------------|--------|--------|--------|--------|--------|--|--|--|--|--|--|
|          | -6.2°         | -4.2°  | -3.2°  | -2.2°  | -1.2°  | -0.2°  | 0.8°   | 1.8°   | 2.8°   | 3.8°   | 5.8°   | 7.85°  | 9.85°         | 13.85° | 17.85° | 21.85° | 23.9°  | 25.9°  |  |  |  |  |  |  |
| 0        | 0.784         | 0.915  | 0.958  | 0.990  | 1.005  | 1.009  | 1.009  | 0.997  | 0.974  | 0.933  | 0.808  | 0.635  | 0.400         | -0.235 | -1.108 | -2.163 | -2.755 | -3.431 |  |  |  |  |  |  |
| 0.005    | 0.772         | 0.843  | 0.869  | 0.880  | 0.897  | 0.900  | 0.905  | 0.884  | -0.023 | -0.148 | -0.412 | -0.689 | -0.994        | -1.677 | -2.619 | -3.884 | -3.956 | -4.084 |  |  |  |  |  |  |
| 0.015    | 0.470         | 0.343  | 0.276  | 0.197  | 0.129  | 0.050  | -0.028 | -0.118 | -0.198 | -0.288 | -0.476 | -0.664 | -0.866        | -1.202 | -1.637 | -2.084 | -2.275 | -2.518 |  |  |  |  |  |  |
| 0.030    | 0.239         | 0.137  | 0.077  | 0.013  | -0.039 | -0.102 | -0.160 | -0.230 | -0.288 | -0.354 | -0.490 | -0.621 | -0.761        | -0.980 | -1.251 | -1.528 | -1.642 | -1.768 |  |  |  |  |  |  |
| 0.050    | 0.110         | 0.021  | -0.022 | -0.073 | -0.113 | -0.159 | -0.203 | -0.255 | -0.297 | -0.345 | -0.442 | -0.533 | -0.610        | -0.769 | -0.953 | -1.120 | -1.203 | -1.283 |  |  |  |  |  |  |
| 0.075    | 0.021         | -0.050 | -0.083 | -0.122 | -0.152 | -0.188 | -0.221 | -0.260 | -0.292 | -0.326 | -0.396 | -0.458 | -0.497        | -0.628 | -0.748 | -0.854 | -0.907 | -0.956 |  |  |  |  |  |  |
| 0.100    | -0.029        | -0.087 | -0.114 | -0.146 | -0.171 | -0.198 | -0.224 | -0.255 | -0.279 | -0.306 | -0.361 | -0.401 | -0.447        | -0.537 | -0.618 | -0.688 | -0.723 | -0.755 |  |  |  |  |  |  |
| 0.200    | -0.113        | -0.147 | -0.162 | -0.179 | -0.190 | -0.204 | -0.216 | -0.231 | -0.240 | -0.253 | -0.276 | -0.292 | -0.310        | -0.339 | -0.367 | -0.390 | -0.407 | -0.428 |  |  |  |  |  |  |
| 0.300    | -0.132        | -0.153 | -0.162 | -0.171 | -0.177 | -0.183 | -0.189 | -0.196 | -0.207 | -0.203 | -0.214 | -0.223 | -0.226        | -0.238 | -0.256 | -0.279 | -0.296 | -0.323 |  |  |  |  |  |  |
| 0.400    | -0.111        | -0.125 | -0.129 | -0.135 | -0.136 | -0.139 | -0.140 | -0.141 | -0.140 | -0.139 | -0.144 | -0.144 | -0.146        | -0.153 | -0.175 | -0.209 | -0.234 | -0.265 |  |  |  |  |  |  |
| 0.500    | -0.087        | -0.095 | -0.098 | -0.101 | -0.100 | -0.104 | -0.097 | -0.095 | -0.094 | -0.093 | -0.092 | -0.090 | -0.091        | -0.101 | -0.132 | -0.175 | -0.206 | -0.242 |  |  |  |  |  |  |
| 0.650    | -             | -      | -      | -      | -      | -      | -      | -      | -      | -      | -      | -      | -             | -      | -      | -      | -      | -      |  |  |  |  |  |  |
| 0.750    | 0.001         | -0.001 | 0      | -0.001 | 0.003  | 0.005  | 0.008  | 0.012  | 0.015  | 0.018  | 0.016  | 0.014  | 0.008         | -0.018 | -0.067 | -0.126 | -0.152 | -0.213 |  |  |  |  |  |  |
| 0.850    | 0.030         | 0.030  | 0.030  | 0.030  | 0.035  | 0.038  | 0.042  | 0.045  | 0.048  | 0.048  | 0.046  | 0.044  | 0.037         | 0.011  | -0.033 | -0.089 | -0.126 | -0.167 |  |  |  |  |  |  |
| 0.950    | -             | -      | -      | -      | -      | -      | -      | -      | -      | -      | -      | -      | -             | -      | -      | -      | -      | -      |  |  |  |  |  |  |
| 0.005    | -0.447        | -0.181 | -0.061 | 0.069  | 0.176  | 0.283  | 0.380  | 0.478  | 0.558  | 0.637  | 0.773  | 0.870  | 0.946         | 1.012  | 0.980  | 0.845  | 0.736  | 0.598  |  |  |  |  |  |  |
| 0.015    | -0.521        | -0.340 | -0.253 | -0.159 | -0.078 | 0.005  | 0.083  | 0.165  | 0.236  | 0.309  | 0.444  | 0.561  | 0.669         | 0.847  | 0.956  | 1.007  | 1.002  | 0.999  |  |  |  |  |  |  |
| 0.030    | -0.536        | -0.408 | -0.346 | -0.277 | -0.215 | -0.152 | -0.092 | -0.027 | 0.050  | 0.091  | 0.205  | 0.311  | 0.413         | 0.602  | 0.755  | 0.875  | 0.923  | 0.959  |  |  |  |  |  |  |
| 0.050    | -             | -      | -      | -      | -      | -      | -      | -      | -      | -      | -      | -      | -             | -      | -      | -      | -      | -      |  |  |  |  |  |  |
| 0.075    | -0.408        | -0.344 | -0.318 | -0.283 | -0.249 | -0.215 | -0.179 | -0.144 | -0.109 | -0.073 | 0      | 0.071  | 0.141         | 0.287  | 0.424  | 0.556  | 0.616  | 0.674  |  |  |  |  |  |  |
| 0.100    | -0.373        | -0.326 | -0.302 | -0.280 | -0.252 | -0.225 | -0.197 | -0.168 | -0.140 | -0.110 | -0.049 | 0.010  | 0.073         | 0.200  | 0.326  | 0.450  | 0.510  | 0.566  |  |  |  |  |  |  |
| 0.200    | -0.264        | -0.253 | -0.243 | -0.236 | -0.224 | -0.213 | -0.198 | -0.184 | -0.169 | -0.154 | -0.119 | -0.084 | -0.044        | 0.041  | 0.132  | 0.231  | 0.282  | 0.330  |  |  |  |  |  |  |
| 0.300    | -0.208        | -0.204 | -0.201 | -0.198 | -0.220 | -0.215 | -0.208 | -0.201 | -0.194 | -0.183 | -0.161 | -0.136 | -0.108        | -0.044 | 0.032  | 0.115  | 0.157  | 0.202  |  |  |  |  |  |  |
| 0.400    | -0.144        | -0.144 | -0.145 | -0.145 | -0.147 | -0.162 | -0.157 | -0.154 | -0.150 | -0.144 | -0.130 | -0.120 | -0.094        | -0.045 | 0.014  | 0.084  | 0.120  | 0.158  |  |  |  |  |  |  |
| 0.500    | -0.082        | -0.086 | -0.088 | -0.090 | -0.087 | -0.086 | -0.082 | -0.094 | -0.108 | -0.113 | -0.096 | -0.082 | -0.069        | -0.030 | 0.020  | 0.080  | 0.112  | 0.148  |  |  |  |  |  |  |
| 0.650    | -0.004        | -0.007 | -0.009 | -0.012 | -0.013 | -0.015 | -0.016 | -0.018 | -0.017 | -0.016 | -0.12  | -0.003 | 0.009         | 0.029  | 0.060  | 0.112  | 0.139  | 0.168  |  |  |  |  |  |  |
| 0.750    | 0.033         | 0.033  | 0.031  | 0.028  | 0.027  | 0.026  | 0.025  | 0.023  | 0.024  | 0.023  | 0.027  | 0.034  | 0.044         | 0.072  | 0.108  | 0.148  | 0.162  | 0.187  |  |  |  |  |  |  |
| 0.850    | 0.038         | 0.037  | 0.035  | 0.033  | 0.034  | 0.030  | 0.030  | 0.028  | 0.027  | 0.028  | 0.031  | 0.037  | 0.044         | 0.069  | 0.097  | 0.136  | 0.156  | 0.179  |  |  |  |  |  |  |
| 0.950    | 0.082         | 0.084  | 0.084  | 0.082  | 0.083  | 0.080  | 0.079  | 0.076  | 0.074  | 0.072  | 0.071  | 0.073  | 0.073         | 0.084  | 0.097  | 0.116  | 0.127  | 0.141  |  |  |  |  |  |  |

Table 6 (Contd)

Wing AP/5, Inverted attitude

 $C_p$  $V = 250 \text{ ft/sec}; R = 3.2 \times 10^6$ 

| $\alpha$<br>X/C | 6.5°   | 4.5°   | 3.5°   | 2.5°   | 1.5°   | 0.5°   | -0.5°  | -1.5°  | -2.5°  | -3.5°  | -5.5°  | -7.55° | -9.55° | -13.55° | -17.55° | -21.55° | -25.6° | -29.6° | -30.9° |
|-----------------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|---------|---------|---------|--------|--------|--------|
| Upper surface   |        |        |        |        |        |        |        |        |        |        |        |        |        |         |         |         |        |        |        |
| 0               | 0.785  | 0.872  | 0.961  | 0.992  | 1.008  | 1.010  | 1.009  | 0.997  | 0.971  | 0.933  | 0.810  | 0.621  | 0.386  | -0.315  | -1.235  | -2.421  | -3.877 | -5.488 | -5.997 |
| 0.005           | -0.444 | -0.185 | -0.063 | 0.052  | 0.169  | 0.269  | 0.367  | 0.456  | 0.541  | 0.617  | 0.751  | 0.862  | 0.937  | 1.010   | 0.988   | 0.878   | 0.657  | 0.343  | 0.229  |
| 0.015           | -0.501 | -0.313 | -0.230 | -0.145 | -0.055 | 0.024  | 0.102  | 0.176  | 0.249  | 0.319  | 0.448  | 0.569  | 0.667  | 0.839   | 0.950   | 1.006   | 1.003  | 0.941  | 0.911  |
| 0.030           | -0.507 | -0.369 | -0.314 | -0.251 | -0.184 | -0.123 | -0.063 | -0.004 | 0.054  | 0.110  | 0.220  | 0.329  | 0.423  | 0.606   | 0.755   | 0.873   | 0.958  | 1.003  | 1.008  |
| 0.050           | -0.454 | -0.354 | -0.317 | -0.272 | -0.222 | -0.178 | -0.130 | -0.088 | -0.040 | 0.005  | 0.094  | 0.183  | 0.264  | 0.431   | 0.613   | 0.710   | 0.822  | 0.908  | 0.929  |
| 0.075           | -0.405 | -0.335 | -0.308 | -0.273 | -0.237 | -0.203 | -0.168 | -0.137 | -0.099 | -0.063 | 0.007  | 0.082  | 0.149  | 0.293   | 0.429   | 0.559   | 0.679  | 0.780  | 0.808  |
| 0.100           | -0.370 | -0.313 | -0.293 | -0.266 | -0.238 | -0.211 | -0.184 | -0.159 | -0.129 | -0.100 | -0.042 | 0.020  | 0.079  | 0.205   | 0.327   | 0.449   | 0.568  | 0.674  | 0.705  |
| 0.200           | -0.279 | -0.258 | -0.249 | -0.239 | -0.226 | -0.213 | -0.200 | -0.188 | -0.172 | -0.156 | -0.123 | -0.086 | -0.049 | 0.037   | 0.128   | 0.227   | 0.329  | 0.431  | 0.459  |
| 0.300           | -0.219 | -0.211 | -0.209 | -0.198 | -0.200 | -0.193 | -0.187 | -0.182 | -0.173 | -0.164 | -0.143 | -0.117 | -0.093 | -0.036  | 0.028   | 0.103   | 0.195  | 0.290  | 0.317  |
| 0.400           | -0.147 | -0.162 | -0.146 | -0.147 | -0.147 | -0.145 | -0.144 | -0.145 | -0.140 | -0.134 | -0.122 | -0.104 | -0.085 | -0.038  | 0.018   | 0.086   | 0.157  | 0.234  | 0.261  |
| 0.500           | -0.094 | -0.099 | -0.098 | -0.101 | -0.102 | -0.103 | -0.104 | -0.109 | -0.105 | -0.104 | -0.096 | -0.086 | -0.075 | -0.034  | 0.013   | 0.072   | 0.142  | 0.217  | 0.240  |
| 0.650           | -      | -      | -      | -      | -      | -      | -      | -      | -      | -      | -      | -      | -      | -       | -       | -       | -      | -      | -      |
| 0.750           | 0.014  | 0.010  | 0.011  | 0.008  | 0.005  | 0.001  | -0.002 | -0.007 | -0.008 | -0.008 | -0.008 | -0.003 | 0.004  | 0.026   | 0.057   | 0.098   | 0.152  | 0.213  | 0.252  |
| 0.850           | 0.048  | 0.039  | 0.044  | 0.042  | 0.037  | 0.035  | 0.030  | 0.025  | 0.023  | 0.022  | 0.020  | 0.021  | 0.025  | 0.043   | 0.065   | 0.094   | 0.139  | 0.191  | 0.208  |
| 0.950           | -      | -      | -      | -      | -      | -      | -      | -      | -      | -      | -      | -      | -      | -       | -       | -       | -      | -      | -      |
| Lower surface   |        |        |        |        |        |        |        |        |        |        |        |        |        |         |         |         |        |        |        |
| 0.005           | 0.792  | 0.626  | 0.595  | 0.516  | 0.420  | 0.329  | 0.224  | 0.115  | -0.001 | -0.120 | -0.385 | -0.691 | -0.989 | -1.709  | -2.454  | -3.439  | -4.117 | -4.578 | -4.799 |
| 0.015           | 0.461  | 0.308  | 0.261  | 0.189  | 0.108  | 0.034  | -0.050 | -0.132 | -0.218 | -0.303 | -0.487 | -0.686 | -0.877 | -1.302  | -1.601  | -2.133  | -2.648 | -3.054 | -3.151 |
| 0.030           | 0.221  | 0.093  | 0.051  | -0.007 | -0.072 | -0.130 | -0.193 | -0.257 | -0.319 | -0.381 | -0.513 | -0.651 | -0.780 | -1.064  | -1.299  | -1.595  | -1.871 | -2.067 | -2.086 |
| 0.050           | -      | -      | -      | -      | -      | -      | -      | -      | -      | -      | -      | -      | -      | -       | -       | -       | -      | -      | -      |
| 0.075           | 0.012  | -0.074 | -0.095 | -0.130 | -0.168 | -0.200 | -0.236 | -0.272 | -0.301 | -0.329 | -0.397 | -0.463 | -0.517 | -0.642  | -0.760  | -0.866  | -0.965 | -1.033 | -1.024 |
| 0.100           | -0.039 | -0.103 | -0.129 | -0.157 | -0.187 | -0.214 | -0.241 | -0.269 | -0.289 | -0.313 | -0.363 | -0.409 | -0.447 | -0.540  | -0.623  | -0.694  | -0.760 | -0.813 | -0.836 |
| 0.200           | -0.112 | -0.148 | -0.163 | -0.177 | -0.193 | -0.206 | -0.219 | -0.232 | -0.235 | -0.243 | -0.261 | -0.279 | -0.293 | -0.323  | -0.354  | -0.376  | -0.408 | -0.455 | -0.492 |
| 0.300           | -0.154 | -0.176 | -0.189 | -0.197 | -0.206 | -0.211 | -0.219 | -0.202 | -0.199 | -0.200 | -0.206 | -0.212 | -0.217 | -0.228  | -0.246  | -0.265  | -0.339 | -0.352 | -0.368 |
| 0.400           | -0.123 | -0.143 | -0.145 | -0.150 | -0.155 | -0.158 | -0.160 | -0.145 | -0.145 | -0.144 | -0.144 | -0.144 | -0.143 | -0.148  | -0.166  | -0.194  | -0.242 | -0.299 | -0.317 |
| 0.500           | -0.089 | -0.103 | -0.106 | -0.097 | -0.083 | -0.084 | -0.087 | -0.091 | -0.088 | -0.085 | -0.083 | -0.095 | -0.080 | -0.088  | -0.117  | -0.155  | -0.211 | -0.283 | -0.298 |
| 0.650           | -0.005 | -0.023 | -0.015 | -0.017 | -0.017 | -0.015 | -0.013 | -0.013 | -0.009 | -0.008 | -0.006 | -0.005 | -0.007 | -0.026  | -0.064  | -0.109  | -0.171 | -0.252 | -0.278 |
| 0.750           | 0.033  | 0.021  | 0.026  | 0.026  | 0.025  | 0.027  | 0.028  | 0.028  | 0.030  | 0.033  | 0.032  | 0.031  | 0.027  | 0.005   | -0.032  | -0.070  | -0.127 | -0.198 | -0.220 |
| 0.850           | 0.040  | 0.029  | 0.035  | 0.033  | 0.033  | 0.035  | 0.037  | 0.037  | 0.038  | 0.042  | 0.039  | 0.037  | 0.037  | 0.032   | 0.014   | -0.019  | -0.048 | -0.081 | -0.130 |
| 0.950           | 0.084  | 0.075  | 0.082  | 0.082  | 0.083  | 0.084  | 0.087  | 0.087  | 0.088  | 0.089  | 0.085  | 0.080  | 0.074  | 0.058   | 0.022   | 0.001   | -0.020 | -0.036 | -0.037 |



Table 7  
LOCAL FORCE AND MOMENT COEFFICIENTS FROM INTEGRATED  
PRESSURE MEASUREMENTS

Wing AP/1

 $V = 125 \text{ ft/sec}, R = 1.6 \times 10^6$ 

| $\alpha$          | $C_N$  | $C_T$   | $C_L$  | $C_D$   | $C_m$  |
|-------------------|--------|---------|--------|---------|--------|
| Normal attitude   |        |         |        |         |        |
| - 4.35°           | -0.321 | -0.0159 | -0.321 | 0.0105  | -0.010 |
| - 2.2°            | -0.179 | -0.0059 | -0.179 | 0.0083  | -0.002 |
| - 1.1°            | -0.082 | -0.0012 | -0.082 | 0.0008  | -0.004 |
| 0°                | 0.011  | 0.0014  | 0.011  | 0.0013  | -0.005 |
| 1.1°              | 0.094  | -0.0015 | 0.094  | -0.0003 | -0.005 |
| 2.2°              | 0.165  | -0.0042 | 0.165  | 0.0011  | -0.002 |
| 4.35°             | 0.323  | -0.0154 | 0.323  | 0.0070  | 0.002  |
| 6.5°              | 0.461  | -0.0347 | 0.462  | 0.0150  | 0.006  |
| 8.7°              | 0.643  | -0.0621 | 0.645  | 0.0320  | 0.003  |
| 10.9°             | 0.797  | -0.0979 | 0.802  | 0.0495  | 0.010  |
| 13.0°             | 0.920  | -0.1431 | 0.929  | 0.0621  | 0.016  |
| 13.25°            | 0.929  | -0.1501 | 0.939  | 0.0608  | 0.013  |
| 15.0°             | 0.717  | 0.0271  | 0.687  | 0.2074  | -0.089 |
| 15.9°             | 0.611  | 0.0374  | 0.579  | 0.1994  |        |
| Inverted attitude |        |         |        |         |        |
| 4.7°              | 0.349  | -0.0167 | 0.349  | 0.0098  | -0.002 |
| 2.5°              | 0.196  | -0.0052 | 0.196  | 0.0022  | -0.005 |
| 1.45°             | 0.116  | -0.0003 | 0.116  | 0.0019  | -0.008 |
| 0.35°             | 0.023  | 0.0034  | 0.023  | 0.0003  | -0.006 |
| - 0.75°           | -0.060 | -0.0011 | -0.060 | 0.0002  | -0.009 |
| - 1.85°           | -0.149 | -0.0034 | -0.149 | 0.0024  | -0.009 |
| - 4.0°            | -0.298 | -0.0158 | -0.298 | 0.0071  | -0.014 |
| - 6.2°            | -0.463 | -0.0360 | -0.463 | 0.0171  | -0.013 |
| - 8.4°            | -0.630 | -0.0645 | -0.633 | 0.0321  | -0.012 |
| -10.55°           | -0.793 | -0.0972 | -0.797 | 0.0550  | -0.014 |
| -11.65°           | -0.871 | -0.1203 | -0.877 | 0.0635  | -0.016 |
| -12.75°           | -0.942 | -0.1455 | -0.951 | 0.0717  | -0.020 |
| -13.4°            | -0.983 | -0.1633 | -0.994 | 0.0749  | -0.019 |
| -14.5°            | -0.715 | 0.0244  | -0.685 | 0.2068  | -0.086 |
| -14.85°           | -0.576 | 0.0370  | -0.545 | 0.1914  | -0.073 |

Table 8

LOCAL FORCE AND MOMENT COEFFICIENTS FROM INTEGRATED  
PRESSURE MEASUREMENTS

Wing AP/2 $V = 125 \text{ ft/sec}, R = 1.6 \times 10^6$ 

| $\alpha$          | $C_N$  | $C_T$   | $C_L$  | $C_D$  | $C_m$  |
|-------------------|--------|---------|--------|--------|--------|
| Normal attitude   |        |         |        |        |        |
| - 4.1°            | -0.250 | -0.0109 | -0.250 | 0.0086 | -0.012 |
| - 2.05°           | -0.125 | -0.0048 | -0.125 | 0.0004 | -0.005 |
| - 0.05°           | 0.005  | 0.0001  | 0.005  | 0      | -0.005 |
| 2.15°             | 0.133  | -0.0031 | 0.133  | 0.0011 | 0      |
| 4.0°              | 0.240  | -0.0129 | 0.240  | 0.0024 | 0.007  |
| 6.05°             | 0.362  | -0.0243 | 0.363  | 0.0119 | 0.007  |
| 8.15°             | 0.491  | -0.0375 | 0.492  | 0.0296 | 0.012  |
| 10.25°            | 0.603  | -0.0528 | 0.603  | 0.0516 | 0.015  |
| 12.35°            | 0.740  | -0.0785 | 0.740  | 0.0768 | 0.019  |
| 14.4°             | 0.844  | -0.1134 | 0.846  | 0.0949 | 0.019  |
| 15.1°             | 0.876  | -0.1229 | 0.878  | 0.1044 | 0.020  |
| 16.5°             | 0.701  | 0.0293  | 0.665  | 0.2231 | -0.090 |
| 17.65°            | 0.654  | 0.0404  | 0.636  | 0.2327 | -0.092 |
| Inverted attitude |        |         |        |        |        |
| 4.55°             | 0.277  | -0.0121 | 0.277  | 0.0082 | 0.001  |
| 2.45°             | 0.149  | -0.0017 | 0.149  | 0.0037 | -0.005 |
| 0.35°             | 0.022  | 0.0022  | 0.022  | 0.0022 | -0.008 |
| - 1.7°            | -0.106 | -0.0034 | -0.106 | 0.0005 | -0.010 |
| - 3.8°            | -0.226 | -0.0132 | -0.226 | 0.0032 | -0.017 |
| - 5.9°            | -0.355 | -0.0262 | -0.356 | 0.0126 | -0.019 |
| - 8.0°            | -0.485 | -0.0417 | -0.486 | 0.0290 | -0.020 |
| -10.05°           | -0.606 | -0.0564 | -0.606 | 0.0540 | -0.021 |
| -12.15°           | -0.732 | -0.0753 | -0.731 | 0.0849 | -0.019 |
| -14.2°            | -0.840 | -0.1061 | -0.840 | 0.1120 | -0.025 |
| -15.25°           | -0.896 | -0.1269 | -0.897 | 0.1189 | -0.027 |
| -16.1°            | -0.678 | 0.0315  | -0.641 | 0.2223 | 0.084  |
| -17.45°           | -0.615 | 0.0399  | -0.573 | 0.2258 | 0.091  |

Table 9  
LOCAL FORCE AND MOMENT COEFFICIENTS FROM INTEGRATED  
PRESSURE MEASUREMENTS

Wing AP/3

 $V = 125 \text{ ft/sec}, R = 1.6 \times 10^6$ 

| $\alpha$          | $C_N$  | $C_T$   | $C_L$  | $C_D$   | $C_m$  |
|-------------------|--------|---------|--------|---------|--------|
| Normal attitude   |        |         |        |         |        |
| - 5.75°           | -0.234 | -0.0164 | -0.234 | 0.0104  | -0.025 |
| - 3.7°            | -0.151 | -0.0086 | -0.151 | 0.0033  | -0.017 |
| - 2.7°            | -0.109 | -0.0048 | -0.109 | 0.0019  | -0.015 |
| - 1.7°            | -0.070 | -0.0037 | -0.070 | 0       | -0.013 |
| - 0.65°           | -0.035 | -0.0010 | -0.035 | -0.0001 | -0.009 |
| 0.35°             | -0.009 | -0.0009 | -0.009 | -0.0008 | -0.011 |
| 1.35°             | 0.057  | -0.0011 | 0.057  | -0.0005 | -0.005 |
| 2.35°             | 0.100  | -0.0022 | 0.100  | 0.0006  | 0.002  |
| 3.4°              | 0.139  | -0.0042 | 0.139  | 0.0021  | 0.006  |
| 4.4°              | 0.177  | -0.0065 | 0.177  | 0.0046  | 0.010  |
| 6.45°             | 0.269  | -0.0153 | 0.270  | 0.0112  | 0.019  |
| 8.45°             | 0.338  | -0.0262 | 0.339  | 0.0190  | 0.018  |
| 10.5°             | 0.437  | -0.0396 | 0.438  | 0.0344  | 0.024  |
| 12.5°             | 0.523  | -0.0570 | 0.524  | 0.0503  | 0.030  |
| 14.55°            | 0.614  | -0.0773 | 0.615  | 0.0708  | 0.033  |
| 16.55°            | 0.701  | -0.1031 | 0.703  | 0.0912  | -      |
| 18.6°             | 0.773  | -0.1317 | 0.776  | 0.1108  | -      |
| Inverted attitude |        |         |        |         |        |
| 7.35°             | 0.299  | -0.0144 | 0.299  | 0.0199  | 0.007  |
| 5.35°             | 0.223  | -0.0062 | 0.223  | 0.0115  | 0.002  |
| 4.3°              | 0.171  | -0.0023 | 0.171  | 0.0082  | 0      |
| 3.3°              | 0.135  | -0.0016 | 0.135  | 0.0043  | -0.003 |
| 2.3°              | 0.095  | 0.0011  | 0.095  | 0.0035  | -0.007 |
| 1.8°              | 0.047  | 0.0010  | 0.047  | 0.0014  | -0.007 |
| 0.25°             | 0.010  | 0.0019  | 0.010  | 0.0018  | -0.009 |
| - 0.75°           | -0.028 | -0.0008 | -0.028 | 0       | -0.013 |
| - 1.75°           | -0.070 | -0.0018 | -0.070 | 0.0014  | -0.018 |
| - 2.75°           | -0.105 | -0.0039 | -0.105 | 0.0027  | -0.018 |
| - 4.8°            | -0.184 | -0.0114 | -0.184 | 0.0066  | -0.025 |
| - 6.85°           | -0.275 | -0.0208 | -0.275 | 0.0160  | -0.030 |
| - 8.85°           | -0.378 | -0.0351 | -0.379 | 0.0289  | -0.030 |
| -10.9°            | -0.453 | -0.0511 | -0.454 | 0.0417  | -0.035 |
| -12.9°            | -0.553 | -0.0722 | -0.554 | 0.0610  | -0.038 |
| -14.95°           | -0.640 | -0.0926 | -0.641 | 0.0846  | -0.043 |
| -16.95°           | -0.726 | -0.1196 | -0.730 | 0.1076  | -0.047 |
| -18.0°            | -0.776 | -0.1376 | -0.779 | 0.1197  | -0.046 |
| -18.3°            | -0.792 | -0.1426 | -0.795 | 0.1242  | -0.065 |

Table 9 (Contd)

LOCAL FORCE AND MOMENT COEFFICIENTS FROM INTEGRATED  
PRESSURE MEASUREMENTS

Wing AP/3

 $V = 250 \text{ ft/sec}, R = 3.2 \times 10^6$ 

| $\alpha$          | $C_N$  | $C_T$   | $C_L$  | $C_D$   | $C_m$  |
|-------------------|--------|---------|--------|---------|--------|
| Normal attitude   |        |         |        |         |        |
| - 3.75°           | -0.144 | -0.0045 | -0.144 | 0.0067  | -0.017 |
| - 2.7°            | -0.101 | -0.0030 | -0.101 | 0.0031  | -0.014 |
| - 1.7°            | -0.062 | -0.0019 | -0.062 | 0.0007  | -0.012 |
| - 0.7°            | -0.025 | -0.0011 | -0.025 | -0.0005 | -0.007 |
| 0.3°              | 0.014  | -0.0012 | 0.014  | -0.0013 | -0.005 |
| 1.3°              | 0.053  | -0.0011 | 0.053  | -0.0005 | -0.006 |
| 2.35°             | 0.094  | -0.0033 | 0.094  | -0.0006 | 0.002  |
| 3.35°             | 0.143  | -0.0054 | 0.143  | 0.0012  | 0.004  |
| 4.35°             | 0.186  | -0.0085 | 0.186  | 0.0035  | 0.005  |
| 6.4°              | 0.273  | -0.0160 | 0.273  | 0.0112  | 0.012  |
| 8.4°              | 0.357  | -0.0270 | 0.357  | 0.0212  | 0.015  |
| 10.45°            | 0.435  | -0.0409 | 0.436  | 0.0334  | 0.014  |
| 12.5°             | 0.521  | -0.0591 | 0.522  | 0.0486  | 0.017  |
| 14.5°             | 0.612  | -0.0816 | 0.614  | 0.0669  | 0.023  |
| 16.55°            | 0.692  | -0.1049 | 0.694  | 0.0879  | 0.023  |
| 17.55°            | 0.720  | -0.1178 | 0.723  | 0.0959  | 0.023  |
| Inverted attitude |        |         |        |         |        |
| 5.15°             | 0.216  | -0.0092 | 0.216  | 0.0077  | 0.003  |
| 4.15°             | 0.172  | -0.0045 | 0.172  | 0.0059  | -0.002 |
| 3.15°             | 0.125  | -0.0025 | 0.125  | 0.0028  | -0.004 |
| 2.1°              | 0.091  | -0.0011 | 0.091  | 0.0011  | -0.005 |
| 1.1°              | 0.042  | -0.0006 | 0.042  | -0.0004 | -0.009 |
| 0.1°              | 0.003  | 0.0015  | 0.003  | 0.0015  | -0.011 |
| - 0.9°            | -0.032 | 0.0002  | -0.032 | 0.0011  | -0.013 |
| - 1.95°           | -0.076 | -0.0010 | -0.076 | 0.0025  | -0.018 |
| - 2.95°           | -0.119 | -0.0023 | -0.119 | 0.0053  | -0.019 |
| - 5.0°            | -0.206 | -0.0087 | -0.206 | 0.0118  | -0.024 |
| - 7.0°            | -0.293 | -0.0192 | -0.293 | 0.0202  | -0.028 |
| - 9.05°           | -0.377 | -0.0310 | -0.377 | 0.0332  | -0.029 |
| -11.05°           | -0.464 | -0.0455 | -0.464 | 0.0501  | -0.035 |
| -13.1°            | -0.549 | -0.0627 | -0.548 | 0.0700  | -0.041 |
| -15.1°            | -0.632 | -0.0859 | -0.631 | 0.0897  | -0.042 |
| -16.15°           | -0.677 | -0.1064 | -0.679 | 0.0943  | -0.041 |



Table 10  
LOCAL FORCE AND MOMENT COEFFICIENTS FROM INTEGRATED  
PRESSURE MEASUREMENTS

Wing AP/4

V = 125 ft/sec, R =  $1.6 \times 10^6$ 

| $\alpha$          | $C_N$  | $C_T$   | $C_L$  | $C_D$   | $C_m$  |
|-------------------|--------|---------|--------|---------|--------|
| Normal attitude   |        |         |        |         |        |
| - 5.75°           | -0.175 | -0.0113 | -0.175 | 0.0082  | -0.025 |
| - 3.75°           | -0.119 | -0.0057 | -0.119 | 0.0034  | -0.018 |
| - 2.75°           | -0.085 | -0.0027 | -0.085 | 0.0023  | -0.015 |
| - 1.75°           | -0.054 | -0.0003 | -0.054 | 0.0019  | -0.012 |
| - 0.6°            | -0.022 | 0       | -0.022 | 0.0005  | -0.009 |
| 0.3°              | 0.009  | 0.0005  | 0.009  | 0.0004  | -0.005 |
| 1.3°              | 0.054  | 0.0002  | 0.054  | 0.0008  | 0      |
| 2.3°              | 0.076  | -0.0010 | 0.076  | 0.0013  | 0      |
| 3.3°              | 0.101  | -0.0029 | 0.101  | 0.0019  | 0.005  |
| 4.3°              | 0.137  | -0.0048 | 0.137  | 0.0041  | 0.007  |
| 6.35°             | 0.198  | -0.0098 | 0.198  | 0.0101  | 0.014  |
| 10.35°            | 0.336  | -0.0282 | 0.336  | 0.0292  | 0.023  |
| 14.4°             | 0.477  | -0.0530 | 0.477  | 0.0623  | 0.025  |
| 18.45°            | 0.631  | -0.0885 | 0.628  | 0.1091  | 0.030  |
| 20.45°            | 0.710  | -0.1085 | 0.705  | 0.1390  | 0.034  |
| 20.85°            | 0.701  | -0.1134 | 0.697  | 0.1362  | -0.028 |
| 21.05°            | 0.661  | -0.0039 | 0.621  | 0.2273  | -0.028 |
| Inverted attitude |        |         |        |         |        |
| 6.95°             | 0.214  | -0.0121 | 0.214  | 0.0117  | 0.013  |
| 4.95°             | 0.151  | -0.0065 | 0.151  | 0.0049  | 0.009  |
| 3.95°             | 0.121  | -0.0039 | 0.121  | 0.0033  | 0.005  |
| 2.95°             | 0.090  | -0.0018 | 0.090  | 0.0018  | 0.003  |
| 1.95°             | 0.062  | -0.0006 | 0.062  | 0.0009  | -0.001 |
| 0.9°              | 0.032  | -0.0008 | 0.032  | -0.0007 | -0.004 |
| - 0.1°            | -0.008 | -0.0010 | -0.008 | -0.0009 | -0.008 |
| - 1.1°            | -0.034 | -0.0006 | -0.034 | 0.0004  | -0.011 |
| - 2.1°            | -0.068 | -0.0021 | -0.068 | 0.0012  | -0.015 |
| - 3.1°            | -0.099 | -0.0044 | -0.099 | 0.0021  | -0.017 |
| - 5.15°           | -0.167 | -0.0093 | -0.167 | 0.0074  | -0.022 |
| - 9.15°           | -0.297 | -0.0259 | -0.297 | 0.0248  | -0.033 |
| -13.2°            | -0.455 | -0.0538 | -0.455 | 0.0563  | -0.042 |
| -17.25°           | -0.602 | -0.0894 | -0.601 | 0.0993  | -0.049 |
| -19.25°           | -0.682 | -0.1123 | -0.680 | 0.1260  | -0.051 |
| -21.25°           | -0.758 | -0.1339 | -0.753 | 0.1580  | -0.052 |
| -21.55°           | -0.771 | -0.1328 | -0.764 | 0.1642  | -0.054 |

Table 10 (Contd)

LOCAL FORCE AND MOMENT COEFFICIENTS FROM INTEGRATED  
PRESSURE MEASUREMENTS

Wing AP/4

 $V = 250 \text{ ft/sec}, R = 3.2 \times 10^6$ 

| $\alpha$          | $C_N$  | $C_T$   | $C_L$  | $C_D$   | $C_m$  |
|-------------------|--------|---------|--------|---------|--------|
| Normal attitude   |        |         |        |         |        |
| - 5.75°           | -0.180 | -0.0108 | -0.180 | 0.0090  | -0.021 |
| - 3.75°           | -0.115 | -0.0048 | -0.115 | 0.0038  | -0.016 |
| - 2.75°           | -0.081 | -0.0025 | -0.081 | 0.0022  | -0.014 |
| - 1.75°           | -0.048 | -0.0020 | -0.048 | 0.0001  | -0.014 |
| - 0.75°           | -0.024 | 0       | -0.024 | 0.0005  | -0.008 |
| 0.3°              | 0.006  | -0.0006 | 0.006  | -0.0006 | -0.004 |
| 1.3°              | 0.039  | -0.0009 | 0.039  | -0.0003 | -0.001 |
| 2.3°              | 0.069  | -0.0016 | 0.069  | -0.0005 | 0.002  |
| 3.3°              | 0.098  | -0.0032 | 0.098  | 0.0015  | 0.007  |
| 4.3°              | 0.132  | -0.0047 | 0.132  | 0.0040  | 0.008  |
| 6.35°             | 0.194  | -0.0101 | 0.194  | 0.0095  | 0.014  |
| 10.35°            | 0.333  | -0.0265 | 0.333  | 0.0306  | 0.024  |
| 14.4°             | 0.472  | -0.0529 | 0.471  | 0.0615  | 0.039  |
| 18.4°             | 0.601  | -0.0897 | 0.599  | 0.0918  | 0.032  |
| 20.45°            | 0.707  | -0.1084 | 0.702  | 0.1386  | 0.027  |
| 21.45°            | 0.736  | -0.1181 | 0.730  | 0.1522  | 0.024  |
| Inverted attitude |        |         |        |         |        |
| 6.85°             | 0.213  | -0.0114 | 0.213  | 0.0122  | 0.014  |
| 4.85°             | 0.147  | -0.0058 | 0.147  | 0.0052  | 0.009  |
| 3.85°             | 0.102  | -0.0038 | 0.102  | 0.0021  | 0.011  |
| 2.85°             | 0.083  | -0.0020 | 0.083  | 0.0014  | 0.005  |
| 1.85°             | 0.052  | -0.0005 | 0.052  | 0.0006  | -0.001 |
| 0.85°             | 0.020  | 0       | 0.020  | 0.0001  | -0.003 |
| - 0.2°            | -0.013 | -0.0003 | -0.013 | -0.0001 | -0.007 |
| - 1.2°            | -0.036 | 0       | -0.036 | 0.0011  | -0.011 |
| - 2.2°            | -0.065 | -0.0023 | -0.065 | 0.0009  | -0.014 |
| - 3.2°            | -0.097 | -0.0037 | -0.097 | 0.0026  | -0.017 |
| - 5.2°            | -0.165 | -0.0092 | -0.165 | 0.0075  | -0.023 |
| - 9.25°           | -0.313 | -0.0278 | -0.313 | 0.0259  | -0.032 |
| -13.3°            | -0.456 | -0.0543 | -0.456 | 0.0565  | -0.040 |
| -17.3°            | -0.598 | -0.0843 | -0.595 | 0.1033  | -0.040 |
| -19.35°           | -0.668 | -0.1015 | -0.663 | 0.1318  | -0.036 |
| -21.35°           | -0.741 | -0.1183 | -0.732 | 0.1666  | -0.032 |
| -23.35°           | -0.823 | -0.1486 | -0.813 | 0.1979  | -0.029 |
| -24.4°            | -0.851 | -0.1600 | -0.839 | 0.2137  | -0.024 |
| -25.4°            | -0.895 | -0.1480 | -0.870 | 0.2584  | -0.026 |

Table 11  
LOCAL FORCE AND MOMENT COEFFICIENTS FROM INTEGRATED  
PRESSURE MEASUREMENTS

Wing AP/5

 $V = 125 \text{ ft/sec}, R = 1.6 \times 10^6$ 

| $\alpha$          | $C_N$  | $C_T$   | $C_L$  | $C_D$  | $C_m$  |
|-------------------|--------|---------|--------|--------|--------|
| Normal attitude   |        |         |        |        |        |
| - 5.8°            | -0.095 | -0.0038 | -0.095 | 0.0068 | -0.020 |
| - 3.8°            | -0.064 | 0.0002  | -0.064 | 0.0051 | -0.015 |
| - 2.8°            | -0.041 | 0.0005  | -0.041 | 0.0024 | -0.015 |
| - 1.8°            | -0.025 | 0.0018  | -0.025 | 0.0028 | -0.009 |
| - 0.8°            | -0.011 | 0.0029  | -0.011 | 0.0031 | -0.007 |
| 0.2°              | -0.002 | 0.0024  | -0.002 | 0.0024 | -0.003 |
| 1.2°              | 0.018  | 0.0020  | 0.018  | 0.0022 | 0.002  |
| 2.2°              | 0.035  | 0.0018  | 0.035  | 0.0028 | 0.006  |
| 3.2°              | 0.049  | 0.0010  | 0.049  | 0.0032 | 0.010  |
| 4.2°              | 0.062  | 0.0003  | 0.062  | 0.0042 | 0.013  |
| 6.2°              | 0.100  | -0.0026 | 0.100  | 0.0072 | 0.016  |
| 8.2°              | 0.141  | -0.0063 | 0.141  | 0.0125 | 0.020  |
| 10.2°             | 0.178  | -0.0101 | 0.177  | 0.0198 | 0.022  |
| 14.2°             | 0.280  | -0.0224 | 0.277  | 0.0442 | 0.019  |
| 18.25°            | 0.388  | -0.0355 | 0.381  | 0.0838 | 0.009  |
| 22.25°            | 0.523  | -0.0549 | 0.506  | 0.1420 | -0.002 |
| 24.25°            | 0.591  | -0.0672 | 0.566  | 0.1751 | -0.012 |
| 25.25°            | 0.631  | -0.0757 | 0.605  | 0.1945 | -0.018 |
| 25.55°            | 0.643  | -0.0765 | 0.615  | 0.2019 | -0.019 |
| 26.25°            | 0.604  | -0.0172 | 0.552  | 0.2460 | -0.028 |
| Inverted attitude |        |         |        |        |        |
| 7.0°              | 0.109  | -0.0040 | 0.109  | 0.0083 | 0.016  |
| 5.0°              | 0.076  | 0.0003  | 0.076  | 0.0062 | 0.011  |
| 4.0°              | 0.061  | 0.0012  | 0.061  | 0.0048 | 0.007  |
| 3.0°              | 0.048  | 0.0010  | 0.048  | 0.0030 | 0.003  |
| 2.0°              | 0.031  | 0.0024  | 0.031  | 0.0032 | 0      |
| 1.0°              | 0.015  | 0.0028  | 0.015  | 0.0029 | -0.002 |
| 0°                | -0.001 | 0.0027  | -0.001 | 0.0027 | -0.006 |
| - 1.0°            | -0.016 | 0.0015  | -0.016 | 0.0020 | -0.010 |
| - 2.0°            | -0.033 | 0.0005  | -0.033 | 0.0020 | -0.013 |
| - 3.0°            | -0.050 | -0.0010 | -0.050 | 0.0022 | -0.016 |
| - 5.0°            | -0.080 | -0.0024 | -0.080 | 0.0054 | -0.019 |
| - 7.0°            | -0.119 | -0.0060 | -0.119 | 0.0098 | -0.026 |
| - 9.0°            | -0.159 | -0.0097 | -0.158 | 0.0170 | -0.039 |
| -13.0°            | -0.259 | -0.0225 | -0.257 | 0.0391 | -0.030 |
| -17.05°           | -0.362 | -0.0370 | -0.356 | 0.0745 | -0.026 |
| -21.05°           | -0.481 | -0.0595 | -0.469 | 0.1222 | -0.013 |
| -23.05°           | -0.556 | -0.0740 | -0.539 | 0.1552 | -0.008 |
| -25.05°           | -0.626 | -0.0819 | -0.600 | 0.1973 | -0.001 |
| -27.05°           | -0.699 | -0.0945 | -0.663 | 0.2409 | 0.009  |
| -28.3°            | -0.740 | -0.0980 | -0.695 | 0.2716 | 0.016  |
| -29.05°           | -0.652 | -0.0143 | -0.574 | 0.3103 | 0.015  |

Table 11 (Contd)

LOCAL FORCE AND MOMENT COEFFICIENTS FROM INTEGRATED  
PRESSURE MEASUREMENTS

Wing AP/5

 $V = 250 \text{ ft/sec, } R = 3.2 \times 10^6$ 

| $\alpha$                     | $C_N$  | $C_T$   | $C_L$  | $C_D$  | $C_m$  |
|------------------------------|--------|---------|--------|--------|--------|
| Normal <sup>o</sup> attitude |        |         |        |        |        |
| - 6.2 <sup>o</sup>           | -0.101 | -0.0027 | -0.101 | 0.0085 | 0.020  |
| - 4.2 <sup>o</sup>           | -0.065 | 0.0002  | -0.065 | 0.0051 | -0.015 |
| - 3.2 <sup>o</sup>           | -0.050 | 0.0010  | -0.050 | 0.0039 | -0.012 |
| - 2.2 <sup>o</sup>           | -0.032 | 0.0017  | -0.032 | 0.0030 | -0.009 |
| - 1.2 <sup>o</sup>           | -0.019 | 0.0020  | -0.019 | 0.0024 | -0.006 |
| - 0.2 <sup>o</sup>           | -0.005 | 0.0025  | -0.005 | 0.0025 | 0      |
| 0.8 <sup>o</sup>             | 0.012  | 0.0022  | 0.012  | 0.0023 | 0.002  |
| 1.8 <sup>o</sup>             | 0.027  | 0.0023  | 0.027  | 0.0031 | 0.006  |
| 2.8 <sup>o</sup>             | 0.042  | 0.0010  | 0.042  | 0.0029 | 0.010  |
| 3.8 <sup>o</sup>             | 0.059  | 0.0004  | 0.059  | 0.0042 | 0.013  |
| 5.8 <sup>o</sup>             | 0.100  | -0.0029 | 0.100  | 0.0070 | 0.015  |
| 7.85 <sup>o</sup>            | 0.139  | -0.0062 | 0.139  | 0.0125 | 0.019  |
| 9.85 <sup>o</sup>            | 0.189  | -0.0109 | 0.188  | 0.0209 | 0.020  |
| 13.85 <sup>o</sup>           | 0.280  | -0.0221 | 0.277  | 0.0448 | 0.020  |
| 17.85 <sup>o</sup>           | 0.395  | -0.0391 | 0.388  | 0.0829 | 0.012  |
| 21.85 <sup>o</sup>           | 0.525  | -0.0582 | 0.509  | 0.1401 | -0.002 |
| 23.9 <sup>o</sup>            | 0.585  | -0.0689 | 0.563  | 0.1724 | -0.014 |
| 25.9 <sup>o</sup>            | 0.657  | -0.0790 | 0.627  | 0.2141 | -0.026 |
| Inverted attitude            |        |         |        |        |        |
| 6.5 <sup>o</sup>             | 0.111  | -0.0041 | 0.111  | 0.0082 | 0.016  |
| 4.5 <sup>o</sup>             | 0.069  | -0.0013 | 0.069  | 0.0040 | 0.011  |
| 3.5 <sup>o</sup>             | 0.053  | 0       | 0.053  | 0.0031 | 0.009  |
| 2.5 <sup>o</sup>             | 0.037  | 0.0019  | 0.037  | 0.0034 | 0.005  |
| 1.5 <sup>o</sup>             | 0.022  | 0.0021  | 0.022  | 0.0026 | 0.001  |
| 0.5 <sup>o</sup>             | 0.006  | 0.0020  | 0.006  | 0.0020 | -0.002 |
| - 0.5 <sup>o</sup>           | -0.010 | 0.0025  | -0.010 | 0.0026 | -0.005 |
| - 1.5 <sup>o</sup>           | -0.021 | 0.0018  | -0.021 | 0.0024 | -0.009 |
| - 2.5 <sup>o</sup>           | -0.036 | 0.0009  | -0.036 | 0.0025 | -0.012 |
| - 3.5 <sup>o</sup>           | -0.052 | 0.0001  | -0.052 | 0.0034 | -0.016 |
| - 5.5 <sup>o</sup>           | -0.088 | -0.0024 | -0.088 | 0.0064 | -0.019 |
| - 7.55 <sup>o</sup>          | -0.131 | -0.0059 | -0.131 | 0.0117 | -0.024 |
| - 9.55 <sup>o</sup>          | -0.168 | -0.0095 | -0.167 | 0.0187 | -0.027 |
| -13.55 <sup>o</sup>          | -0.265 | -0.0226 | -0.263 | 0.0408 | -0.028 |
| -17.55 <sup>o</sup>          | -0.371 | -0.0383 | -0.365 | 0.0764 | -0.021 |
| -21.55 <sup>o</sup>          | -0.490 | -0.0573 | -0.476 | 0.1280 | -0.020 |
| -25.6 <sup>o</sup>           | -0.625 | -0.0778 | -0.597 | 0.2013 | 0.001  |
| -29.6 <sup>o</sup>           | -0.755 | -0.0989 | -0.705 | 0.2887 | 0.025  |
| -30.8 <sup>o</sup>           | -0.795 | -0.1004 | -0.733 | 0.3228 | 0.031  |

Table 12

BALANCE MEASUREMENTS OF LIFT, DRAG AND  
PITCHING MOMENT

Wing AF/1

$V = 125 \text{ ft/sec}; R = 1.6 \times 10^6$

$V = 250 \text{ ft/sec}; R = 3.2 \times 10^6$

| $\alpha$ | $\bar{c}_L$ | $\bar{c}_D$ | $\bar{c}_m$ |
|----------|-------------|-------------|-------------|
| - 4.3°   | -0.263      | 0.0124      | -0.0045     |
| - 3.2°   | -0.199      | 0.0092      | -0.0033     |
| - 2.15°  | -0.131      | 0.0070      | -0.0023     |
| - 1.05°  | -0.067      | 0.0058      | -0.0013     |
| 0        | 0           | 0.0054      | 0           |
| 1.05°    | 0.064       | 0.0058      | 0.0011      |
| 2.15°    | 0.130       | 0.0070      | 0.0023      |
| 3.2°     | 0.199       | 0.0092      | 0.0032      |
| 4.3°     | 0.262       | 0.0123      | 0.0043      |
| 6.4°     | 0.396       | 0.0218      | 0.0066      |
| 8.55°    | 0.539       | 0.0353      | 0.0046      |
| 10.7°    | 0.672       | 0.0519      | 0.0039      |
| 12.85°   | 0.801       | 0.0720      | 0.0030      |
| 15.0°    | 0.919       | 0.0951      | 0.0013      |
| 16.05°   | 0.972       | 0.1077      | -0.0001     |
| 17.1°    | 1.011       | 0.1209      | -0.0026     |

| $\alpha$ | $\bar{c}_L$ | $\bar{c}_D$ | $\bar{c}_m$ |
|----------|-------------|-------------|-------------|
| - 3.15°  | -0.198      | 0.0097      | -0.0036     |
| - 2.1°   | -0.133      | 0.0076      | -0.0024     |
| - 1.0°   | -0.065      | 0.0066      | -0.0013     |
| 0.05°    | 0.002       | 0.0063      | 0           |
| 1.1°     | 0.069       | 0.0067      | 0.0012      |
| 2.2°     | 0.136       | 0.0081      | 0.0023      |
| 3.25°    | 0.202       | 0.0106      | 0.0035      |
| 4.35°    | 0.268       | 0.0139      | 0.0044      |
| 6.4°     | 0.401       | 0.0225      | 0.0063      |
| 8.55°    | 0.535       | 0.0347      | 0.0071      |
| 10.7°    | 0.674       | 0.0512      | 0.0058      |
| 12.85°   | 0.807       | 0.0709      | 0.0049      |
| 15.0°    | 0.935       | 0.0945      | 0.0036      |
| 17.1°    | 1.036       | 0.1195      | 0.0020      |

Table 13

BALANCE MEASUREMENTS OF LIFT, DRAG AND  
PITCHING MOMENT

Wing AF/2

$V = 125 \text{ ft/sec}; R = 1.6 \times 10^6$

$V = 250 \text{ ft/sec}; R = 3.2 \times 10^6$

| $\alpha$ | $\bar{c}_L$ | $\bar{c}_D$ | $\bar{c}_m$ |
|----------|-------------|-------------|-------------|
| -4.45°   | -0.217      | 0.0129      | -0.0050     |
| -3.4°    | -0.168      | 0.0100      | -0.0042     |
| -2.35°   | -0.115      | 0.0077      | -0.0029     |
| -1.3°    | -0.064      | 0.0063      | -0.0016     |
| -0.3°    | -0.014      | 0.0057      | -0.0002     |
| 0.75°    | 0.035       | 0.0059      | 0.0013      |
| 1.8°     | 0.087       | 0.0069      | 0.0028      |
| 2.8°     | 0.139       | 0.0086      | 0.0041      |
| 3.85°    | 0.188       | 0.0110      | 0.0050      |
| 5.9°     | 0.289       | 0.0189      | 0.0065      |
| 8.0°     | 0.392       | 0.0295      | 0.0072      |
| 10.05°   | 0.502       | 0.0443      | 0.0045      |
| 12.15°   | 0.610       | 0.0626      | 0.0031      |
| 14.2°    | 0.713       | 0.0836      | 0.0014      |
| 16.25°   | 0.811       | 0.1085      | -0.0015     |
| 17.3°    | 0.860       | 0.1226      | -0.0034     |
| 18.35°   | 0.899       | 0.1362      | -0.0057     |

| $\alpha$ | $\bar{c}_L$ | $\bar{c}_D$ | $\bar{c}_m$ |
|----------|-------------|-------------|-------------|
| -3.35°   | -0.163      | 0.0110      | -0.0046     |
| -2.3°    | -0.113      | 0.0087      | -0.0036     |
| -1.25°   | -0.062      | 0.0074      | -0.0023     |
| -0.2°    | -0.011      | 0.0068      | -0.0009     |
| 0.8°     | 0.039       | 0.0069      | 0.0006      |
| 1.85°    | 0.091       | 0.0078      | 0.0020      |
| 2.9°     | 0.142       | 0.0096      | 0.0033      |
| 3.9°     | 0.193       | 0.0124      | 0.0047      |
| 6.0°     | 0.292       | 0.0195      | 0.0059      |
| 8.05°    | 0.399       | 0.0302      | 0.0070      |
| 10.1°    | 0.502       | 0.0440      | 0.0073      |
| 12.2°    | 0.614       | 0.0610      | 0.0053      |
| 14.25°   | 0.725       | 0.0804      | 0.0022      |
| 16.35°   | 0.830       | 0.1099      | -0.0004     |
| 17.4°    | 0.881       | 0.1239      | -0.0016     |
| 18.4°    | 0.930       | 0.1390      | -0.0033     |

Table 14

BALANCE MEASUREMENTS OF LIFT, DRAG AND  
PITCHING MOMENT

Wing AF/3

$V = 125 \text{ ft/sec}; R = 1.6 \times 10^6$

$V = 250 \text{ ft/sec}; R = 3.2 \times 10^6$

| $\alpha$ | $\bar{c}_L$ | $\bar{c}_D$ | $\bar{c}_m$ |
|----------|-------------|-------------|-------------|
| - 4.1°   | -0.136      | 0.0136      | -0.0069     |
| - 3.1°   | -0.101      | 0.0113      | -0.0057     |
| - 2.05°  | -0.066      | 0.0095      | -0.0042     |
| - 1.05°  | -0.034      | 0.0087      | -0.0025     |
| - 0.05°  | -0.002      | 0.0082      | -0.0002     |
| 0.95°    | 0.032       | 0.0084      | 0.0026      |
| 1.95°    | 0.063       | 0.0092      | 0.0046      |
| 3.0°     | 0.097       | 0.0107      | 0.0063      |
| 4.0°     | 0.131       | 0.0127      | 0.0073      |
| 6.1°     | 0.203       | 0.0189      | 0.0086      |
| 8.1°     | 0.274       | 0.0281      | 0.0096      |
| 10.15°   | 0.352       | 0.0406      | 0.0078      |
| 12.15°   | 0.438       | 0.0582      | 0.0026      |
| 14.2°    | 0.529       | 0.0800      | -0.0026     |
| 16.25°   | 0.607       | 0.1029      | -0.0080     |
| 18.25°   | 0.694       | 0.1324      | -0.0145     |
| 20.3°    | 0.778       | 0.1655      | -0.0225     |
| 22.3°    | 0.854       | 0.2017      | -0.0314     |
| 22.85°   | 0.595       | 0.2707      | -0.1034     |

| $\alpha$ | $\bar{c}_L$ | $\bar{c}_D$ | $\bar{c}_m$ |
|----------|-------------|-------------|-------------|
| - 2.15°  | -0.066      | 0.0108      | -0.0042     |
| - 1.1°   | -0.035      | 0.0099      | -0.0022     |
| - 0.1°   | -0.003      | 0.0095      | 0.0001      |
| 0.9°     | 0.029       | 0.0096      | 0.0026      |
| 1.9°     | 0.061       | 0.0104      | 0.0047      |
| 2.95°    | 0.095       | 0.0118      | 0.0065      |
| 3.95°    | 0.128       | 0.0140      | 0.0075      |
| 6.0°     | 0.204       | 0.0207      | 0.0088      |
| 8.0°     | 0.278       | 0.0302      | 0.0091      |
| 10.05°   | 0.354       | 0.0425      | 0.0082      |
| 12.05°   | 0.434       | 0.0586      | 0.0060      |
| 14.1°    | 0.519       | 0.0790      | 0.0021      |
| 16.15°   | 0.607       | 0.1040      | -0.0043     |
| 18.15°   | 0.696       | 0.1336      | -0.0110     |
| 20.2°    | 0.782       | 0.1664      | -0.0182     |
| 22.25°   | 0.867       | 0.2043      | -0.0263     |

Table 15

BALANCE MEASUREMENTS OF LIFT, DRAG AND  
PITCHING MOMENT

Wing AF/4

$V = 125 \text{ ft/sec}; R = 1.6 \times 10^6$

$V = 250 \text{ ft/sec}; R = 3.2 \times 10^6$

| $\alpha$ | $\bar{c}_L$ | $\bar{c}_D$ | $\bar{c}_m$ |
|----------|-------------|-------------|-------------|
| - 4.2°   | -0.104      | 0.0128      | -0.0087     |
| - 3.15°  | -0.077      | 0.0112      | -0.0074     |
| - 2.15°  | -0.051      | 0.0098      | -0.0058     |
| - 1.15°  | -0.028      | 0.0090      | -0.0035     |
| - 0.15°  | -0.003      | 0.0087      | -0.0003     |
| 0.85°    | 0.019       | 0.0088      | 0.0024      |
| 1.85°    | 0.042       | 0.0092      | 0.0051      |
| 2.85°    | 0.068       | 0.0105      | 0.0075      |
| 3.9°     | 0.095       | 0.0120      | 0.0086      |
| 5.9°     | 0.150       | 0.0164      | 0.0104      |
| 7.9°     | 0.208       | 0.0243      | 0.0098      |
| 9.9°     | 0.269       | 0.0248      | 0.0079      |
| 11.95°   | 0.334       | 0.0492      | 0.0032      |
| 13.95°   | 0.407       | 0.0676      | -0.0051     |
| 16.0°    | 0.477       | 0.0895      | -0.0134     |
| 18.0°    | 0.554       | 0.1173      | -0.0248     |
| 20.0°    | 0.632       | 0.1497      | -0.0373     |
| 22.05°   | 0.712       | 0.1877      | -0.0507     |
| 24.05°   | 0.786       | 0.2277      | -0.0638     |
| 25.05°   | 0.820       | 0.2507      | -0.0727     |
| 25.35°   | 0.738       | 0.3527      | -0.1401     |

| $\alpha$ | $\bar{c}_L$ | $\bar{c}_D$ | $\bar{c}_m$ |
|----------|-------------|-------------|-------------|
| - 4.15°  | -0.102      | 0.0137      | -0.0088     |
| - 3.1°   | -0.075      | 0.0117      | -0.0077     |
| - 2.1°   | -0.049      | 0.0104      | -0.0057     |
| - 1.1°   | -0.025      | 0.0096      | -0.0033     |
| - 0.1°   | -0.002      | 0.0093      | -0.0003     |
| 0.9°     | 0.021       | 0.0093      | 0.0026      |
| 1.9°     | 0.045       | 0.0100      | 0.0049      |
| 2.9°     | 0.070       | 0.0111      | 0.0073      |
| 3.95°    | 0.097       | 0.0129      | 0.0085      |
| 5.95°    | 0.153       | 0.0187      | 0.0100      |
| 7.95°    | 0.211       | 0.0267      | 0.0095      |
| 9.95°    | 0.273       | 0.0375      | 0.0072      |
| 12.0°    | 0.336       | 0.0511      | 0.0039      |
| 14.0°    | 0.406       | 0.0694      | -0.0027     |
| 16.05°   | 0.476       | 0.0911      | -0.0104     |
| 18.05°   | 0.548       | 0.1170      | -0.0192     |
| 20.05°   | 0.619       | 0.1463      | -0.0290     |
| 22.1°    | 0.693       | 0.1811      | -0.0405     |
| 24.1°    | 0.767       | 0.2202      | -0.0533     |
| 25.1°    | 0.804       | 0.2411      | -0.0600     |
| 26.1°    | 0.838       | 0.2632      | -0.0667     |



Table 16

BALANCE MEASUREMENTS OF LIFT, DRAG AND  
PITCHING MOMENT

Wing AF/5

$V = 125 \text{ ft/sec}; R = 1.6 \times 10^6$

$V = 250 \text{ ft/sec}; R = 3.2 \times 10^6$

| $\alpha$ | $\bar{C}_L$ | $\bar{C}_D$ | $\bar{C}_m$ |
|----------|-------------|-------------|-------------|
| - 4.1°   | -0.054      | 0.0141      | -0.0075     |
| - 3.1    | -0.038      | 0.0126      | -0.0073     |
| - 2.1°   | -0.025      | 0.0119      | -0.0051     |
| - 1.1°   | -0.011      | 0.0112      | -0.0049     |
| - 0.1°   | -0.001      | 0.0112      | -0.0013     |
| 0.9°     | 0.012       | 0.0115      | -0.0003     |
| 1.9°     | 0.023       | 0.0115      | 0.0036      |
| 2.9°     | 0.036       | 0.0121      | 0.0052      |
| 3.9°     | 0.048       | 0.0132      | 0.0071      |
| 5.9°     | 0.079       | 0.0156      | 0.0077      |
| 7.9°     | 0.116       | 0.0210      | 0.0031      |
| 9.9°     | 0.157       | 0.0296      | 0           |
| 13.9°    | 0.246       | 0.0549      | -0.0103     |
| 17.95°   | 0.351       | 0.0951      | -0.0388     |
| 21.95°   | 0.469       | 0.1545      | -0.0707     |
| 25.95°   | 0.600       | 0.2563      | -0.1123     |
| 30.0°    | 0.725       | 0.3812      | -0.1435     |
| 34.0°    | 0.865       | 0.5364      | -0.2052     |
| 38.0°    | 0.940       | 0.6729      | -0.2293     |
| 42.05°   | 1.010       | 0.8314      | -0.2674     |
| 46.0°    | 0.981       | 0.9120      | -0.2480     |

| $\alpha$ | $\bar{C}_L$ | $\bar{C}_D$ | $\bar{C}_m$ |
|----------|-------------|-------------|-------------|
| - 4.15°  | -0.054      | 0.0145      | -0.0069     |
| - 3.15°  | -0.038      | 0.0138      | -0.0062     |
| - 2.1°   | -0.025      | 0.0133      | -0.0048     |
| - 1.1°   | -0.013      | 0.0127      | -0.0027     |
| - 0.1°   | -0.001      | 0.0127      | -0.0004     |
| 0.9°     | 0.010       | 0.0126      | 0.0023      |
| 1.9°     | 0.022       | 0.0129      | 0.0044      |
| 2.9°     | 0.035       | 0.0133      | 0.0063      |
| 3.9°     | 0.048       | 0.0142      | 0.0071      |
| 5.9°     | 0.081       | 0.0184      | 0.0069      |
| 7.9°     | 0.115       | 0.0237      | 0.0048      |
| 9.9°     | 0.153       | 0.0312      | 0.0015      |
| 13.9°    | 0.236       | 0.0542      | -0.0108     |
| 17.9°    | 0.336       | 0.0926      | -0.0326     |
| 21.95°   | 0.448       | 0.1477      | -0.0609     |
| 25.95°   | 0.567       | 0.2218      | -0.0938     |
| 29.95°   | 0.678       | 0.3088      | -0.1270     |
| 34.0°    | 0.798       | 0.4881      | -0.1838     |

Table 17

BOUNDARY LAYER TRANSITION POSITION AT  
CENTRE SECTION: A SERIES WINGS

| $V = 125 \text{ ft/sec}; R = 1.6 \times 10^6$ |                   |               | $V = 250 \text{ ft/sec}; R = 3.2 \times 10^6$ |                   |               |
|---|-------------------|---------------|---|-------------------|---------------|
| $\alpha$                                      | $X_T/C$           |               | $\alpha$                                      | $X_T/C$           |               |
|   | Upper surface     | Lower surface |   | Upper surface     | Lower surface |
| <u>AF/1</u>                                   |                   |               |   |                   |               |
| - 4.3°  | 0.82              | 0.25          | - 2.05°                                       | 0.54              | 0.40          |
| - 2.15°                                       | 0.70              | 0.51          | 0.10°   | 0.47              | 0.46          |
| 0°  | 0.58              | 0.58          | 2.25°   | 0.36              | 0.54          |
| 2.15°   | 0.51              | 0.68          | 4.4°  | 0.10              | 0.68          |
| 4.25°   | 0.22              | 0.80          | 6.4°  | 0.03 <sub>1</sub> | 0.84          |
| 6.4°  | 0.06              | 1.00          | 8.55°   | 0.01 <sub>3</sub> | 1.00          |
| 8.55°   | 0.02 <sub>2</sub> | -             |   |                   |               |
| 10.7°   | 0.01 <sub>3</sub> | -             |   |                   |               |
| <u>AF/2</u>                                   |                   |               |   |                   |               |
| - 4.45°                                       | 0.78              | 0.40          | - 2.3°  | 0.57              | 0.40          |
| - 2.35°                                       | 0.69              | 0.52          | - 0.2°  | 0.50              | 0.48          |
| - 0.3°  | 0.60              | 0.60          | 1.85°   | 0.43              | 0.56          |
| 1.8°  | 0.52              | 0.70          | 3.9°  | 0.16              | 0.66          |
| 3.85°   | 0.41              | 0.75          | 6.0°  | 0.06              | 0.70          |
| 5.9°  | 0.20              | 0.83          | 8.05°   | 0.01 <sub>9</sub> | 0.77          |
| 8.0°  | 0.03              | 1.00          | 10.1°   | 0.01 <sub>0</sub> | 1.00          |
| 10.05°  | 0.01 <sub>2</sub> | -             |   |                   |               |
| <u>AF/3</u>                                   |                   |               |   |                   |               |
| - 4.15°                                       | 0.75              | 0.44          | - 2.15°                                       | 0.54              | 0.42          |
| - 2.1°  | 0.69              | 0.52          | - 0.1°  | 0.52              | 0.52          |
| - 0.1°  | 0.60              | 0.58          | 1.9°  | 0.47              | 0.57          |
| 1.9°  | 0.53              | 0.66          | 3.95°   | 0.27              | 0.56          |
| 3.95°   | 0.46              | 0.74          | 6.0°  | 0.09              | 0.62          |
| 6.1°  | 0.29              | 0.78          | 8.0°  | 0.04 <sub>2</sub> | 0.68          |
| 8.1°  | 0.10              | 0.94          | 10.05°  | 0.02 <sub>1</sub> | 0.81          |
| 10.15°  | 0.03 <sub>6</sub> | 1.00          | 12.05°  | 0.01 <sub>0</sub> | -             |
| 12.15°  | 0.01 <sub>6</sub> | -             |   |                   |               |

Table 17 (Contd)

BOUNDARY LAYER TRANSITION POSITION AT  
CENTRE SECTION: A SERIES WINGS

| $V = 125 \text{ ft/sec}; R = 1.6 \times 10^6$ |                   |               | $V = 250 \text{ ft/sec}; R = 3.2 \times 10^6$ |                   |               |
|---|-------------------|---------------|---|-------------------|---------------|
| $\alpha$                                      | $x_T/c$           |               | $\alpha$                                      | $x_T/c$           |               |
|   | Upper surface     | Lower surface |   | Upper surface     | Lower surface |
| AF/4  |                   |               |   |                   |               |
| - 4.2°  | 0.73              | 0.46          | - 4.15°                                       | 0.58              | 0.29          |
| - 2.15°                                       | 0.67              | 0.54          | - 2.1°  | 0.50              | 0.44          |
| - 0.15°                                       | 0.60              | 0.58          | - 0.1°  | 0.52              | 0.50          |
| 1.85°   | 0.52              | 0.65          | 1.9°  | 0.44              | 0.54          |
| 3.85°   | 0.46              | 0.73          | 3.95°   | 0.38              | 0.58          |
| 5.9°  | 0.33              | 0.77          | 5.95°   | 0.18              | 0.62          |
| 7.9°  | 0.14              | 0.81          | 7.95°   | 0.06 <sub>2</sub> | 0.75          |
| 9.9°  | 0.05 <sub>2</sub> | 0.98          | 9.95°   | 0.03 <sub>1</sub> | 0.83          |
| 11.95°  | 0.03 <sub>1</sub> | -             | 12.0°   | 0.01 <sub>0</sub> | 0.85          |
| 13.95°  | 0.02 <sub>1</sub> | -             |   |                   |               |
| AF/5  |                   |               |   |                   |               |
| - 4.15°                                       | 0.75              | 0.48          | - 4.1°  | 0.62              | 0.42          |
| - 0.1°  | 0.60              | 0.58          | - 0.1°  | 0.48              | 0.50          |
| 3.9°  | 0.48              | 0.75          | 3.9°  | 0.40              | 0.58          |
| 7.9°  |                   |               | 7.9°  | 0.10              | 0.67          |
| 11.9°   | 0.07 <sub>3</sub> | 0.85          | 11.9°   | 0.05 <sub>2</sub> | 0.71          |
| 15.95°  | 0.02 <sub>5</sub> | -             | 15.9°   | 0.01 <sub>0</sub> | -             |
| 20.95°  | 0.01 <sub>3</sub> | -             |   |                   |               |

Table 18

LIFT CURVE SLOPES AT ZERO LIFT, WINGS  
AF/1 AND AF/5

| Aspect ratio | $\bar{C}_l/\alpha$ |                 |        |                 |        |
|--------------|--------------------|-----------------|--------|-----------------|--------|
|              | Exp.               | Original method |        | Modified method |        |
|              |                    | k=1.00          | k=0.92 | k=1.00          | k=0.92 |
| 4.0          | 3.5                | 3.91            | 3.76   | 3.64            | 3.45   |
| 0.5          | 0.70               | 0.75            | 0.72   | 0.72            | 0.70   |

Table 19

Wing BP/O

$C_p$

$V = 250$  ft/sec;  $R = 3.2 \times 10^6$

| $\alpha$<br>X/C | -4.05° | -2.0°  | 0°     | 2.0°   | 4.05°  | 6.05°  | 8.1°   | 10.1°  | 12.15° | 14.15°  | 16.15°  |
|-----------------|--------|--------|--------|--------|--------|--------|--------|--------|--------|---------|---------|
| Upper surface   |        |        |        |        |        |        |        |        |        |         |         |
| $\theta$        | -2.252 | -1.123 | 0.354  | 1.002  | 0.824  | -0.319 | -2.620 | -5.761 | -9.053 | -11.486 | -10.488 |
| 0.005           | 1.011  | 0.895  | 0.541  | -0.104 | -0.969 | -2.130 | -3.572 | -5.154 | -6.548 | -7.099  | -6.763  |
| 0.015           | 0.778  | 0.494  | 0.062  | -0.556 | -1.281 | -2.185 | -3.116 | -4.141 | -5.075 | -5.675  | -5.039  |
| 0.030           | 0.468  | 0.164  | -0.230 | -0.740 | -1.296 | -1.962 | -2.663 | -3.363 | -4.014 | -4.423  | -4.000  |
| 0.050           | 0.246  | -0.035 | -0.316 | -0.797 | -1.238 | -1.735 | -2.241 | -2.757 | -3.249 | -3.572  | -3.075  |
| 0.075           | 0.072  | -0.185 | -0.482 | -0.836 | -1.199 | -1.572 | -2.000 | -2.441 | -2.777 | -2.982  | -2.657  |
| 0.100           | -0.044 | -0.281 | -0.542 | -0.842 | -1.149 | -1.531 | -1.888 | -2.236 | -2.489 | -2.639  | -2.336  |
| 0.200           | -0.203 | -0.368 | -0.544 | -0.727 | -0.988 | -1.104 | -1.314 | -1.512 | -1.652 | -1.724  | -1.340  |
| 0.300           | -0.255 | -0.380 | -0.514 | -0.633 | -0.764 | -0.908 | -1.051 | -1.179 | -1.261 | -1.304  | -1.138  |
| 0.400           | -0.246 | -0.342 | -0.451 | -0.526 | -0.625 | -0.726 | -0.823 | -0.908 | -0.959 | -0.978  | -0.902  |
| 0.500           | -0.174 | -0.227 | -0.292 | -0.370 | -0.437 | -0.509 | -0.570 | -0.619 | -0.649 | -0.657  | -0.684  |
| 0.650           | -0.103 | -0.150 | -0.196 | -0.245 | -0.288 | -0.331 | -0.367 | -0.394 | -0.403 | -0.413  | -0.613  |
| 0.750           | -0.020 | -0.030 | -0.044 | -0.057 | -0.070 | -0.084 | -0.093 | -0.101 | -0.107 | -0.089  | -0.038  |
| 0.850           | -0.022 | -0.034 | -0.052 | -0.069 | -0.081 | -0.096 | -0.100 | -0.102 | -0.109 | -0.136  | -0.437  |
| 0.950           | 0.053  | 0.058  | 0.056  | 0.052  | 0.051  | 0.043  | 0.040  | 0.091  | 0.066  | -0.057  | -0.427  |
| Lower surface   |        |        |        |        |        |        |        |        |        |         |         |
| 0.005           | -2.231 | -0.886 | -0.164 | 0.527  | 0.902  | 1.015  | 0.928  | 0.680  | 0.373  | 0.053   | 0.322   |
| 0.015           | -2.021 | -0.669 | -0.129 | 0.352  | 0.690  | 0.915  | 1.010  | 0.992  | 0.916  | 0.830   | 0.901   |
| 0.030           | 0.267  | -0.517 | -0.124 | 0.245  | 0.592  | 0.758  | 0.913  | 0.990  | 1.009  | 1.008   | 1.001   |
| 0.050           | -0.846 | -0.435 | -0.125 | 0.165  | 0.410  | 0.621  | 0.784  | 0.905  | 0.960  | 0.985   | 0.955   |
| 0.075           | -0.646 | -0.375 | -0.120 | 0.115  | 0.328  | 0.518  | 0.675  | 0.811  | 0.879  | 0.910   | 0.876   |
| 0.100           | -0.571 | -0.344 | -0.125 | 0.080  | 0.269  | 0.442  | 0.591  | 0.732  | 0.804  | 0.731   | 0.694   |
| 0.200           | -0.464 | -0.319 | -0.171 | -0.024 | 0.114  | 0.251  | 0.374  | 0.515  | 0.583  | 0.590   | 0.551   |
| 0.300           | -0.393 | -0.287 | -0.175 | -0.070 | 0.040  | 0.151  | 0.255  | 0.388  | 0.447  | 0.439   | 0.389   |
| 0.400           | -0.297 | -0.216 | -0.131 | -0.053 | 0.035  | 0.124  | 0.207  | 0.329  | 0.374  | 0.350   | 0.298   |
| 0.500           | -0.215 | -0.154 | -0.085 | -0.026 | 0.045  | 0.116  | 0.185  | 0.292  | 0.330  | 0.293   | 0.228   |
| 0.650           | -0.103 | -0.059 | -0.015 | 0.039  | 0.075  | 0.127  | 0.175  | 0.266  | 0.290  | 0.240   | 0.153   |
| 0.750           | -0.030 | 0.003  | 0.037  | 0.079  | 0.096  | 0.136  | 0.173  | 0.254  | 0.270  | 0.208   | 0.101   |
| 0.850           | 0.082  | 0.107  | 0.072  | 0.097  | 0.127  | 0.134  | 0.160  | 0.231  | 0.236  | 0.164   | 0.023   |
| 0.950           | 0.080  | 0.094  | 0.102  | 0.110  | 0.123  | 0.125  | 0.131  | 0.188  | 0.178  | 0.084   | -0.112  |

Table 19 (Contd)

Wing BP/O

$\Delta C_p$

$V = 250 \text{ ft/sec}; R = 3.2 \times 10^6$

| $\alpha$<br>X/C | -4.05° | -2.0°  | 0°     | 2.0°   | 4.05°  | 6.05°  | 8.1°   | 10.1°  | 12.15° | 14.15° | 16.15° |
|-----------------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| 0               | 0      | 0      | 0      | 0      | 0      | 0      | 0      | 0      | 0      | 0      | 0      |
| 0.005           | 3.242  | 1.781  | 0.705  | -0.631 | -1.871 | -3.145 | -4.500 | -5.834 | -6.921 | -7.152 | -7.085 |
| 0.015           | 2.799  | 1.163  | 0.191  | -0.908 | -1.971 | -3.100 | -4.126 | -5.133 | -5.991 | -6.505 | -5.940 |
| 0.030           | 1.735  | 0.681  | -0.106 | -0.985 | -1.888 | -2.720 | -3.576 | -4.353 | -5.023 | -5.431 | -5.001 |
| 0.050           | 1.092  | 0.400  | -0.251 | -0.962 | -1.648 | -2.356 | -3.025 | -3.662 | -4.209 | -4.557 | -4.030 |
| 0.075           | 0.718  | 0.190  | -0.362 | -0.951 | -1.527 | -2.090 | -2.675 | -3.252 | -3.656 | -3.892 | -3.533 |
| 0.100           | 0.527  | 0.063  | -0.417 | -0.922 | -1.418 | -1.973 | -2.479 | -2.968 | -3.293 | -3.370 | -3.030 |
| 0.200           | 0.261  | -0.049 | -0.373 | -0.703 | -1.102 | -1.355 | -1.688 | -2.027 | -2.235 | -2.314 | -1.891 |
| 0.300           | 0.138  | -0.093 | -0.339 | -0.563 | -0.804 | -1.059 | -1.306 | -1.567 | -1.708 | -1.743 | -1.527 |
| 0.400           | 0.051  | -0.126 | -0.320 | -0.473 | -0.660 | -0.850 | -1.030 | -1.237 | -1.333 | -1.328 | -1.200 |
| 0.500           | 0.041  | -0.073 | -0.207 | -0.344 | -0.482 | -0.625 | -0.755 | -0.911 | -0.979 | -0.950 | -0.912 |
| 0.650           | 0      | -0.091 | -0.181 | -0.284 | -0.363 | -0.458 | -0.542 | -0.660 | -0.693 | -0.650 | -0.766 |
| 0.750           | 0.010  | -0.033 | -0.081 | -0.136 | -0.166 | -0.220 | -0.266 | -0.355 | -0.377 | -0.297 | -0.139 |
| 0.850           | -0.104 | -0.141 | -0.124 | -0.166 | -0.208 | -0.230 | -0.260 | -0.333 | -0.345 | -0.300 | -0.460 |
| 0.950           | -0.027 | -0.036 | -0.046 | -0.058 | -0.072 | -0.082 | -0.090 | -0.097 | -0.112 | -0.141 | -0.315 |

Table-20

Wing BP/1, normal attitude

C<sub>p</sub>

V = 250 ft/sec; R = 3.2 x 10<sup>6</sup>

| $\alpha$<br>X/C | -4.3°  | -2.1°  | -1.0°  | -0.9°  | 0.05°  | 1.15°  | 2.25°  | 4.45°  | 6.6°   | 8.8°   | 10.95° | 13.15° | 15.3°  | 17.4°  | 18.45° |
|-----------------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| Upper surface   |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |
| 0               | -2.086 | -0.942 | -0.250 | -0.236 | 0.282  | 0.632  | 0.906  | 1.008  | 0.588  | -0.551 | -2.384 | -4.818 | -      | -      | -      |
| 0.005           | 1.004  | 0.893  | 0.777  | 0.762  | 0.602  | 0.419  | 0.171  | -0.437 | -1.209 | -2.154 | -3.248 | -4.483 | -      | -      | -      |
| 0.015           | 0.742  | 0.497  | 0.333  | 0.320  | 0.133  | -0.058 | -0.297 | -0.831 | -1.454 | -2.171 | -2.869 | -3.691 | -4.488 | -      | -      |
| 0.030           | 0.431  | 0.174  | 0.023  | 0.013  | -0.154 | -0.319 | -0.513 | -0.932 | -1.397 | -1.917 | -2.451 | -2.989 | -3.620 | -4.170 | -4.427 |
| 0.050           | 0.217  | -0.017 | -0.150 | -0.158 | -0.300 | -0.436 | -0.598 | -0.931 | -1.295 | -1.668 | -2.032 | -2.462 | -2.915 | -3.292 | -3.468 |
| 0.075           | 0.051  | -0.164 | -0.277 | -0.284 | -0.405 | -0.521 | -0.655 | -0.931 | -1.223 | -1.496 | -1.811 | -2.141 | -2.482 | -2.768 | -2.879 |
| 0.100           | -0.063 | -0.252 | -0.354 | -0.360 | -0.465 | -0.566 | -0.678 | -0.908 | -1.174 | -1.445 | -1.701 | -1.964 | -2.213 | -2.492 | -2.494 |
| 0.200           | -0.198 | -0.327 | -0.395 | -0.399 | -0.470 | -0.534 | -0.606 | -0.715 | -0.858 | -1.045 | -1.155 | -1.301 | -1.439 | -1.541 | -1.572 |
| 0.300           | -0.255 | -0.350 | -0.403 | -0.404 | -0.455 | -0.502 | -0.533 | -0.630 | -0.727 | -0.832 | -0.921 | -1.013 | -1.093 | -1.140 | -1.133 |
| 0.400           | -0.229 | -0.301 | -0.342 | -0.343 | -0.385 | -0.393 | -0.429 | -0.502 | -0.567 | -0.637 | -0.695 | -0.755 | -0.801 | -0.815 | -0.786 |
| 0.500           | -0.181 | -0.218 | -0.236 | -0.240 | -0.271 | -0.293 | -0.323 | -0.376 | -0.421 | -0.470 | -0.509 | -0.546 | -0.570 | -0.562 | -0.522 |
| 0.650           | -0.085 | -0.117 | -0.137 | -0.137 | -0.153 | -0.168 | -0.194 | -0.213 | -0.235 | -0.262 | -0.279 | -0.294 | -0.298 | -0.280 | -0.242 |
| 0.750           | -0.045 | -0.065 | -0.078 | -0.079 | -0.088 | -0.096 | -0.106 | -0.124 | -0.135 | -0.150 | -0.157 | -0.162 | -0.160 | -0.148 | -0.152 |
| 0.850           | -0.005 | -0.015 | -0.022 | -0.028 | -0.030 | -0.031 | -0.035 | -0.040 | -0.044 | -0.051 | -0.049 | -0.047 | -0.043 | -0.049 | -0.090 |
| 0.950           | 0.072  | 0.076  | 0.078  | 0.073  | 0.073  | 0.075  | 0.076  | 0.077  | 0.081  | 0.077  | 0.077  | 0.074  | 0.059  | -0.021 | -0.049 |
| Lower surface   |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |
| 0.005           | -2.306 | -0.919 | -0.574 | -0.572 | -0.227 | 0.048  | 0.329  | 0.732  | 0.961  | 1.013  | 0.929  | 0.715  | 0.370  | -0.044 | -0.247 |
| 0.015           | -1.496 | -0.607 | -0.367 | -0.358 | -0.149 | 0.032  | 0.228  | 0.545  | 0.783  | 0.937  | 1.007  | 1.007  | 0.942  | 0.933  | 0.755  |
| 0.030           | -0.871 | -0.444 | -0.271 | -0.264 | -0.113 | 0.008  | 0.157  | 0.412  | 0.625  | 0.789  | 0.907  | 0.981  | 1.013  | 1.008  | 0.997  |
| 0.050           | -0.664 | -0.393 | -0.256 | -0.251 | -0.129 | -0.029 | 0.090  | 0.305  | 0.494  | 0.653  | 0.781  | 0.883  | 0.955  | 0.996  | 1.004  |
| 0.075           | -0.549 | -0.334 | -0.225 | -0.222 | -0.121 | -0.045 | 0.056  | 0.238  | 0.403  | 0.549  | 0.674  | 0.778  | 0.863  | 0.980  | 0.947  |
| 0.100           | -0.491 | -0.305 | -0.212 | -0.209 | -0.122 | -0.057 | 0.028  | 0.189  | 0.339  | 0.471  | 0.590  | 0.691  | 0.783  | 0.851  | 0.877  |
| 0.200           | -0.402 | -0.283 | -0.222 | -0.219 | -0.163 | -0.114 | -0.055 | 0.061  | 0.173  | 0.278  | 0.376  | 0.466  | 0.554  | 0.627  | 0.654  |
| 0.300           | -0.337 | -0.253 | -0.204 | -0.206 | -0.163 | -0.135 | -0.089 | 0.001  | 0.091  | 0.178  | 0.258  | 0.336  | 0.414  | 0.480  | 0.505  |
| 0.400           | -0.248 | -0.184 | -0.149 | -0.149 | -0.117 | -0.101 | -0.065 | 0.006  | 0.077  | 0.145  | 0.213  | 0.277  | 0.340  | 0.397  | 0.414  |
| 0.500           | -0.170 | -0.122 | -0.094 | -0.096 | -0.070 | -0.057 | -0.027 | 0.029  | 0.085  | 0.139  | 0.194  | 0.248  | 0.299  | 0.343  | 0.358  |
| 0.650           | -0.058 | -0.026 | -0.007 | 0.020  | 0.008  | 0.029  | 0.037  | 0.071  | 0.114  | 0.153  | 0.191  | 0.230  | 0.267  | 0.297  | 0.302  |
| 0.750           | 0.009  | 0.037  | 0.052  | 0.048  | 0.061  | 0.077  | 0.081  | 0.123  | 0.131  | 0.163  | 0.193  | 0.221  | 0.241  | 0.270  | 0.270  |
| 0.850           | 0.046  | 0.063  | 0.091  | 0.071  | 0.077  | 0.090  | 0.088  | 0.119  | 0.146  | 0.148  | 0.170  | 0.190  | 0.219  | 0.217  | 0.207  |
| 0.950           | 0.100  | 0.110  | 0.114  | 0.110  | 0.114  | 0.119  | 0.110  | 0.129  | 0.142  | 0.145  | 0.151  | 0.159  | 0.159  | 0.146  | 0.115  |

Table 20 (Contd)

Wing BP/1, inverted attitude

 $C_p$  $V = 250 \text{ ft/sec}; R = 3.2 \times 10^6$ 

| $\alpha$<br>$x/c$ | $-4.0^\circ$ | $-1.85^\circ$ | $-0.75^\circ$ | $0.35^\circ$ | $1.45^\circ$ | $2.55^\circ$ | $4.7^\circ$ |
|-------------------|--------------|---------------|---------------|--------------|--------------|--------------|-------------|
| Upper surface     |              |               |               |              |              |              |             |
| 0                 | -2.023       | -0.870        | -0.164        | 0.311        | 0.604        | 0.911        | 1.001       |
| 0.005             | 1.006        | 0.884         | 0.752         | 0.590        | 0.405        | 0.167        | -0.489      |
| 0.015             | 0.739        | 0.481         | 0.304         | 0.121        | -0.077       | -0.307       | -0.883      |
| 0.030             | 0.423        | 0.158         | -0.006        | -0.167       | -0.335       | -0.525       | -0.976      |
| 0.050             | 0.209        | -0.033        | -0.176        | -0.311       | -0.451       | -0.609       | -0.974      |
| 0.075             | 0.039        | -0.177        | -0.301        | -0.420       | -0.441       | -0.671       | -0.971      |
| 0.100             | -0.073       | -0.268        | -0.379        | -0.481       | -0.585       | -0.695       | -0.946      |
| 0.200             | -0.207       | -0.343        | -0.418        | -0.486       | -0.552       | -0.623       | -0.744      |
| 0.300             | -0.265       | -0.366        | -0.421        | -0.470       | -0.521       | -0.546       | -0.654      |
| 0.400             | -0.239       | -0.315        | -0.360        | -0.398       | -0.410       | -0.442       | -0.523      |
| 0.500             | -0.191       | -0.228        | -0.251        | -0.284       | -0.312       | -0.337       | -0.396      |
| 0.650             | -0.092       | -0.128        | -0.147        | -0.164       | -0.179       | -0.193       | -0.227      |
| 0.750             | -0.061       | -0.073        | -0.086        | -0.094       | -0.104       | -0.111       | -0.133      |
| 0.850             | -0.029       | -0.032        | -0.034        | -0.039       | -0.043       | -0.047       | -0.056      |
| 0.950             | 0.063        | 0.065         | 0.064         | 0.066        | 0.065        | 0.066        | 0.064       |
| Lower surface     |              |               |               |              |              |              |             |
| 0.005             | -2.259       | -0.884        | -0.542        | -0.204       | 0.074        | 0.339        | 0.753       |
| 0.015             | -1.465       | -0.585        | -0.331        | -0.135       | 0.048        | 0.236        | 0.564       |
| 0.030             | -0.847       | -0.424        | -0.242        | -0.101       | -0.008       | 0.163        | 0.427       |
| 0.050             | -0.624       | -0.375        | -0.232        | -0.117       | -0.019       | 0.098        | 0.319       |
| 0.075             | -0.533       | -0.321        | -0.203        | -0.110       | -0.033       | 0.064        | 0.250       |
| 0.100             | -0.474       | -0.291        | -0.192        | -0.113       | -0.049       | 0.038        | 0.201       |
| 0.200             | -0.388       | -0.272        | -0.206        | -0.152       | -0.105       | -0.056       | 0.070       |
| 0.300             | -0.327       | -0.243        | -0.193        | -0.153       | -0.128       | -0.081       | 0.010       |
| 0.400             | -0.238       | -0.176        | -0.141        | -0.109       | -0.096       | -0.058       | 0.011       |
| 0.500             | -0.163       | -0.116        | -0.088        | -0.064       | -0.050       | -0.020       | 0.033       |
| 0.650             | -0.053       | -0.024        | -0.004        | 0.011        | 0.030        | 0.053        | 0.073       |
| 0.750             | 0.010        | 0.033         | 0.048         | 0.059        | 0.075        | 0.091        | 0.122       |
| 0.850             | 0.045        | 0.058         | 0.070         | 0.076        | 0.087        | 0.097        | 0.117       |
| 0.950             | 0.096        | 0.103         | 0.108         | 0.110        | 0.114        | 0.120        | 0.124       |

Table 20 (Contd)

Wing BP/1, normal attitude

 $\Delta C_p$  $V = 250 \text{ ft/sec}; R = 3.2 \times 10^6$ 

| $\alpha$<br>x/c | $-4.3^\circ$ | $-2.1^\circ$ | $-1.0^\circ$ | $-0.9^\circ$ | $0.05^\circ$ | $1.15^\circ$ | $2.25^\circ$ |
|-----------------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|
| 0               | 0            | 0            | 0            | 0            | 0            | 0            | 0            |
| 0.005           | 3.310        | 1.812        | 1.351        | 1.334        | 0.829        | 0.467        | -0.158       |
| 0.015           | 2.238        | 1.104        | 0.700        | 0.678        | 0.282        | -0.026       | -0.525       |
| 0.030           | 1.302        | 0.618        | 0.294        | 0.277        | -0.041       | -0.327       | -0.670       |
| 0.050           | 0.881        | 0.376        | 0.106        | 0.093        | -0.171       | -0.407       | -0.688       |
| 0.075           | 0.600        | 0.170        | -0.052       | -0.062       | -0.284       | -0.476       | -0.711       |
| 0.100           | 0.428        | 0.050        | -0.142       | -0.151       | -0.343       | -0.509       | -0.706       |
| 0.200           | 0.204        | -0.044       | -0.173       | -0.180       | -0.307       | -0.420       | -0.551       |
| 0.300           | 0.082        | -0.097       | -0.199       | -0.198       | -0.292       | -0.367       | -0.444       |
| 0.400           | 0.019        | -0.117       | -0.193       | -0.194       | -0.268       | -0.292       | -0.364       |
| 0.500           | -0.011       | -0.096       | -0.142       | -0.144       | -0.201       | -0.241       | -0.296       |
| 0.650           | -0.027       | -0.091       | -0.130       | -0.157       | -0.161       | -0.197       | -0.231       |
| 0.750           | -0.054       | -0.102       | -0.130       | -0.127       | -0.149       | -0.173       | -0.187       |
| 0.850           | -0.051       | -0.078       | -0.113       | -0.099       | -0.107       | -0.121       | -0.123       |
| 0.950           | -0.028       | -0.034       | -0.036       | -0.037       | -0.041       | -0.044       | -0.034       |

Wing BP/1, inverted attitude

 $\Delta C_p$  $V = 250 \text{ ft/sec}; R = 3.2 \times 10^6$ 

| $\alpha$<br>x/c | $-4.0^\circ$ | $-1.85^\circ$ | $-0.75^\circ$ | $0.35^\circ$ | $1.45^\circ$ | $2.55^\circ$ | $4.7^\circ$ |
|-----------------|--------------|---------------|---------------|--------------|--------------|--------------|-------------|
| 0               | 0            | 0             | 0             | 0            | 0            | 0            | 0           |
| 0.005           | 3.265        | 1.768         | 1.294         | 0.794        | 0.331        | -0.172       | -1.242      |
| 0.015           | 2.204        | 1.066         | 0.635         | 0.256        | -0.125       | -0.543       | -1.447      |
| 0.030           | 1.270        | 0.582         | 0.236         | -0.066       | -0.327       | -0.688       | -1.403      |
| 0.050           | 0.833        | 0.342         | 0.056         | -0.194       | -0.432       | -0.707       | -1.293      |
| 0.075           | 0.572        | 0.144         | -0.098        | -0.310       | -0.408       | -0.735       | -1.221      |
| 0.100           | 0.401        | 0.023         | -0.187        | -0.368       | -0.536       | -0.733       | -1.147      |
| 0.200           | 0.181        | -0.071        | -0.212        | -0.334       | -0.447       | -0.567       | -0.814      |
| 0.300           | 0.062        | -0.123        | -0.228        | -0.317       | -0.393       | -0.465       | -0.664      |
| 0.400           | -0.001       | -0.139        | -0.219        | -0.289       | -0.314       | -0.384       | -0.534      |
| 0.500           | -0.028       | -0.112        | -0.163        | -0.220       | -0.262       | -0.317       | -0.429      |
| 0.650           | -0.039       | -0.104        | -0.143        | -0.175       | -0.209       | -0.246       | -0.300      |
| 0.750           | -0.071       | -0.106        | -0.134        | -0.153       | -0.179       | -0.202       | -0.255      |
| 0.850           | -0.074       | -0.090        | -0.104        | -0.115       | -0.130       | -0.144       | -0.173      |
| 0.950           | -0.033       | -0.038        | -0.044        | -0.044       | -0.049       | -0.054       | -0.060      |



Table 21

V = 250 ft/sec; R = 3.2 x 10<sup>6</sup>

Wing BP/2, normal attitude

C<sub>p</sub>

| $\alpha$<br>X/C | -4.7°  | -2.1°  | 0°     | 2.1°   | 4.15°  | 6.25°  | 8.35°  | 10.45° | 12.5°  | 14.6°  | 16.65° | 18.75°  | 19.75°  | 20.8°   |
|-----------------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|---------|---------|---------|
| Upper surface   |        |        |        |        |        |        |        |        |        |        |        |         |         |         |
| 0               | -2.183 | -0.999 | -0.037 | 0.760  | 1.013  | 0.922  | 0.332  | -0.837 | -2.369 | -4.425 | -7.203 | -10.166 | -11.396 | -13.048 |
| 0.005           | 1.005  | 0.938  | 0.692  | 0.324  | -0.099 | -0.658 | -1.347 | -2.159 | -3.069 | -4.055 | -5.192 | -6.367  | -6.850  | -7.362  |
| 0.015           | 0.743  | 0.487  | 0.242  | -0.145 | -0.534 | -1.009 | -1.557 | -2.177 | -2.779 | -3.350 | -4.022 | -4.285  | -5.030  | -5.493  |
| 0.030           | 0.422  | 0.155  | -0.071 | -0.404 | -0.712 | -1.072 | -1.476 | -1.919 | -2.372 | -2.790 | -3.314 | -3.771  | -3.952  | -4.158  |
| 0.050           | 0.209  | -0.032 | -0.227 | -0.505 | -0.749 | -1.034 | -1.347 | -1.663 | -1.966 | -2.298 | -2.670 | -2.996  | -3.162  | -3.272  |
| 0.075           | 0.042  | -0.171 | -0.342 | -0.576 | -0.777 | -1.007 | -1.258 | -1.471 | -1.744 | -1.988 | -2.269 | -2.506  | -2.595  | -2.699  |
| 0.100           | -0.105 | -0.254 | -0.402 | -0.603 | -0.771 | -0.963 | -1.206 | -1.396 | -1.613 | -1.804 | -2.013 | -2.185  | -2.246  | -2.316  |
| 0.200           | -0.201 | -0.330 | -0.425 | -0.550 | -0.626 | -0.733 | -0.850 | -0.965 | -1.086 | -1.185 | -1.294 | -1.381  | -1.410  | -1.436  |
| 0.300           | -0.256 | -0.349 | -0.418 | -0.499 | -0.555 | -0.629 | -0.702 | -0.783 | -0.842 | -0.907 | -0.970 | -1.011  | -1.023  | -1.022  |
| 0.400           | -0.228 | -0.297 | -0.349 | -0.393 | -0.436 | -0.486 | -0.535 | -0.587 | -0.622 | -0.663 | -0.693 | -0.716  | -0.715  | -0.701  |
| 0.500           | -0.180 | -0.204 | -0.243 | -0.289 | -0.324 | -0.356 | -0.386 | -0.422 | -0.444 | -0.468 | -0.484 | -0.492  | -0.485  | -0.464  |
| 0.650           | -0.081 | -0.111 | -0.133 | -0.156 | -0.173 | -0.189 | -0.203 | -0.222 | -0.231 | -0.240 | -0.241 | -0.239  | -0.231  | -0.213  |
| 0.750           | -0.037 | -0.055 | -0.070 | -0.080 | -0.089 | -0.097 | -0.104 | -0.116 | -0.117 | -0.120 | -0.116 | -0.111  | -0.108  | -0.110  |
| 0.850           | 0.001  | -0.007 | -0.013 | -0.017 | -0.020 | -0.020 | -0.019 | -0.024 | -0.021 | -0.019 | -0.012 | -0.013  | -0.018  | -0.041  |
| 0.950           | 0.084  | 0.088  | 0.087  | 0.090  | 0.091  | 0.094  | 0.096  | 0.095  | 0.096  | 0.103  | 0.088  | 0.063   | 0.046   | 0.005   |
| Lower surface   |        |        |        |        |        |        |        |        |        |        |        |         |         |         |
| 0.005           | -2.112 | -0.817 | -0.376 | 0.211  | 0.584  | 0.849  | 0.986  | 1.018  | 0.954  | 0.804  | 0.560  | 0.261   | 0.130   | -0.052  |
| 0.015           | -1.456 | -0.590 | -0.265 | 0.118  | 0.392  | 0.618  | 0.812  | 0.946  | 1.002  | 1.014  | 0.977  | 0.892   | 0.849   | 0.786   |
| 0.030           | -0.774 | -0.458 | -0.222 | 0.066  | 0.279  | 0.477  | 0.647  | 0.794  | 0.888  | 0.963  | 1.008  | 1.016   | 1.015   | 1.008   |
| 0.050           | -0.623 | -0.371 | -0.189 | 0.024  | 0.199  | 0.367  | 0.521  | 0.661  | 0.764  | 0.855  | 0.932  | 0.974   | 0.987   | 1.004   |
| 0.075           | -0.525 | -0.317 | -0.170 | -0.001 | 0.145  | 0.290  | 0.426  | 0.553  | 0.656  | 0.750  | 0.836  | 0.892   | 0.913   | 0.939   |
| 0.100           | -0.473 | -0.294 | -0.168 | -0.021 | 0.106  | 0.234  | 0.356  | 0.475  | 0.570  | 0.662  | 0.750  | 0.814   | 0.836   | 0.864   |
| 0.200           | -0.382 | -0.271 | -0.191 | -0.091 | -0.003 | 0.089  | 0.179  | 0.274  | 0.353  | 0.432  | 0.513  | 0.577   | 0.602   | 0.632   |
| 0.300           | -0.316 | -0.243 | -0.181 | -0.120 | -0.054 | 0.017  | 0.090  | 0.167  | 0.231  | 0.300  | 0.372  | 0.428   | 0.451   | 0.479   |
| 0.400           | -0.228 | -0.173 | -0.130 | -0.088 | -0.039 | 0.015  | 0.071  | 0.133  | 0.186  | 0.242  | 0.301  | 0.349   | 0.369   | 0.392   |
| 0.500           | -0.152 | -0.110 | -0.081 | -0.049 | -0.012 | 0.031  | 0.074  | 0.125  | 0.169  | 0.213  | 0.262  | 0.301   | 0.318   | 0.335   |
| 0.650           | -0.049 | -0.022 | -0.004 | 0.030  | 0.050  | 0.067  | 0.098  | 0.137  | 0.168  | 0.199  | 0.235  | 0.262   | 0.274   | 0.284   |
| 0.750           | 0.018  | 0.038  | 0.051  | 0.078  | 0.094  | 0.113  | 0.117  | 0.151  | 0.174  | 0.199  | 0.224  | 0.245   | 0.254   | 0.257   |
| 0.850           | 0.053  | 0.071  | 0.078  | 0.094  | 0.101  | 0.117  | 0.129  | 0.144  | 0.162  | 0.177  | 0.196  | 0.205   | 0.210   | 0.205   |
| 0.950           | 0.108  | 0.118  | 0.120  | 0.127  | 0.126  | 0.131  | 0.142  | 0.148  | 0.153  | 0.157  | 0.161  | 0.205   | 0.210   | 0.130   |

Table 21 (Contd.)

Wing BP/2, normal attitude

 $\Delta C_p$ V = 250 ft/sec; R =  $3.2 \times 10^6$ 

| $\chi/c$ | $\alpha$ | $-4.7^\circ$ | $-2.1^\circ$ | $0^\circ$ | $2.1^\circ$ | $4.15^\circ$ | $6.25^\circ$ | $8.35^\circ$ | $10.45^\circ$ | $12.5^\circ$ | $14.6^\circ$ | $16.65^\circ$ | $18.75^\circ$ | $19.75^\circ$ | $20.8^\circ$ |
|----------|----------|--------------|--------------|-----------|-------------|--------------|--------------|--------------|---------------|--------------|--------------|---------------|---------------|---------------|--------------|
| 0        | 0        | 0            | 0            | 0         | 0           | 0            | 0            | 0            | 0             | 0            | 0            | 0             | 0             | 0             | 0            |
| 0.005    |          | 3.117        | 1.755        | 1.068     | 0.113       | -0.683       | -1.507       | -2.333       | -3.177        | -4.023       | -4.859       | -5.752        | -6.628        | -6.980        | -7.310       |
| 0.015    |          | 2.202        | 1.077        | 0.507     | -0.263      | -0.926       | -1.627       | -2.369       | -3.123        | -3.781       | -4.364       | -4.999        | -5.177        | -5.879        | -6.279       |
| 0.030    |          | 1.196        | 0.613        | 0.151     | -0.470      | -0.991       | -1.549       | -2.123       | -2.713        | -3.260       | -3.753       | -4.322        | -4.787        | -4.967        | -5.166       |
| 0.050    |          | 0.832        | 0.339        | -0.038    | -0.529      | -0.948       | -1.401       | -1.868       | -2.324        | -2.730       | -3.153       | -3.602        | -3.970        | -4.149        | -4.276       |
| 0.075    |          | 0.567        | 0.146        | -0.172    | -0.575      | -0.922       | -1.297       | -1.684       | -2.024        | -2.400       | -2.738       | -3.105        | -3.398        | -3.508        | -3.638       |
| 0.100    |          | 0.368        | 0.040        | -0.234    | -0.582      | -0.877       | -1.197       | -1.562       | -1.871        | -2.183       | -2.466       | -2.763        | -2.999        | -3.082        | -3.180       |
| 0.200    |          | 0.181        | -0.059       | -0.234    | -0.459      | -0.623       | -0.822       | -1.029       | -1.239        | -1.439       | -1.617       | -1.807        | -1.958        | -2.012        | -2.068       |
| 0.300    |          | 0.060        | -0.106       | -0.237    | -0.379      | -0.501       | -0.646       | -0.792       | -0.950        | -1.013       | -1.207       | -1.342        | -1.439        | -1.474        | -1.501       |
| 0.400    |          | 0            | -0.124       | -0.219    | -0.305      | -0.397       | -0.501       | -0.606       | -0.720        | -0.808       | -0.905       | -0.994        | -1.065        | -1.084        | -1.093       |
| 0.500    |          | -0.028       | -0.094       | -0.162    | -0.240      | -0.312       | -0.387       | -0.460       | -0.547        | -0.613       | -0.681       | -0.746        | -0.793        | -0.803        | -0.799       |
| 0.650    |          | -0.033       | -0.089       | -0.129    | -0.186      | -0.223       | -0.256       | -0.301       | -0.359        | -0.399       | -0.439       | -0.476        | -0.501        | -0.505        | -0.497       |
| 0.750    |          | -0.055       | -0.093       | -0.121    | -0.158      | -0.183       | -0.210       | -0.221       | -0.267        | -0.291       | -0.319       | -0.340        | -0.356        | -0.362        | -0.367       |
| 0.850    |          | -0.052       | -0.064       | -0.091    | -0.111      | -0.111       | -0.137       | -0.148       | -0.168        | -0.183       | -0.196       | -0.208        | -0.218        | -0.228        | -0.246       |
| 0.950    |          | -0.024       | -0.030       | -0.033    | -0.037      | -0.037       | -0.037       | -0.046       | -0.053        | -0.057       | -0.054       | -0.073        | -0.091        | -0.101        | -0.125       |

Table 22

Wing BP/3, normal attitude

 $C_p$  $V = 250 \text{ ft/sec}; R = 3.2 \times 10^6$ 

| $\alpha$<br>$^\circ/C$ | -6.35° | -5.35° | -4.3°  | -3.3°  | -2.3°  | -1.3°  | -0.25° | 0.75°  | 1.75°  | 3.8°   | 5.8°   | 7.85°  | 9.9°   | 11.9°  | 13.95° | 15.95° | 18.0°  | 20.0°  | 22.05° |
|------------------------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| Upper surface          |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |
| 0                      | -1.736 | -1.282 | -0.844 | -0.451 | -0.157 | 0.213  | 0.430  | 0.631  | 0.808  | 1.003  | 1.028  | 0.862  | 0.470  | -0.163 | -1.053 | -2.174 | -3.588 | -5.050 | -6.807 |
| 0.005                  | 1.045  | 1.024  | 1.004  | 0.957  | 0.933  | 0.826  | 0.717  | 0.590  | 0.495  | 0.184  | -0.178 | -0.637 | -1.134 | -1.617 | -2.381 | -3.116 | -3.947 | -4.638 | -5.371 |
| 0.015                  | -      | -      | -      | -      | -      | -      | -      | -      | -      | -      | -      | -      | -      | -      | -      | -      | -      | -      | -      |
| 0.030                  | 0.470  | 0.409  | 0.338  | 0.245  | 0.164  | 0.055  | -0.036 | -0.149 | -0.233 | -0.477 | -0.719 | -0.985 | -1.219 | -1.499 | -1.844 | -2.203 | -2.513 | -2.837 | -3.209 |
| 0.050                  | 0.277  | 0.210  | 0.139  | 0.064  | -0.003 | -0.099 | -0.176 | -0.263 | -0.348 | -0.537 | -0.729 | -0.940 | -1.109 | -1.335 | -1.546 | -1.767 | -2.015 | -2.253 | -2.512 |
| 0.075                  | 0.098  | 0.035  | -0.030 | -0.096 | -0.151 | -0.235 | -0.301 | -0.375 | -0.445 | -0.603 | -0.755 | -0.925 | -1.055 | -1.224 | -1.385 | -1.566 | -1.749 | -1.919 | -2.102 |
| 0.100                  | 0      | -0.059 | -0.115 | -0.172 | -0.220 | -0.293 | -0.350 | -0.413 | -0.472 | -0.604 | -0.731 | -0.875 | -0.987 | -1.111 | -1.247 | -1.389 | -1.530 | -1.669 | -1.805 |
| 0.200                  | -0.168 | -0.207 | -0.242 | -0.281 | -0.308 | -0.353 | -0.389 | -0.425 | -0.459 | -0.536 | -0.579 | -0.654 | -0.725 | -0.798 | -0.865 | -0.934 | -1.002 | -1.064 | -1.128 |
| 0.300                  | -0.236 | -0.261 | -0.287 | -0.309 | -0.331 | -0.361 | -0.384 | -0.406 | -0.429 | -0.473 | -0.507 | -0.552 | -0.592 | -0.638 | -0.672 | -0.710 | -0.750 | -0.782 | -0.816 |
| 0.400                  | -0.207 | -0.224 | -0.242 | -0.257 | -0.274 | -0.294 | -0.311 | -0.328 | -0.339 | -0.341 | -0.368 | -0.397 | -0.422 | -0.448 | -0.469 | -0.492 | -0.516 | -0.535 | -0.556 |
| 0.500                  | -0.164 | -0.177 | -0.190 | -0.193 | -0.191 | -0.194 | -0.208 | -0.219 | -0.231 | -0.253 | -0.268 | -0.285 | -0.298 | -0.313 | -0.327 | -0.341 | -0.356 | -0.367 | -0.380 |
| 0.650                  | -0.050 | -0.059 | -0.070 | -0.074 | -0.082 | -0.089 | -0.093 | -0.096 | -0.102 | -0.111 | -0.119 | -0.127 | -0.133 | -0.141 | -0.149 | -0.157 | -0.167 | -0.174 | -0.182 |
| 0.750                  | -0.039 | -0.042 | -0.045 | -0.047 | -0.051 | -0.052 | -0.056 | -0.054 | -0.056 | -0.060 | -0.059 | -0.061 | -0.064 | -0.066 | -0.070 | -0.072 | -0.149 | -0.082 | -0.086 |
| 0.850                  | 0.009  | 0.006  | 0.006  | 0.007  | 0.003  | 0.004  | 0.002  | 0.006  | 0.004  | 0.006  | 0.008  | 0.008  | 0.007  | 0.008  | 0.006  | 0.006  | 0.004  | -0.008 | 0      |
| 0.950                  | 0.075  | 0.076  | 0.077  | 0.079  | 0.078  | 0.079  | 0.081  | 0.088  | 0.087  | 0.087  | 0.093  | 0.096  | 0.097  | 0.098  | 0.097  | 0.095  | 0.093  | 0.092  | 0.083  |
| Lower surface          |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |
| 0.005                  | -2.464 | -2.110 | -1.779 | -1.462 | -1.233 | -0.873 | -0.578 | -0.304 | -0.085 | 0.325  | 0.629  | 0.847  | 0.973  | 1.013  | 0.990  | 0.890  | 0.710  | 0.470  | 0.148  |
| 0.015                  | -1.255 | -1.082 | -0.917 | -0.752 | -0.634 | -0.447 | -0.329 | -0.170 | -0.052 | 0.197  | 0.407  | 0.596  | 0.744  | 0.867  | 0.950  | 1.000  | 1.013  | 0.998  | 0.950  |
| 0.030                  | -0.913 | -0.794 | -0.679 | -0.561 | -0.482 | -0.347 | -0.261 | -0.150 | -0.058 | 0.126  | 0.294  | 0.450  | 0.584  | 0.707  | 0.806  | 0.888  | 0.949  | 0.988  | 1.000  |
| 0.050                  | -0.725 | -0.640 | -0.554 | -0.467 | -0.407 | -0.305 | -0.238 | -0.149 | -0.077 | 0.072  | 0.209  | 0.342  | 0.458  | 0.569  | 0.669  | 0.758  | 0.833  | 0.894  | 0.944  |
| 0.075                  | -0.590 | -0.506 | -0.463 | -0.397 | -0.350 | -0.271 | -0.219 | -0.143 | -0.090 | 0.032  | 0.146  | 0.258  | 0.359  | 0.460  | 0.552  | 0.641  | 0.718  | 0.786  | 0.847  |
| 0.100                  | -0.502 | -0.449 | -0.396 | -0.340 | -0.303 | -0.240 | -0.195 | -0.139 | -0.093 | 0.010  | 0.109  | 0.208  | 0.296  | 0.387  | 0.473  | 0.555  | 0.631  | 0.678  | 0.737  |
| 0.200                  | -0.385 | -0.358 | -0.327 | -0.295 | -0.274 | -0.237 | -0.208 | -0.171 | -0.143 | -0.077 | -0.009 | 0.060  | 0.123  | 0.193  | 0.258  | 0.327  | 0.394  | 0.455  | 0.518  |
| 0.300                  | -0.316 | -0.298 | -0.279 | -0.258 | -0.246 | -0.222 | -0.204 | -0.176 | -0.159 | -0.110 | -0.062 | -0.012 | 0.037  | 0.089  | 0.143  | 0.271  | 0.256  | 0.311  | 0.365  |
| 0.400                  | -0.211 | -0.201 | -0.188 | -0.174 | -0.165 | -0.153 | -0.139 | -0.128 | -0.114 | -0.082 | -0.045 | -0.009 | 0.028  | 0.070  | 0.111  | 0.157  | 0.203  | 0.249  | 0.294  |
| 0.500                  | -0.140 | -0.131 | -0.125 | -0.117 | -0.113 | -0.105 | -0.097 | -0.081 | -0.073 | -0.045 | -0.017 | 0.010  | 0.037  | 0.069  | 0.101  | 0.138  | 0.176  | 0.214  | 0.252  |
| 0.650                  | -0.021 | -0.018 | -0.014 | -0.007 | -0.006 | -0.001 | 0.002  | 0.010  | 0.017  | 0.035  | 0.045  | 0.057  | 0.077  | 0.097  | 0.120  | 0.149  | 0.175  | 0.203  | 0.231  |
| 0.750                  | 0.038  | 0.040  | 0.043  | 0.048  | 0.049  | 0.051  | 0.055  | 0.061  | 0.064  | 0.076  | 0.126  | 0.110  | 0.103  | 0.116  | 0.135  | 0.157  | 0.179  | 0.201  | 0.224  |
| 0.850                  | 0.056  | 0.057  | 0.059  | 0.064  | 0.063  | 0.065  | 0.066  | 0.069  | 0.070  | 0.076  | 0.086  | 0.095  | 0.106  | 0.118  | 0.127  | 0.147  | 0.162  | 0.179  | 0.196  |
| 0.950                  | 0.096  | 0.097  | 0.098  | 0.100  | 0.100  | 0.100  | 0.101  | 0.101  | 0.099  | 0.101  | 0.104  | 0.108  | 0.111  | 0.116  | 0.123  | 0.137  | 0.143  | 0.151  | 0.158  |

Table 22 (Contd)

Wing BP/3, Inverted attitude  $C_p$   $V = 250 \text{ ft/sec}; R = 3.2 \times 10^6$ 

| $\alpha$<br>$\chi/C$ | $-5.75^\circ$ | $-4.75^\circ$ | $-3.75^\circ$ | $-2.7^\circ$ | $-1.7^\circ$ | $-0.7^\circ$ | $0.3^\circ$ | $1.35^\circ$ | $2.35^\circ$ | $4.4^\circ$ | $6.4^\circ$ |
|----------------------|---------------|---------------|---------------|--------------|--------------|--------------|-------------|--------------|--------------|-------------|-------------|
| 0                    | -1.647        | -1.168        | -0.731        | -0.360       | -0.030       | 0.259        | 0.508       | 0.701        | 0.848        | 1.002       | 0.966       |
| 0.005                | 1.013         | 0.999         | 0.969         | 0.921        | 0.929        | 0.778        | 0.679       | 0.564        | 0.434        | 0.111       | -0.289      |
| 0.015                | 0.771         | 0.699         | 0.619         | 0.535        | 0.445        | 0.342        | 0.232       | 0.112        | -0.013       | -0.298      | -0.629      |
| 0.030                | 0.473         | 0.384         | 0.295         | 0.210        | 0.123        | 0.024        | -0.078      | -0.185       | -0.294       | -0.532      | -0.793      |
| 0.050                | 0.260         | 0.184         | 0.107         | 0.030        | -0.045       | -0.129       | -0.210      | -0.302       | -0.389       | -0.580      | -0.785      |
| 0.075                | 0.082         | 0.012         | -0.055        | -0.123       | -0.187       | -0.260       | -0.332      | -0.408       | -0.480       | -0.634      | -0.800      |
| 0.100                | -0.017        | -0.076        | -0.138        | -0.199       | -0.253       | -0.315       | -0.376      | -0.440       | -0.503       | -0.631      | -0.767      |
| 0.200                | -0.184        | -0.223        | -0.269        | -0.299       | -0.335       | -0.372       | -0.405      | -0.445       | -0.481       | -0.546      | -0.602      |
| 0.300                | -0.249        | -0.277        | -0.304        | -0.330       | -0.353       | -0.377       | -0.398      | -0.425       | -0.455       | -0.485      | -0.525      |
| 0.400                | -0.220        | -0.241        | -0.261        | -0.277       | -0.293       | -0.311       | -0.325      | -0.347       | -0.356       | -0.356      | -0.388      |
| 0.500                | -0.178        | -0.192        | -0.208        | -0.210       | -0.205       | -0.212       | -0.220      | -0.236       | -0.247       | -0.266      | -0.285      |
| 0.650                | -0.062        | -0.075        | -0.085        | -0.092       | -0.098       | -0.104       | -0.104      | -0.111       | -0.117       | -0.126      | -0.137      |
| 0.750                | -0.055        | -0.058        | -0.063        | -0.065       | -0.069       | -0.070       | -0.069      | -0.072       | -0.075       | -0.075      | -0.076      |
| 0.850                | -0.007        | -0.012        | -0.013        | -0.014       | -0.015       | -0.015       | -0.010      | -0.013       | -0.013       | -0.013      | -0.010      |
| 0.950                | 0.060         | 0.059         | 0.061         | 0.061        | 0.062        | 0.063        | 0.062       | 0.069        | 0.069        | 0.073       | 0.076       |
| 0.005                | -2.336        | -2.005        | -1.675        | -1.383       | -1.099       | -0.795       | -0.484      | -0.234       | -0.014       | 0.381       | 0.671       |
| 0.015                | -1.209        | -1.035        | -0.867        | -0.707       | -0.559       | -0.417       | -0.270      | -0.132       | -0.009       | 0.303       | 0.422       |
| 0.030                | -0.880        | -0.762        | -0.644        | -0.533       | -0.429       | -0.322       | -0.226      | -0.123       | -0.030       | 0.155       | 0.324       |
| 0.050                | -0.699        | -0.615        | -0.529        | -0.446       | -0.367       | -0.286       | -0.211      | -0.125       | -0.053       | 0.094       | 0.233       |
| 0.075                | -0.574        | -0.508        | -0.444        | -0.371       | -0.320       | -0.256       | -0.198      | -0.127       | -0.069       | 0.051       | 0.167       |
| 0.100                | -0.486        | -0.434        | -0.381        | -0.328       | -0.278       | -0.227       | -0.176      | -0.124       | -0.075       | 0.027       | 0.125       |
| 0.200                | -0.376        | -0.349        | -0.318        | -0.288       | -0.260       | -0.229       | -0.198      | -0.162       | -0.131       | -0.065      | 0.005       |
| 0.300                | -0.312        | -0.294        | -0.275        | -0.255       | -0.238       | -0.219       | -0.198      | -0.171       | -0.150       | -0.102      | -0.053      |
| 0.400                | -0.208        | -0.197        | -0.186        | -0.172       | -0.161       | -0.150       | -0.132      | -0.124       | -0.110       | -0.074      | -0.039      |
| 0.500                | -0.140        | -0.133        | -0.126        | -0.119       | -0.112       | -0.104       | -0.091      | -0.080       | -0.067       | -0.040      | -0.012      |
| 0.650                | -0.023        | -0.022        | -0.017        | -0.013       | -0.010       | -0.006       | 0           | 0.008        | 0.017        | 0.037       | 0.042       |
| 0.750                | 0.034         | 0.034         | 0.037         | 0.041        | 0.044        | 0.046        | 0.054       | 0.058        | 0.064        | 0.077       | 0.093       |
| 0.850                | 0.051         | 0.051         | 0.051         | 0.055        | 0.056        | 0.058        | 0.063       | 0.063        | 0.066        | 0.075       | 0.083       |
| 0.950                | 0.086         | 0.086         | 0.086         | 0.087        | 0.088        | 0.088        | 0.090       | 0.088        | 0.090        | 0.093       | 0.095       |

Table 22 (Contd)

Wing BP/3, normal attitude

$\Delta C_p$

V = 250 ft/sec; R = 3.2 x 10<sup>6</sup>

| $\alpha$<br>X/C | -6.35° | -5.35° | -4.3°  | -3.3°  | -2.3°  | -1.3°  | -0.25° | 0.75°  | 1.75°  | 3.8°   | 5.8°   | 7.85°  | 9.9°   | 11.9°  | 13.95° | 15.95° | 18.0°  | 20.0°  | 22.05° |
|-----------------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| 0               | 0      | 0      | 0      | 0      | 0      | 0      | 0      | 0      | 0      | 0      | 0      | 0      | 0      | 0      | 0      | 0      | 0      | 0      | 0      |
| 0.005           | 3.509  | 3.134  | 2.783  | 2.419  | 2.166  | 1.699  | 1.295  | 0.894  | 0.580  | -0.141 | -0.807 | -1.484 | -2.107 | -2.630 | -3.371 | -4.116 | -4.657 | -5.108 | -5.519 |
| 0.015           | -      | -      | -      | -      | -      | -      | -      | -      | -      | -      | -      | -      | -      | -      | -      | -      | -      | -      | -      |
| 0.030           | 1.383  | 1.203  | 1.017  | 0.806  | 0.646  | 0.402  | 0.225  | 0.001  | -0.175 | -0.603 | -1.013 | -1.435 | -1.803 | -2.206 | -2.650 | -3.091 | -3.462 | -3.825 | -4.209 |
| 0.050           | 1.002  | 0.850  | 0.693  | 0.531  | 0.404  | 0.206  | 0.062  | -0.114 | -0.271 | -0.609 | -0.938 | -1.282 | -1.567 | -1.904 | -2.215 | -2.525 | -2.848 | -3.147 | -3.456 |
| 0.075           | 0.688  | 0.541  | 0.433  | 0.301  | 0.199  | 0.036  | -0.082 | -0.232 | -0.355 | -0.635 | -0.901 | -1.183 | -1.414 | -1.684 | -1.937 | -2.207 | -2.467 | -2.705 | -2.949 |
| 0.100           | 0.502  | 0.390  | 0.281  | 0.168  | 0.083  | -0.053 | -0.155 | -0.274 | -0.379 | -0.614 | -0.840 | -1.083 | -1.283 | -1.498 | -1.720 | -1.944 | -2.161 | -2.347 | -2.542 |
| 0.200           | 0.217  | 0.151  | 0.085  | 0.014  | 0.034  | -0.116 | -0.181 | -0.254 | -0.316 | -0.459 | -0.570 | -0.714 | -0.848 | -0.991 | -1.123 | -1.261 | -1.396 | -1.519 | -1.646 |
| 0.300           | 0.080  | 0.037  | 0.008  | -0.051 | -0.085 | -0.139 | -0.180 | -0.230 | -0.270 | -0.363 | -0.445 | -0.540 | -0.629 | -0.727 | -0.815 | -0.981 | -1.006 | -1.039 | -1.181 |
| 0.400           | 0.004  | -0.023 | -0.054 | -0.083 | -0.109 | -0.141 | -0.172 | -0.200 | -0.225 | -0.259 | -0.323 | -0.388 | -0.450 | -0.518 | -0.580 | -0.649 | -0.719 | -0.784 | -0.850 |
| 0.500           | -0.024 | -0.046 | -0.065 | -0.076 | -0.078 | -0.089 | -0.111 | -0.138 | -0.158 | -0.208 | -0.251 | -0.295 | -0.335 | -0.382 | -0.428 | -0.479 | -0.532 | -0.581 | -0.632 |
| 0.650           | -0.029 | -0.041 | -0.056 | -0.067 | -0.076 | -0.088 | -0.095 | -0.106 | -0.119 | -0.146 | -0.164 | -0.184 | -0.210 | -0.238 | -0.269 | -0.306 | -0.342 | -0.377 | -0.413 |
| 0.750           | -0.077 | -0.082 | -0.088 | -0.095 | -0.100 | -0.103 | -0.111 | -0.115 | -0.120 | -0.136 | -0.185 | -0.171 | -0.167 | -0.182 | -0.205 | -0.229 | -0.328 | -0.283 | -0.310 |
| 0.850           | -0.047 | -0.051 | -0.053 | -0.057 | -0.060 | -0.061 | -0.064 | -0.063 | -0.064 | -0.070 | -0.078 | -0.087 | -0.099 | -0.110 | -0.121 | -0.141 | -0.158 | -0.187 | -0.196 |
| 0.950           | -0.021 | -0.021 | -0.021 | -0.021 | -0.022 | -0.021 | -0.020 | -0.013 | -0.012 | -0.014 | -0.011 | -0.012 | -0.014 | -0.018 | -0.026 | -0.042 | -0.050 | -0.059 | -0.075 |

Wing BP/3, inverted attitude

$\Delta C_p$

V = 250 ft/sec; R = 3.2 x 10<sup>6</sup>

| $\alpha$<br>X/C | -5.75° | -4.75° | -3.75° | -2.7°  | -1.7°  | -0.7°  | 0.3°   | 1.35°  | 2.35°  | 4.4°   | 6.4°   |
|-----------------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| 0               | 0      | 0      | 0      | 0      | 0      | 0      | 0      | 0      | 0      | 0      | 0      |
| 0.005           | 3.349  | 3.004  | 2.644  | 2.304  | 2.028  | 1.573  | 1.163  | 0.798  | 0.448  | -0.270 | -0.966 |
| 0.015           | 1.980  | 1.734  | 1.486  | 1.242  | 1.004  | 0.759  | 0.502  | 0.244  | -0.004 | -0.601 | -1.051 |
| 0.030           | 1.353  | 1.146  | 0.939  | 0.743  | 0.552  | 0.346  | 0.148  | -0.062 | -0.264 | -0.687 | -1.117 |
| 0.050           | 0.959  | 0.799  | 0.636  | 0.476  | 0.322  | 0.157  | 0.001  | -0.177 | -0.336 | -0.674 | -1.018 |
| 0.075           | 0.656  | 0.520  | 0.389  | 0.248  | 0.133  | -0.004 | -0.134 | -0.281 | -0.411 | -0.685 | -0.967 |
| 0.100           | 0.469  | 0.358  | 0.243  | 0.129  | 0.025  | -0.088 | -0.200 | -0.316 | -0.428 | -0.658 | -0.892 |
| 0.200           | 0.192  | 0.126  | 0.049  | -0.011 | -0.075 | -0.143 | -0.207 | -0.283 | -0.350 | -0.481 | -0.607 |
| 0.300           | 0.063  | 0.017  | -0.029 | -0.075 | -0.115 | -0.158 | -0.200 | -0.254 | -0.305 | -0.383 | -0.472 |
| 0.400           | -0.012 | -0.044 | -0.075 | -0.105 | -0.132 | -0.161 | -0.193 | -0.223 | -0.239 | -0.282 | -0.349 |
| 0.500           | -0.038 | -0.059 | -0.082 | -0.091 | -0.093 | -0.108 | -0.129 | -0.156 | -0.180 | -0.226 | -0.273 |
| 0.650           | -0.039 | -0.053 | -0.068 | -0.079 | -0.088 | -0.098 | -0.104 | -0.119 | -0.134 | -0.163 | -0.179 |
| 0.750           | -0.089 | -0.092 | -0.100 | -0.106 | -0.113 | -0.116 | -0.123 | -0.130 | -0.139 | -0.152 | -0.169 |
| 0.850           | -0.058 | -0.063 | -0.064 | -0.069 | -0.071 | -0.073 | -0.073 | -0.076 | -0.079 | -0.088 | -0.093 |
| 0.950           | -0.026 | -0.027 | -0.025 | -0.026 | -0.026 | -0.025 | -0.028 | -0.019 | -0.021 | -0.020 | -0.019 |

Table 23

Wing BP/4, normal attitude

 $C_p$  $V = 250 \text{ ft/sec}; R = 3.2 \times 10^6$ 

| $\alpha$<br>x/c | -6.3°  | -4.3°  | -3.3°  | -2.3°  | -1.3°  | -0.3°  | 0.75°  | 1.75°  | 3.75°  | 5.75°  | 9.8°   | 13.85° | 17.85° | 21.9°  | 25.95° | 27.95° | 28.95°  | 30.0°   |  |
|-----------------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|---------|---------|--|
| Upper surface   |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |         |         |  |
| 0               | -1.464 | -0.722 | -0.400 | -0.108 | -0.139 | 0.277  | 0.556  | 0.723  | 0.941  | 1.010  | 0.797  | -0.138 | -1.837 | -4.335 | -7.537 | -9.452 | -10.524 | -11.513 |  |
| 0.005           | 1.010  | 0.971  | 0.933  | 0.882  | 0.819  | 0.749  | 0.660  | 0.560  | 0.323  | 0.032  | -0.697 | -1.639 | -2.833 | -4.206 | -5.704 | -6.410 | -6.813  | -7.142  |  |
| 0.015           | 0.758  | 0.629  | 0.558  | 0.526  | 0.397  | 0.316  | 0.220  | 0.119  | -0.108 | -0.353 | -0.925 | -1.617 | -2.332 | -3.238 | -4.058 | -4.505 | -4.733  | -4.909  |  |
| 0.030           | 0.452  | 0.312  | 0.240  | 0.164  | 0.082  | -0.006 | -0.084 | -0.171 | -0.363 | -0.560 | -1.000 | -1.488 | -2.034 | -2.553 | -3.114 | -3.379 | -3.509  | -3.599  |  |
| 0.050           | 0.248  | 0.123  | 0.058  | -0.005 | -0.074 | -0.137 | -0.213 | -0.283 | -0.434 | -0.592 | -0.922 | -1.291 | -1.609 | -1.999 | -2.375 | -2.564 | -2.646  | -2.723  |  |
| 0.075           | 0.076  | -0.039 | -0.095 | -0.148 | -0.207 | -0.259 | -0.322 | -0.380 | -0.502 | -0.627 | -0.882 | -1.097 | -1.407 | -1.687 | -1.945 | -2.064 | -2.121  | -2.161  |  |
| 0.100           | -0.015 | -0.118 | -0.166 | -0.211 | -0.263 | -0.313 | -0.361 | -0.409 | -0.510 | -0.612 | -0.820 | -0.988 | -1.231 | -1.446 | -1.634 | -1.717 | -1.757  | -1.788  |  |
| 0.200           | -0.174 | -0.230 | -0.267 | -0.292 | -0.320 | -0.347 | -0.375 | -0.402 | -0.453 | -0.495 | -0.581 | -0.679 | -0.783 | -0.872 | -0.952 | -0.983 | -1.002  | -1.020  |  |
| 0.300           | -0.231 | -0.276 | -0.293 | -0.310 | -0.327 | -0.342 | -0.360 | -0.375 | -0.409 | -0.429 | -0.478 | -0.528 | -0.585 | -0.636 | -0.677 | -0.692 | -0.699  | -0.704  |  |
| 0.400           | -0.198 | -0.228 | -0.241 | -0.250 | -0.263 | -0.272 | -0.284 | -0.295 | -0.275 | -0.295 | -0.326 | -0.352 | -0.388 | -0.429 | -0.461 | -0.477 | -0.487  | -0.495  |  |
| 0.500           | -0.156 | -0.178 | -0.177 | -0.165 | -0.166 | -0.172 | -0.181 | -0.188 | -0.201 | -0.210 | -0.223 | -0.238 | -0.264 | -0.299 | -0.331 | -0.346 | -0.356  | -0.366  |  |
| 0.650           | -0.042 | -0.058 | -0.063 | -0.064 | -0.067 | -0.068 | -0.069 | -0.071 | -0.076 | -0.081 | -0.086 | -0.097 | -0.124 | -0.157 | -0.189 | -0.204 | -0.216  | -0.227  |  |
| 0.750           | -0.031 | -0.037 | -0.040 | -0.037 | -0.038 | -0.037 | -0.035 | -0.036 | -0.034 | -0.034 | -0.032 | -0.040 | -0.064 | -0.091 | -0.111 | -0.130 | -0.140  | -0.151  |  |
| 0.850           | 0.017  | 0.012  | 0.013  | 0.014  | 0.014  | 0.017  | 0.019  | 0.019  | 0.020  | 0.021  | 0.023  | 0.015  | -0.004 | -0.022 | -0.040 | -0.050 | -0.060  | -0.093  |  |
| 0.950           | 0.082  | 0.079  | 0.080  | 0.080  | 0.084  | 0.087  | 0.091  | 0.092  | 0.095  | 0.096  | 0.099  | 0.096  | 0.080  | 0.068  | 0.063  | 0.032  | 0.033   | 0.019   |  |
| Lower surface   |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |         |         |  |
| 0.005           | -2.144 | -1.629 | -1.383 | -1.129 | -0.863 | -0.646 | -0.406 | -0.198 | 0.172  | 0.472  | 0.870  | 1.011  | 0.924  | 0.604  | 0.096  | -0.256 | -0.445  | -0.624  |  |
| 0.015           | -1.105 | -0.830 | -0.701 | -0.571 | -0.447 | -0.352 | -0.226 | -0.107 | 0.104  | 0.299  | 0.622  | 0.858  | 0.987  | 1.010  | 0.940  | 0.869  | 0.824   | 0.777   |  |
| 0.030           | -0.803 | -0.616 | -0.525 | -0.438 | -0.348 | -0.274 | -0.190 | -0.105 | 0.055  | 0.202  | 0.471  | 0.696  | 0.865  | 0.967  | 1.010  | 1.010  | 1.005   | 0.997   |  |
| 0.050           | -0.632 | -0.497 | -0.433 | -0.367 | -0.300 | -0.242 | -0.179 | -0.111 | 0.016  | 0.135  | 0.359  | 0.559  | 0.729  | 0.861  | 0.953  | 0.982  | 0.995   | 1.003   |  |
| 0.075           | -0.505 | -0.405 | -0.356 | -0.306 | -0.257 | -0.209 | -0.163 | -0.112 | -0.012 | 0.086  | 0.272  | 0.452  | 0.613  | 0.746  | 0.857  | 0.903  | 0.924   | 0.941   |  |
| 0.100           | -0.426 | -0.348 | -0.312 | -0.269 | -0.229 | -0.189 | -0.152 | -0.113 | -0.029 | 0.052  | 0.216  | 0.372  | 0.525  | 0.657  | 0.772  | 0.825  | 0.848   | 0.870   |  |
| 0.200           | -0.330 | -0.292 | -0.273 | -0.250 | -0.229 | -0.207 | -0.185 | -0.156 | -0.103 | -0.051 | 0.060  | 0.178  | 0.299  | 0.414  | 0.528  | 0.583  | 0.610   | 0.635   |  |
| 0.300           | -0.263 | -0.241 | -0.230 | -0.218 | -0.206 | -0.193 | -0.179 | -0.164 | -0.129 | -0.093 | -0.011 | 0.079  | 0.178  | 0.276  | 0.380  | 0.432  | 0.459   | 0.482   |  |
| 0.400           | -0.172 | -0.161 | -0.157 | -0.148 | -0.141 | -0.135 | -0.126 | -0.120 | -0.096 | -0.072 | -0.011 | 0.058  | 0.140  | 0.222  | 0.313  | 0.358  | 0.380   | 0.403   |  |
| 0.500           | -0.108 | -0.105 | -0.102 | -0.099 | -0.096 | -0.093 | -0.086 | -0.079 | -0.059 | -0.041 | 0.005  | 0.058  | 0.125  | 0.195  | 0.273  | 0.313  | 0.334   | 0.352   |  |
| 0.650           | -0.002 | -0.004 | 0      | 0      | 0      | 0.002  | 0.005  | 0.008  | 0.024  | 0.032  | 0.049  | 0.089  | 0.140  | 0.195  | 0.257  | 0.288  | 0.304   | 0.319   |  |
| 0.750           | 0.049  | 0.049  | 0.050  | 0.049  | 0.048  | 0.049  | 0.051  | 0.054  | 0.063  | 0.071  | 0.099  | 0.111  | 0.151  | 0.197  | 0.251  | 0.274  | 0.287   | 0.301   |  |
| 0.850           | 0.070  | 0.063  | 0.064  | 0.062  | 0.063  | 0.062  | 0.063  | 0.063  | 0.067  | 0.072  | 0.090  | 0.113  | 0.140  | 0.175  | 0.219  | 0.237  | 0.244   | 0.254   |  |
| 0.950           | 0.113  | 0.099  | 0.099  | 0.100  | 0.099  | 0.101  | 0.098  | 0.093  | 0.095  | 0.095  | 0.099  | 0.106  | 0.126  | 0.142  | 0.165  | 0.170  | 0.171   | 0.173   |  |

Table 23 (Contd)

Wing BP/4, inverted attitude

$C_p$

$V = 250 \text{ ft/sec}; R = 3.2 \times 10^6$

| $\alpha$<br>$x/c$ | $-5.75^\circ$ | $-4.75^\circ$ | $-3.7^\circ$ | $-2.7^\circ$ | $-1.7^\circ$ | $-0.7^\circ$ | $0.3^\circ$ | $1.3^\circ$ | $2.3^\circ$ | $4.35^\circ$ | $6.35^\circ$ |
|-------------------|---------------|---------------|--------------|--------------|--------------|--------------|-------------|-------------|-------------|--------------|--------------|
| Upper surface     |               |               |              |              |              |              |             |             |             |              |              |
| 0                 | -1.316        | -0.949        | -0.626       | -0.290       | -0.012       | 0.234        | 0.438       | 0.628       | 0.784       | 0.968        | 1.012        |
| 0.005             | 1.008         | 0.989         | 0.962        | 0.917        | 0.863        | 0.795        | 0.720       | 0.623       | 0.512       | 0.265        | -0.034       |
| 0.015             | 0.737         | 0.672         | 0.609        | 0.530        | 0.455        | 0.374        | 0.285       | 0.180       | 0.073       | -0.153       | -0.406       |
| 0.030             | 0.430         | 0.360         | 0.292        | 0.211        | 0.136        | 0.057        | -0.025      | -0.116      | -0.211      | -0.403       | -0.602       |
| 0.050             | 0.228         | 0.164         | 0.103        | 0.034        | -0.029       | -0.097       | -0.163      | -0.238      | -0.316      | -0.465       | -0.621       |
| 0.075             | 0.056         | -0.001        | -0.054       | -0.113       | -0.169       | -0.160       | -0.281      | -0.342      | -0.406      | -0.528       | -0.649       |
| 0.100             | -0.034        | -0.085        | -0.131       | -0.184       | -0.231       | -0.279       | -0.326      | -0.378      | -0.428      | -0.530       | -0.627       |
| 0.200             | -0.185        | -0.218        | -0.246       | -0.277       | -0.304       | -0.331       | -0.357      | -0.384      | -0.413      | -0.465       | -0.492       |
| 0.300             | -0.240        | -0.264        | -0.283       | -0.302       | -0.319       | -0.334       | -0.349      | -0.365      | -0.382      | -0.412       | -0.431       |
| 0.400             | -0.220        | -0.222        | -0.233       | -0.247       | -0.256       | -0.266       | -0.279      | -0.289      | -0.293      | -0.282       | -0.295       |
| 0.500             | -0.161        | -0.174        | -0.182       | -0.177       | -0.166       | -0.168       | -0.175      | -0.182      | -0.188      | -0.199       | -0.206       |
| 0.650             | -0.047        | -0.056        | -0.061       | -0.063       | -0.065       | -0.067       | -0.068      | -0.068      | -0.070      | -0.073       | -0.075       |
| 0.750             | -0.033        | -0.038        | -0.039       | -0.039       | -0.036       | -0.040       | -0.034      | -0.031      | -0.029      | -0.028       | -0.023       |
| 0.850             | 0.014         | 0.011         | 0.013        | 0.015        | 0.016        | 0.019        | 0.021       | 0.026       | 0.027       | 0.031        | 0.037        |
| 0.950             | 0.083         | 0.082         | 0.084        | 0.088        | 0.091        | 0.094        | 0.096       | 0.102       | 0.105       | 0.111        | 0.117        |
| Lower surface     |               |               |              |              |              |              |             |             |             |              |              |
| 0.005             | -2.086        | -1.797        | -1.556       | -1.289       | -1.035       | -0.779       | -0.564      | -0.322      | -0.106      | 0.244        | 0.530        |
| 0.015             | -1.053        | -0.917        | -0.790       | -0.652       | -0.525       | -0.408       | -0.308      | -0.170      | -0.055      | 0.151        | 0.341        |
| 0.030             | -0.765        | -0.674        | -0.587       | -0.492       | -0.404       | -0.318       | -0.243      | -0.153      | -0.064      | 0.091        | 0.239        |
| 0.050             | -0.606        | -0.540        | -0.477       | -0.409       | -0.343       | -0.277       | -0.221      | -0.148      | -0.076      | 0.045        | 0.165        |
| 0.075             | -0.486        | -0.438        | -0.391       | -0.338       | -0.288       | -0.239       | -0.192      | -0.140      | -0.085      | 0.012        | 0.111        |
| 0.100             | -0.411        | -0.373        | -0.335       | -0.294       | -0.252       | -0.214       | -0.178      | -0.133      | -0.089      | -0.008       | 0.076        |
| 0.200             | -0.320        | -0.305        | -0.283       | -0.262       | -0.239       | -0.219       | -0.196      | -0.171      | -0.137      | -0.087       | -0.032       |
| 0.300             | -0.254        | -0.247        | -0.235       | -0.223       | -0.210       | -0.200       | -0.185      | -0.168      | -0.150      | -0.117       | -0.077       |
| 0.400             | -0.166        | -0.164        | -0.156       | -0.150       | -0.142       | -0.136       | -0.127      | -0.116      | -0.110      | -0.085       | -0.058       |
| 0.500             | -0.104        | -0.104        | -0.100       | -0.098       | -0.094       | -0.090       | -0.087      | -0.079      | -0.067      | -0.049       | -0.028       |
| 0.650             | 0             | 0             | 0.001        | 0.002        | 0.003        | 0.005        | 0.007       | 0.011       | 0.019       | 0.032        | 0.044        |
| 0.750             | 0.054         | 0.052         | 0.053        | 0.053        | 0.053        | 0.055        | 0.053       | 0.059       | 0.064       | 0.071        | 0.086        |
| 0.850             | 0.073         | 0.070         | 0.072        | 0.072        | 0.073        | 0.075        | 0.073       | 0.077       | 0.079       | 0.084        | 0.093        |
| 0.950             | 0.113         | 0.111         | 0.113        | 0.113        | 0.113        | 0.115        | 0.115       | 0.116       | 0.117       | 0.120        | 0.125        |

Table 23 (Contd).

Wing BP/4, normal attitude

$\Delta C_p$

V = 250 ft/sec; R = 3.2 x 10<sup>6</sup>

| $\alpha$<br>x/c | -6.3°  | -4.3°  | -3.3°  | -2.3°  | -1.3°  | -0.3°  | 0.7°   | 1.7°   | 3.7°   | 5.7°   | 9.8°   | 13.85° | 17.85° | 21.9°  | 25.95° | 27.95° | 28.95° | 30.0°  |
|-----------------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| 0               | 0      | 0      | 0      | 0      | 0      | 0      | 0      | 0      | 0      | 0      | 0      | 0      | 0      | 0      | 0      | 0      | 0      | 0      |
| 0.005           | 3.154  | 2.600  | 2.316  | 2.011  | 1.682  | 1.395  | 1.066  | 0.758  | 0.151  | -0.440 | -1.567 | -2.650 | -3.757 | -4.810 | -5.800 | -6.163 | -6.368 | -6.518 |
| 0.015           | 1.863  | 1.459  | 1.259  | 1.097  | 0.844  | 0.668  | 0.446  | 0.226  | -0.212 | -0.652 | -1.547 | -2.475 | -3.319 | -4.248 | -5.008 | -5.374 | -5.557 | -5.686 |
| 0.030           | 1.255  | 0.928  | 0.765  | 0.602  | 0.430  | 0.268  | 0.106  | -0.066 | -0.418 | -0.762 | -1.471 | -2.184 | -2.899 | -3.520 | -4.124 | -4.389 | -4.514 | -4.596 |
| 0.050           | 0.880  | 0.620  | 0.491  | 0.362  | 0.226  | 0.105  | -0.034 | -0.172 | -0.450 | -0.727 | -1.281 | -1.850 | -2.338 | -2.860 | -3.328 | -3.546 | -3.641 | -3.726 |
| 0.075           | 0.581  | 0.366  | 0.261  | 0.158  | 0.050  | -0.050 | -0.159 | -0.268 | -0.490 | -0.713 | -1.154 | -1.549 | -2.020 | -2.433 | -2.802 | -2.967 | -3.045 | -3.102 |
| 0.100           | 0.411  | 0.230  | 0.146  | 0.058  | -0.034 | -0.124 | -0.209 | -0.296 | -0.481 | -0.664 | -1.036 | -1.360 | -1.756 | -2.103 | -2.406 | -2.542 | -2.605 | -2.658 |
| 0.200           | 0.156  | 0.062  | 0.006  | -0.042 | -0.091 | -0.140 | -0.190 | -0.246 | -0.350 | -0.444 | -0.641 | -0.857 | -1.082 | -1.286 | -1.480 | -1.566 | -1.612 | -1.655 |
| 0.300           | 0.032  | -0.035 | -0.063 | -0.092 | -0.121 | -0.149 | -0.181 | -0.211 | -0.280 | -0.336 | -0.467 | -0.607 | -0.763 | -0.912 | -1.057 | -1.124 | -1.158 | -1.186 |
| 0.400           | -0.026 | -0.067 | -0.084 | -0.102 | -0.122 | -0.137 | -0.158 | -0.175 | -0.179 | -0.223 | -0.315 | -0.410 | -0.528 | -0.651 | -0.774 | -0.835 | -0.867 | -0.898 |
| 0.500           | -0.048 | -0.073 | -0.075 | -0.066 | -0.070 | -0.079 | -0.095 | -0.109 | -0.142 | -0.169 | -0.228 | -0.296 | -0.389 | -0.494 | -0.604 | -0.659 | -0.690 | -0.718 |
| 0.650           | -0.040 | -0.054 | -0.063 | -0.064 | -0.067 | -0.070 | -0.074 | -0.079 | -0.100 | -0.113 | -0.135 | -0.186 | -0.264 | -0.352 | -0.446 | -0.492 | -0.520 | -0.546 |
| 0.750           | -0.080 | -0.086 | -0.090 | -0.086 | -0.086 | -0.086 | -0.086 | -0.090 | -0.097 | -0.105 | -0.131 | -0.151 | -0.215 | -0.288 | -0.362 | -0.404 | -0.427 | -0.452 |
| 0.850           | -0.053 | -0.051 | -0.051 | -0.048 | -0.049 | -0.045 | -0.044 | -0.044 | -0.047 | -0.051 | -0.113 | -0.098 | -0.144 | -0.197 | -0.259 | -0.287 | -0.304 | -0.347 |
| 0.950           | -0.031 | -0.020 | -0.019 | -0.020 | -0.015 | -0.014 | -0.007 | -0.001 | 0      | 0.001  | 0      | -0.010 | -0.046 | -0.074 | -0.102 | -0.138 | -0.138 | -0.154 |

Wing BP/4, inverted attitude

$\Delta C_p$

V = 250 ft/sec; R = 3.2 x 10<sup>6</sup>

| $\alpha$<br>x/c | -5.75° | -4.75° | -3.7°  | -2.7°  | -1.7°  | -0.7°  | 0.3°   | 1.3°   | 2.3°   | 4.35°  | 6.35°  |
|-----------------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| 0               | 0      | 0      | 0      | 0      | 0      | 0      | 0      | 0      | 0      | 0      | 0      |
| 0.005           | 3.094  | 2.786  | 2.518  | 2.206  | 1.898  | 1.574  | 1.284  | 0.945  | 0.618  | 0.021  | -0.564 |
| 0.015           | 1.790  | 1.589  | 1.408  | 1.182  | 0.980  | 0.782  | 0.593  | 0.350  | 0.128  | -0.304 | -0.747 |
| 0.030           | 1.195  | 1.034  | 0.879  | 0.703  | 0.540  | 0.375  | 0.218  | 0.037  | -0.147 | -0.494 | -0.841 |
| 0.050           | 0.834  | 0.704  | 0.580  | 0.443  | 0.314  | 0.180  | 0.058  | -0.090 | -0.240 | -0.510 | -0.786 |
| 0.075           | 0.542  | 0.437  | 0.337  | 0.225  | 0.119  | 0.079  | -0.089 | -0.202 | -0.321 | -0.540 | -0.760 |
| 0.100           | 0.379  | 0.288  | 0.204  | 0.110  | 0.021  | -0.065 | -0.148 | -0.245 | -0.339 | -0.522 | -0.703 |
| 0.200           | 0.135  | 0.087  | 0.037  | -0.015 | -0.065 | -0.112 | -0.161 | -0.213 | -0.276 | -0.378 | -0.460 |
| 0.300           | 0.014  | 0.017  | -0.048 | -0.079 | -0.109 | -0.134 | -0.164 | -0.197 | -0.232 | -0.295 | -0.354 |
| 0.400           | -0.054 | -0.058 | -0.077 | -0.097 | -0.114 | -0.130 | -0.152 | -0.173 | -0.183 | -0.197 | -0.237 |
| 0.500           | -0.057 | -0.070 | -0.082 | -0.079 | -0.072 | -0.078 | -0.088 | -0.103 | -0.121 | -0.150 | -0.178 |
| 0.650           | -0.047 | -0.056 | -0.062 | -0.065 | -0.068 | -0.072 | -0.075 | -0.079 | -0.089 | -0.105 | -0.119 |
| 0.750           | -0.087 | -0.090 | -0.092 | -0.092 | -0.089 | -0.095 | -0.089 | -0.090 | -0.093 | -0.099 | -0.109 |
| 0.850           | -0.059 | -0.059 | -0.059 | -0.057 | -0.057 | -0.056 | -0.052 | -0.051 | -0.052 | -0.053 | -0.056 |
| 0.950           | -0.030 | -0.029 | -0.029 | -0.025 | -0.024 | -0.021 | -0.019 | -0.014 | -0.012 | -0.009 | -0.008 |



Table 24

Wing BP/5, normal attitude

C<sub>p</sub>

V = 250 ft/sec; R = 3.2 x 10<sup>6</sup>

| $\alpha$<br>X/C | -6.35° | -4.35° | -2.35° | -1.35° | -0.35° | 0.65°  | 1.65°  | 3.65°  | 5.65°  | 9.65°  | 13.7°  | 17.7°  | 21.7°  | 25.7°  | 29.75° | 31.75° | 33.75° | 35.75° | 37.25° |
|-----------------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| Upper surface   |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |
| 0               | -0.716 | -0.264 | 0.105  | 0.277  | 0.423  | 0.565  | 0.681  | 0.866  | 0.973  | 1.008  | 0.745  | 0.095  | -0.917 | -2.346 | -4.120 | -5.136 | -6.274 | -7.508 | -8.490 |
| 0.005           | 0.982  | 0.929  | 0.853  | 0.808  | 0.754  | 0.691  | 0.626  | 0.471  | 0.297  | -0.127 | -0.661 | -1.285 | -1.973 | -2.769 | -3.613 | -4.042 | -4.517 | -4.894 | -5.215 |
| 0.015           | 0.659  | 0.553  | 0.442  | 0.382  | 0.320  | 0.247  | 0.179  | 0.029  | -0.128 | -0.483 | -0.889 | -1.338 | -1.804 | -2.216 | -2.747 | -2.946 | -3.158 | -3.402 | -3.554 |
| 0.030           | 0.349  | 0.242  | 0.133  | 0.081  | 0.025  | -0.038 | -0.094 | -0.221 | -0.350 | -0.615 | -0.903 | -1.205 | -1.534 | -1.740 | -2.015 | -2.156 | -2.294 | -2.414 | -2.467 |
| 0.050           | 0.165  | 0.070  | -0.019 | -0.063 | -0.107 | -0.157 | -0.203 | -0.300 | -0.396 | -0.590 | -0.792 | -1.000 | -1.100 | -1.305 | -1.485 | -1.570 | -1.651 | -1.724 | -1.747 |
| 0.075           | 0.014  | -0.069 | -0.141 | -0.178 | -0.212 | -0.254 | -0.291 | -0.363 | -0.435 | -0.578 | -0.716 | -0.814 | -0.945 | -1.065 | -1.177 | -1.227 | -1.275 | -1.309 | -1.313 |
| 0.100           | -0.060 | -0.130 | -0.191 | -0.220 | -0.247 | -0.284 | -0.310 | -0.369 | -0.426 | -0.534 | -0.612 | -0.702 | -0.793 | -0.878 | -0.953 | -0.987 | -1.019 | -1.042 | -1.066 |
| 0.200           | -0.167 | -0.210 | -0.239 | -0.251 | -0.263 | -0.282 | -0.292 | -0.316 | -0.338 | -0.356 | -0.392 | -0.432 | -0.464 | -0.495 | -0.534 | -0.550 | -0.573 | -0.599 | -0.640 |
| 0.300           | -0.209 | -0.233 | -0.250 | -0.255 | -0.265 | -0.266 | -0.271 | -0.284 | -0.284 | -0.291 | -0.299 | -0.321 | -0.347 | -0.379 | -0.430 | -0.455 | -0.485 | -0.510 | -0.537 |
| 0.400           | -0.171 | -0.187 | -0.197 | -0.198 | -0.198 | -0.205 | -0.206 | -0.170 | -0.172 | -0.175 | -0.178 | -0.203 | -0.237 | -0.285 | -0.354 | -0.385 | -0.422 | -0.460 | -0.492 |
| 0.500           | -0.129 | -0.135 | -0.182 | -0.108 | -0.108 | -0.113 | -0.113 | -0.111 | -0.109 | -0.106 | -0.112 | -0.148 | -0.200 | -0.262 | -0.346 | -0.385 | -0.432 | -0.476 | -0.515 |
| 0.650           | -0.029 | -0.036 | -0.035 | -0.031 | -0.028 | -0.027 | -0.024 | -0.021 | -0.019 | -0.023 | -0.046 | -0.105 | -0.174 | -0.256 | -0.363 | -0.414 | -0.468 | -0.508 | -0.536 |
| 0.750           | -0.021 | -0.022 | -0.018 | -0.012 | -0.007 | -0.004 | 0      | 0.006  | 0.009  | -0.001 | -0.030 | -0.096 | -0.169 | -0.260 | -0.373 | -0.420 | -0.458 | -0.482 | -0.508 |
| 0.850           | 0.015  | 0.016  | 0.022  | 0.028  | 0.033  | 0.035  | 0.040  | 0.043  | 0.044  | 0.029  | -0.001 | -0.059 | -0.123 | -0.201 | -0.284 | -0.306 | -0.318 | -0.348 | -0.389 |
| 0.950           | 0.066  | 0.073  | 0.079  | 0.085  | 0.091  | 0.093  | 0.096  | 0.098  | 0.098  | 0.086  | 0.069  | 0.037  | 0.003  | -0.032 | -0.051 | -0.049 | -0.052 | -0.304 | -0.118 |
| Lower surface   |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |
| 0.005           | -1.669 | -1.290 | -0.938 | -0.762 | -0.628 | -0.432 | -0.277 | 0.011  | 0.253  | 0.639  | 0.894  | 1.007  | 0.993  | 0.862  | 0.607  | 0.438  | 0.232  | 0.004  | -0.182 |
| 0.015           | -0.808 | -0.633 | -0.468 | -0.385 | -0.316 | -0.231 | -0.150 | 0.014  | 0.156  | 0.418  | 0.645  | 0.820  | 0.941  | 1.005  | 1.010  | 0.995  | 0.965  | 0.925  | 0.880  |
| 0.030           | -0.576 | -0.461 | -0.351 | -0.292 | -0.241 | -0.184 | -0.128 | -0.013 | 0.093  | 0.295  | 0.487  | 0.651  | 0.789  | 0.896  | 0.968  | 0.991  | 1.006  | 1.016  | 1.010  |
| 0.050           | -0.441 | -0.363 | -0.289 | -0.242 | -0.204 | -0.164 | -0.123 | -0.035 | 0.047  | 0.208  | 0.369  | 0.515  | 0.650  | 0.767  | 0.861  | 0.890  | 0.936  | 0.968  | 0.981  |
| 0.075           | -0.337 | -0.283 | -0.228 | -0.196 | -0.163 | -0.139 | -0.107 | -0.046 | 0.017  | 0.147  | 0.283  | 0.412  | 0.535  | 0.650  | 0.750  | 0.795  | 0.839  | 0.882  | 0.903  |
| 0.100           | -0.271 | -0.230 | -0.190 | -0.164 | -0.139 | -0.118 | -0.093 | -0.054 | -0.001 | 0.108  | 0.226  | 0.342  | 0.455  | 0.565  | 0.665  | 0.714  | 0.759  | 0.805  | 0.830  |
| 0.200           | -0.215 | -0.204 | -0.188 | -0.175 | -0.163 | -0.153 | -0.140 | -0.109 | -0.078 | -0.008 | 0.071  | 0.159  | 0.252  | 0.346  | 0.442  | 0.489  | 0.538  | 0.589  | 0.630  |
| 0.300           | -0.177 | -0.177 | -0.175 | -0.167 | -0.161 | -0.157 | -0.149 | -0.134 | -0.114 | -0.065 | -0.003 | 0.068  | 0.146  | 0.234  | 0.320  | 0.365  | 0.412  | 0.462  | 0.496  |
| 0.400           | -0.110 | -0.116 | -0.119 | -0.116 | -0.113 | -0.113 | -0.109 | -0.104 | -0.090 | -0.055 | -0.007 | 0.052  | 0.118  | 0.195  | 0.275  | 0.314  | 0.361  | 0.409  | 0.439  |
| 0.500           | -0.054 | -0.063 | -0.069 | -0.069 | -0.067 | -0.069 | -0.066 | -0.066 | -0.057 | -0.030 | 0.007  | 0.059  | 0.118  | 0.188  | 0.261  | 0.300  | 0.342  | 0.388  | 0.414  |
| 0.650           | 0.019  | 0.008  | 0.003  | 0.001  | 0.001  | -0.001 | -0.001 | 0.009  | 0.018  | 0.023  | 0.051  | 0.095  | 0.148  | 0.212  | 0.278  | 0.314  | 0.351  | 0.391  | 0.414  |
| 0.750           | 0.056  | 0.048  | 0.044  | 0.045  | 0.045  | 0.042  | 0.042  | 0.048  | 0.055  | 0.074  | 0.104  | 0.137  | 0.173  | 0.233  | 0.293  | 0.325  | 0.361  | 0.396  | 0.414  |
| 0.850           | 0.066  | 0.063  | 0.058  | 0.058  | 0.058  | 0.056  | 0.057  | 0.058  | 0.065  | 0.081  | 0.107  | 0.140  | 0.181  | 0.232  | 0.282  | 0.310  | 0.361  | 0.369  | 0.382  |
| 0.950           | 0.101  | 0.103  | 0.101  | 0.101  | 0.101  | 0.098  | 0.096  | 0.096  | 0.098  | 0.103  | 0.108  | 0.128  | 0.150  | 0.182  | 0.224  | 0.246  | 0.266  | 0.283  | 0.287  |

Table 24 (contd)

Wing BP/5, inverted altitude Cp V = 250 ft/sec; R = 3.2 x 10<sup>6</sup>

| $\alpha$ | $X/C$  | Upper surface |        |        |        |        |        |        |        |        |        | Lower surface |        |        |        |        |        |        |        |       |       |
|----------|--------|---------------|--------|--------|--------|--------|--------|--------|--------|--------|--------|---------------|--------|--------|--------|--------|--------|--------|--------|-------|-------|
| 0        | -0.639 | -0.219        | -0.006 | 0.163  | 0.327  | 0.470  | 0.604  | 0.706  | 0.811  | 0.889  | 0.985  | -1.591        | -1.249 | -0.884 | -0.717 | -0.564 | -0.380 | -0.240 | -0.084 | 0.055 | 0.299 |
| 0.005    | 0.976  | 0.920         | 0.882  | 0.840  | 0.790  | 0.735  | 0.671  | 0.608  | 0.524  | 0.442  | 0.254  | -0.559        | -0.445 | -0.383 | -0.327 | -0.269 | -0.221 | -0.163 | -0.083 | 0.004 | 0.181 |
| 0.015    | 0.641  | 0.538         | 0.479  | 0.423  | 0.360  | 0.291  | 0.175  | 0.057  | -0.003 | -0.075 | -0.175 | -0.559        | -0.445 | -0.383 | -0.327 | -0.269 | -0.221 | -0.163 | -0.083 | 0.004 | 0.181 |
| 0.030    | 0.328  | 0.225         | 0.167  | 0.114  | 0.057  | -0.002 | -0.063 | -0.120 | -0.187 | -0.252 | -0.386 | -0.559        | -0.445 | -0.383 | -0.327 | -0.269 | -0.221 | -0.163 | -0.083 | 0.004 | 0.181 |
| 0.050    | 0.145  | 0.057         | 0.007  | -0.035 | -0.083 | -0.128 | -0.177 | -0.222 | -0.275 | -0.324 | -0.426 | -0.559        | -0.445 | -0.383 | -0.327 | -0.269 | -0.221 | -0.163 | -0.083 | 0.004 | 0.181 |
| 0.075    | -0.008 | -0.081        | -0.122 | -0.156 | -0.195 | -0.233 | -0.273 | -0.306 | -0.349 | -0.385 | -0.462 | -0.559        | -0.445 | -0.383 | -0.327 | -0.269 | -0.221 | -0.163 | -0.083 | 0.004 | 0.181 |
| 0.100    | -0.080 | -0.141        | -0.177 | -0.199 | -0.237 | -0.268 | -0.299 | -0.326 | -0.359 | -0.387 | -0.447 | -0.559        | -0.445 | -0.383 | -0.327 | -0.269 | -0.221 | -0.163 | -0.083 | 0.004 | 0.181 |
| 0.200    | -0.182 | -0.219        | -0.233 | -0.248 | -0.263 | -0.278 | -0.293 | -0.304 | -0.319 | -0.330 | -0.343 | -0.559        | -0.445 | -0.383 | -0.327 | -0.269 | -0.221 | -0.163 | -0.083 | 0.004 | 0.181 |
| 0.300    | -0.224 | -0.251        | -0.257 | -0.264 | -0.270 | -0.277 | -0.281 | -0.288 | -0.294 | -0.294 | -0.294 | -0.559        | -0.445 | -0.383 | -0.327 | -0.269 | -0.221 | -0.163 | -0.083 | 0.004 | 0.181 |
| 0.400    | -0.185 | -0.195        | -0.200 | -0.202 | -0.205 | -0.209 | -0.213 | -0.205 | -0.177 | -0.180 | -0.184 | -0.559        | -0.445 | -0.383 | -0.327 | -0.269 | -0.221 | -0.163 | -0.083 | 0.004 | 0.181 |
| 0.500    | -0.139 | -0.127        | -0.123 | -0.122 | -0.123 | -0.123 | -0.123 | -0.121 | -0.122 | -0.120 | -0.120 | -0.559        | -0.445 | -0.383 | -0.327 | -0.269 | -0.221 | -0.163 | -0.083 | 0.004 | 0.181 |
| 0.550    | -0.048 | -0.044        | -0.043 | -0.040 | -0.035 | -0.014 | -0.010 | -0.008 | -0.006 | -0.006 | -0.006 | -0.559        | -0.445 | -0.383 | -0.327 | -0.269 | -0.221 | -0.163 | -0.083 | 0.004 | 0.181 |
| 0.750    | -0.035 | -0.029        | -0.022 | -0.021 | -0.014 | 0.024  | 0.026  | 0.028  | 0.028  | 0.029  | 0.029  | -0.559        | -0.445 | -0.383 | -0.327 | -0.269 | -0.221 | -0.163 | -0.083 | 0.004 | 0.181 |
| 0.850    | 0.003  | 0.001         | 0.012  | 0      | 0.079  | 0.075  | 0.083  | 0.085  | 0.085  | 0.085  | 0.084  | -0.559        | -0.445 | -0.383 | -0.327 | -0.269 | -0.221 | -0.163 | -0.083 | 0.004 | 0.181 |
| 0.950    | -1.591 | -1.249        | -0.884 | -0.717 | -0.564 | -0.470 | -0.604 | -0.706 | -0.811 | -0.889 | -0.985 | -0.559        | -0.445 | -0.383 | -0.327 | -0.269 | -0.221 | -0.163 | -0.083 | 0.004 | 0.181 |

Table 24 (Contd)

Wing BP/5, normal attitude

$\Delta C_p$

V = 250 ft/sec; R = 3.2 x 10<sup>6</sup>

| $\alpha$<br>x/c | -6.35° | -4.35° | -2.35° | -1.35° | -0.35° | 0.65°  | 1.65°  | 3.65°  | 5.65°  | 9.65°  | 13.7°  | 17.7°  | 21.7°  | 25.7°  | 29.75° | 31.75° | 33.75° | 35.75° | 37.25° |
|-----------------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| 0               | 0      | 0      | 0      | 0      | 0      | 0      | 0      | 0      | 0      | 0      | 0      | 0      | 0      | 0      | 0      | 0      | 0      | 0      | 0      |
| 0.005           | 2.651  | 2.219  | 1.791  | 1.570  | 1.382  | 1.123  | 0.903  | 0.460  | 0.044  | -0.760 | -1.555 | -2.292 | -2.966 | -3.631 | -4.220 | -4.480 | -4.749 | -5.819 | -5.033 |
| 0.015           | 1.467  | 1.186  | 0.910  | 0.767  | 0.636  | 0.478  | 0.329  | 0.015  | -0.284 | -0.901 | -1.534 | -2.158 | -2.745 | -3.221 | -3.757 | -3.941 | -4.123 | -4.327 | -4.434 |
| 0.030           | 0.925  | 0.703  | 0.484  | 0.373  | 0.266  | 0.146  | 0.034  | -0.208 | -0.443 | -0.910 | -1.390 | -1.856 | -2.184 | -2.636 | -2.983 | -3.147 | -3.300 | -3.430 | -3.477 |
| 0.050           | 0.606  | 0.433  | 0.270  | 0.179  | 0.097  | 0.007  | -0.080 | -0.265 | -0.443 | -0.798 | -1.161 | -1.515 | -1.750 | -2.072 | -2.346 | -2.460 | -2.587 | -2.692 | -2.728 |
| 0.075           | 0.351  | 0.214  | 0.087  | 0.018  | -0.049 | -0.115 | -0.184 | -0.317 | -0.452 | -0.725 | -0.999 | -1.226 | -1.480 | -1.713 | -1.927 | -2.022 | -2.114 | -2.191 | -2.216 |
| 0.100           | 0.211  | 0.100  | -0.001 | -0.056 | -0.108 | -0.166 | -0.217 | -0.315 | -0.425 | -0.642 | -0.838 | -1.044 | -1.248 | -1.443 | -1.618 | -1.701 | -1.778 | -1.847 | -1.896 |
| 0.200           | 0.048  | -0.006 | -0.051 | -0.076 | -0.100 | -0.129 | -0.152 | -0.207 | -0.260 | -0.348 | -0.463 | -0.591 | -0.716 | -0.841 | -0.976 | -1.039 | -1.111 | -1.188 | -1.270 |
| 0.300           | -0.032 | -0.056 | -0.075 | -0.088 | -0.104 | -0.109 | -0.122 | -0.150 | -0.170 | -0.226 | -0.296 | -0.389 | -0.493 | -0.613 | -0.750 | -0.820 | -0.897 | -0.972 | -1.033 |
| 0.400           | -0.061 | -0.071 | -0.078 | -0.082 | -0.085 | -0.092 | -0.097 | -0.066 | -0.082 | -0.120 | -0.171 | -0.255 | -0.355 | -0.480 | -0.629 | -0.699 | -0.783 | -0.869 | -0.931 |
| 0.500           | -0.075 | -0.072 | -0.113 | -0.039 | -0.041 | -0.044 | -0.046 | -0.045 | -0.052 | -0.076 | -0.119 | -0.207 | -0.318 | -0.450 | -0.607 | -0.685 | -0.774 | -0.864 | -0.929 |
| 0.650           | -0.048 | -0.044 | -0.038 | -0.032 | -0.029 | -0.026 | -0.023 | -0.030 | -0.037 | -0.046 | -0.097 | -0.200 | -0.322 | -0.468 | -0.641 | -0.728 | -0.819 | -0.899 | -0.950 |
| 0.750           | -0.077 | -0.071 | -0.062 | -0.057 | -0.052 | -0.046 | -0.042 | -0.042 | -0.046 | -0.075 | -0.134 | -0.233 | -0.342 | -0.493 | -0.666 | -0.745 | -0.819 | -0.878 | -0.922 |
| 0.850           | -0.051 | -0.047 | -0.036 | -0.030 | -0.025 | -0.021 | -0.017 | -0.015 | -0.021 | -0.052 | -0.108 | -0.199 | -0.304 | -0.433 | -0.566 | -0.616 | -0.679 | -0.717 | -0.771 |
| 0.950           | -0.035 | -0.030 | -0.022 | -0.016 | -0.010 | -0.005 | 0      | 0.002  | 0      | -0.017 | -0.049 | -0.091 | -0.147 | -0.214 | -0.275 | -0.295 | -0.318 | -0.587 | -0.405 |

Wing BP/5, inverted attitude

$\Delta C_p$

V = 250 ft/sec; R = 3.2 x 10<sup>6</sup>

| $\alpha$<br>x/c | -5.65° | -3.65° | -2.65° | -1.65° | -0.65° | 0.35°  | 1.35°  | 2.35°  | 3.35°  | 4.35°  | 6.4°   |
|-----------------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| 0               | 0      | 0      | 0      | 0      | 0      | 0      | 0      | 0      | 0      | 0      | 0      |
| 0.005           | 2.567  | 2.169  | 1.945  | 1.724  | 1.507  | 1.299  | 1.051  | 0.848  | 0.609  | 0.387  | -0.045 |
| 0.015           | 1.424  | 1.149  | 0.997  | 0.860  | 0.723  | 0.586  | 0.383  | 0.285  | 0.118  | -0.039 | -0.356 |
| 0.030           | 0.887  | 0.670  | 0.550  | 0.441  | 0.326  | 0.219  | 0.100  | -0.008 | -0.134 | -0.256 | -0.500 |
| 0.050           | 0.577  | 0.411  | 0.318  | 0.237  | 0.146  | 0.067  | -0.025 | -0.109 | -0.207 | -0.301 | -0.486 |
| 0.075           | 0.325  | 0.195  | 0.123  | 0.063  | -0.008 | -0.074 | -0.145 | -0.206 | -0.278 | -0.347 | -0.489 |
| 0.100           | 0.189  | 0.086  | 0.024  | -0.019 | -0.081 | -0.134 | -0.187 | -0.231 | -0.284 | -0.341 | -0.455 |
| 0.200           | 0.037  | -0.016 | -0.065 | -0.065 | -0.091 | -0.116 | -0.144 | -0.167 | -0.197 | -0.225 | -0.267 |
| 0.300           | -0.041 | -0.065 | -0.077 | -0.086 | -0.095 | -0.108 | -0.121 | -0.133 | -0.146 | -0.162 | -0.182 |
| 0.400           | -0.065 | -0.076 | -0.081 | -0.083 | -0.089 | -0.095 | -0.101 | -0.098 | -0.068 | -0.078 | -0.095 |
| 0.500           | -0.075 | -0.061 | -0.054 | -0.052 | -0.052 | -0.053 | -0.054 | -0.054 | -0.052 | -0.055 | -0.065 |
| 0.650           | -0.056 | -0.055 | -0.048 | -0.044 | -0.040 | -0.034 | -0.035 | -0.034 | -0.040 | -0.044 | -0.053 |
| 0.750           | -0.080 | -0.074 | -0.071 | -0.063 | -0.062 | -0.055 | -0.054 | -0.052 | -0.054 | -0.056 | -0.061 |
| 0.850           | -0.052 | -0.054 | -0.042 | -0.053 | -0.038 | -0.027 | -0.024 | -0.025 | -0.025 | -0.028 | -0.035 |
| 0.950           | -0.033 | -0.026 | -0.021 | -0.016 | -0.010 | -0.004 | -0.001 | -0.001 | 0.001  | 0      | -0.004 |

Table 25

LOCAL FORCE AND MOMENT COEFFICIENTS FROM INTEGRATED  
PRESSURE MEASUREMENTS

Wing BP/OV = 125 ft/sec, R = 1.6 x 10<sup>6</sup>

| $\alpha$ | $C_N$  | $C_T$   | $C_L$  | $C_D$  | $C_m$   |
|----------|--------|---------|--------|--------|---------|
| - 5.05°  | -0.302 | -0.0041 | -0.301 | 0.0225 | -0.0365 |
| - 4.05°  | -0.207 | -0.0035 | -0.206 | 0.0116 | -0.0374 |
| - 2.0°   | 0.012  | 0.0028  | 0.012  | 0.0024 | -0.0395 |
| 0°       | 0.231  | 0.0013  | 0.231  | 0.0013 | -0.0356 |
| 2.0°     | 0.452  | -0.0126 | 0.453  | 0.0033 | -0.0345 |
| 4.05°    | 0.660  | -0.0439 | 0.661  | 0.0028 | -0.0353 |
| 6.05°    | 0.867  | -0.0892 | 0.872  | 0.0036 | -0.0283 |
| 8.1°     | 1.070  | -0.1467 | 1.081  | 0.0049 | -0.0237 |
| 10.1°    | 1.247  | -0.2149 | 1.262  | 0.0063 | -0.0148 |
| 12.15°   | 1.365  | -0.2647 | 1.388  | 0.0265 | -0.0095 |
| 14.15°   | 1.451  | -0.2952 | 1.481  | 0.0681 | -0.0307 |
| 15.1°    | 1.478  | -0.2986 | 1.505  | 0.0956 | -0.0368 |
| 16.15°   | 1.372  | -0.2142 | 1.378  | 0.1740 | -0.0819 |
| 18.15°   | 1.311  | -0.1169 | 1.284  | 0.2970 | -0.1551 |

Wing BP/OV = 250 ft/sec, R = 3.2 x 10<sup>6</sup>

| $\alpha$ | $C_N$  | $C_T$   | $C_L$  | $C_D$   | $C_m$   |
|----------|--------|---------|--------|---------|---------|
| - 4.05°  | -0.220 | -0.0083 | -0.218 | 0.0074  | -0.0425 |
| - 2.0°   | 0.028  | 0       | 0.028  | 0.0010  | -0.0417 |
| 0°       | 0.218  | -0.0006 | 0.218  | -0.0006 | -0.0347 |
| 2.0°     | 0.434  | -0.0163 | 0.435  | -0.0007 | -0.0341 |
| 4.05°    | 0.656  | -0.0459 | 0.658  | 0.0007  | -0.0328 |
| 6.05°    | 0.864  | -0.0839 | 0.868  | 0.0076  | -0.0305 |
| 8.1°     | 1.077  | -0.1389 | 1.086  | 0.0140  | -0.0277 |
| 10.1°    | 1.307  | -0.2110 | 1.322  | 0.0221  | -0.0319 |
| 12.15°   | 1.445  | -0.2833 | 1.469  | 0.0272  | -0.0229 |
| 14.15°   | 1.472  | -0.3234 | 1.507  | 0.0470  | -0.0082 |
| 16.15°   | 1.401  | -0.1692 | 1.395  | 0.2260  | -0.0618 |

Table 26

LOCAL FORCE AND MOMENT COEFFICIENTS FROM INTEGRATED  
PRESSURE MEASUREMENTS

Wing BP/1

 $V = 125 \text{ ft/sec.}, R = 1.6 \times 10^6$ 

| $\alpha$          | $C_N$  | $C_T$   | $C_L$  | $C_D$   | $C_m$   |
|-------------------|--------|---------|--------|---------|---------|
| Normal attitude   |        |         |        |         |         |
| - 6.55°           | -0.315 | -0.0100 | -0.314 | 0.0249  | -0.0447 |
| - 4.4°            | -0.158 | -0.0056 | -0.158 | 0.0060  | -0.0361 |
| - 2.2°            | -0.001 | 0.0030  | 0      | 0.0030  | -0.0327 |
| - 1.1°            | 0.083  | 0.0024  | 0.083  | 0.0011  | -0.0318 |
| - 0.05°           | 0.159  | 0.0027  | 0.159  | 0.0026  | -0.0317 |
| 1.05°             | 0.240  | -0.0012 | 0.240  | 0.0033  | -0.0294 |
| 2.15°             | 0.319  | -0.0062 | 0.319  | 0.0058  | -0.0271 |
| 4.35°             | 0.482  | -0.0249 | 0.483  | 0.0126  | -0.0249 |
| 6.5°              | 0.645  | -0.0491 | 0.646  | 0.0181  | -0.0240 |
| 8.7°              | 0.794  | -0.0816 | 0.797  | 0.0390  | -0.0192 |
| 10.85°            | 0.949  | -0.1275 | 0.956  | 0.0537  | -0.0145 |
| 13.05°            | 1.105  | -0.1816 | 1.118  | 0.0778  | -0.0133 |
| 15.15°            | 1.229  | -0.2541 | 1.252  | 0.0801  | -0.0086 |
| 17.25°            | 1.312  | -0.2881 | 1.338  | 0.1145  | 0.0035  |
| 17.6°             | 1.336  | -0.2899 | 1.361  | 0.1225  | -0.0044 |
| 18.05°            | 1.127  | -0.1448 | 1.115  | 0.2108  | -0.0959 |
| 19.05°            | 1.133  | -0.1619 | 1.123  | 0.2172  | -0.0968 |
| Inverted attitude |        |         |        |         |         |
| - 3.95°           | -0.127 | -0.0026 | -0.126 | 0.0061  | -0.0422 |
| - 1.75°           | 0.031  | 0.0028  | 0.031  | 0.0019  | -0.0518 |
| - 0.65°           | 0.123  | -0.0003 | 0.123  | -0.0017 | -0.0391 |
| 0.45°             | 0.206  | 0.0019  | 0.206  | 0.0035  | -0.0344 |
| 1.5°              | 0.273  | -0.0006 | 0.273  | 0.0066  | -0.0370 |
| 2.6°              | 0.355  | -0.0075 | 0.355  | 0.0086  | -0.0325 |
| 4.8°              | 0.520  | -0.0263 | 0.521  | 0.0172  | -0.0304 |

Table 26 (Contd)

LOCAL FORCE AND MOMENT COEFFICIENTS FROM INTEGRATED  
PRESSURE MEASUREMENTS

Wing BP/1

 $V = 250 \text{ ft/seo. } R = 3.2 \times 10^6$ 

| $\alpha$          | $C_N$  | $C_T$                                  | $C_L$  | $C_D$   | $C_m$   |
|-------------------|--------|--|--------|---------|---------|
| Normal attitude   |        |  |        |         |         |
| - 4.3°            | -0.155 | -0.0122                                | -0.156 | -0.0006 | -0.0394 |
| - 2.1°            | 0.011  | -0.0009                                | 0.011  | -0.0013 | -0.0347 |
| - 1.0°            | 0.098  | 0.0029                                 | 0.098  | 0.0016  | -0.0386 |
| - 0.9°            | 0.104  | 0.0026                                 | 0.104  | 0.0009  | -0.0356 |
| 0.05°             | 0.182  | 0.0019                                 | 0.182  | 0.0037  | -0.0330 |
| 1.15°             | 0.250  | -0.0012                                | 0.249  | 0.0039  | -0.0320 |
| 2.25°             | 0.332  | -0.0071                                | 0.332  | 0.0059  | -0.0286 |
| 4.45°             | 0.498  | -0.0288                                | 0.499  | 0.0097  | -0.0283 |
| 6.6°              | 0.667  | -0.0521                                | 0.668  | 0.0249  | -0.0238 |
| 8.8°              | 0.826  | -0.0907                                | 0.830  | 0.0365  | -0.0222 |
| 10.95°            | 0.978  | -0.1333                                | 0.985  | 0.0552  | -0.0176 |
| 13.15°            | 1.131  | -0.1873                                | 1.144  | 0.0749  | -0.0153 |
| 15.3°             | 1.284  | Incomplete<br>pressure<br>measurements |        |         | -0.0078 |
| 17.4°             | 1.384  |  |        |         | -0.0037 |
| 18.45°            | 1.411  |  |        |         | 0.0029  |
| Inverted attitude |        |  |        |         |         |
| - 4.0°            | -0.155 | -0.0089                                | -0.116 | -0.0009 | -0.0358 |
| - 1.85°           | 0.031  | 0.0021                                 | 0.031  | 0.0011  | -0.0408 |
| - 0.75°           | 0.118  | 0.0028                                 | 0.118  | 0.0013  | -0.0349 |
| 0.35°             | 0.200  | 0.0026                                 | 0.200  | 0.0038  | -0.0342 |
| 1.45°             | 0.268  | -0.0006                                | 0.268  | 0.0061  | -0.0349 |
| 2.55°             | 0.355  | -0.0076                                | 0.355  | 0.0081  | -0.0320 |
| 4.7°              | 0.524  | -0.0262                                | 0.525  | 0.0170  | -0.0296 |

Table 27

LOCAL FORCE AND MOMENT COEFFICIENTS FROM INTEGRATED  
PRESSURE MEASUREMENTS

Wing BP/2

 $V = 125 \text{ ft/sec. } R = 1.6 \times 10^6$ 

| $\alpha$          | $C_N$  | $C_T$   | $C_L$  | $C_D$  | $C_m$   |
|-------------------|--------|---------|--------|--------|---------|
| Normal attitude   |        |         |        |        |         |
| - 4.15°           | -0.109 | -0.0028 | -0.109 | 0.0052 | -0.0385 |
| - 2.1°            | 0.015  | 0.0023  | 0.015  | 0.0017 | -0.0329 |
| 0°                | 0.132  | 0.0026  | 0.132  | 0.0026 | -0.0294 |
| 2.05°             | 0.257  | -0.0038 | 0.257  | 0.0055 | -0.0250 |
| 4.15°             | 0.381  | -0.0152 | 0.381  | 0.0131 | -0.0207 |
| 6.25°             | 0.508  | -0.0331 | 0.508  | 0.0223 | -0.0165 |
| 8.3°              | 0.628  | -0.0567 | 0.628  | 0.0340 | -0.0173 |
| 10.4°             | 0.764  | -0.0872 | 0.766  | 0.0520 | -0.0127 |
| 12.5°             | 0.878  | -0.1218 | 0.883  | 0.0711 | -0.0089 |
| 14.6°             | 1.008  | -0.1628 | 1.016  | 0.0962 | -0.0038 |
| 16.65°            | 1.109  | -0.2059 | 1.121  | 0.1208 | -0.0022 |
| 18.7°             | 1.187  | -0.2599 | 1.206  | 0.1348 | -0.0019 |
| 19.2°             | 1.209  | -0.2736 | 1.231  | 0.1395 | 0.0019  |
| 19.75°            | 1.234  | -0.2834 | 1.256  | 0.1505 | 0.0018  |
| 19.95°            | 1.231  | -0.2871 | 1.256  | 0.1502 | 0.0018  |
| Inverted attitude |        |         |        |        |         |
| - 3.95°           | -0.108 | -0.0073 | -0.108 | 0.0002 | -0.0244 |
| - 1.9°            | 0.021  | 0.0028  | 0.020  | 0.0020 | -0.0336 |
| 0.2°              | 0.149  | 0.0046  | 0.149  | 0.0051 | -0.0314 |
| 2.3°              | 0.265  | -0.0017 | 0.265  | 0.0086 | -0.0374 |
| 4.35°             | 0.370  | -0.0134 | 0.370  | 0.0147 | -0.0406 |
| 6.45°             | 0.517  | -0.0302 | 0.517  | 0.0282 | -0.0441 |

Table 27 (Contd)LOCAL FORCE AND MOMENT COEFFICIENTS FROM INTEGRATED  
PRESSURE MEASUREMENTSWing BF/2V = 250 ft/sec, R = 3.2 x 10<sup>6</sup>

| $\alpha$        | $C_N$  | $C_T$   | $C_L$  | $C_D$   | $C_m$   |
|-----------------|--------|---------|--------|---------|---------|
| Normal attitude |        |         |        |         |         |
| - 4.7°          | -0.139 | -0.0115 | -0.138 | -0.0001 | -0.0384 |
| - 2.1°          | 0.012  | 0.0031  | 0.012  | -0.0004 | -0.0325 |
| 0°              | 0.131  | 0.0019  | 0.131  | 0.0018  | -0.0305 |
| 2.1°            | 0.269  | -0.0048 | 0.269  | 0.0049  | -0.0277 |
| 4.15°           | 0.382  | -0.0156 | 0.383  | 0.0122  | -0.0223 |
| 6.25°           | 0.511  | -0.0345 | 0.511  | 0.0212  | -0.0159 |
| 8.35°           | 0.655  | -0.0586 | 0.657  | 0.0370  | -0.0134 |
| 10.45°          | 0.783  | -0.0903 | 0.786  | 0.0528  | -0.0130 |
| 12.5°           | 0.904  | -0.1267 | 0.911  | 0.0719  | -0.0093 |
| 14.6°           | 1.024  | -0.1647 | 1.032  | 0.0986  | -0.0058 |
| 16.65°          | 1.146  | -0.2106 | 1.158  | 0.1275  | -0.0021 |
| 18.75°          | 1.243  | -0.2609 | 1.253  | 0.1527  | 0.0008  |
| 19.75°          | 1.279  | -0.2885 | 1.298  | 0.1605  | 0.0022  |
| 20.8°           | 1.312  | -0.3157 | 1.340  | 0.1720  | 0.0047  |



Table 28

LOCAL FORCE AND MOMENT COEFFICIENTS FROM INTEGRATED  
PRESSURE MEASUREMENTS

Wing BP/3

 $V = 125 \text{ ft/sec}, R = 1.6 \times 10^6$ 

| $\alpha$          | $C_N$  | $C_T$   | $C_L$  | $C_D$  | $C_m$   |
|-------------------|--------|---------|--------|--------|---------|
| Normal attitude   |        |         |        |        |         |
| - 6.45°           | -0.171 | -0.0050 | -0.171 | 0.0143 | -0.0452 |
| - 5.45°           | -0.118 | -0.0085 | -0.118 | 0.0028 | -0.0403 |
| - 4.4°            | -0.088 | 0.0017  | -0.087 | 0.0085 | -0.0378 |
| - 3.4°            | -0.049 | 0.0031  | -0.049 | 0.0060 | -0.0334 |
| - 2.4°            | -0.003 | 0.0038  | -0.002 | 0.0039 | -0.0309 |
| - 1.4°            | 0.035  | 0.0036  | 0.035  | 0.0027 | -0.0279 |
| - 0.35°           | 0.079  | 0.0030  | 0.079  | 0.0025 | -0.0237 |
| 0.65°             | 0.122  | 0.0012  | 0.122  | 0.0026 | -0.0225 |
| 1.65°             | 0.162  | -0.0015 | 0.162  | 0.0032 | -0.0191 |
| 3.7°              | 0.252  | -0.0073 | 0.252  | 0.0089 | -0.0142 |
| 5.7°              | 0.327  | -0.0179 | 0.367  | 0.0147 | -0.0071 |
| 7.75°             | 0.419  | -0.0323 | 0.420  | 0.0248 | -0.0043 |
| 9.75°             | 0.503  | -0.0488 | 0.504  | 0.0375 | -0.0018 |
| 11.8°             | 0.599  | -0.0706 | 0.590  | 0.0533 | 0.0011  |
| 13.85°            | 0.681  | -0.0929 | 0.684  | 0.0727 | 0.0028  |
| 15.85°            | 0.761  | -0.1179 | 0.765  | 0.0947 | 0.0064  |
| 17.9°             | 0.862  | -0.1536 | 0.867  | 0.1184 | 0.0069  |
| 19.9°             | 0.952  | -0.1846 | 0.958  | 0.1501 | 0.0082  |
| 21.95°            | 1.031  | -0.2237 | 1.041  | 0.1776 | 0.0062  |
| 23.95°            | 1.101  | -0.2644 | 1.114  | 0.2056 | 0.0044  |
| 25.0°             | 1.137  | -0.2793 | 1.149  | 0.2271 | 0.0016  |
| 25.5°             | 1.116  | -0.2869 | 1.170  | 0.2396 | -0.0020 |
| 25.8°             | 1.168  | -0.2887 | 1.177  | 0.2480 | -0.0051 |
| Inverted attitude |        |         |        |        |         |
| - 5.65°           | -0.122 | -0.0012 | -0.122 | 0.0108 | -0.0446 |
| - 4.65°           | -0.091 | 0.0011  | -0.091 | 0.0086 | -0.0450 |
| - 3.65°           | -0.054 | 0.0016  | -0.054 | 0.0050 | -0.0414 |
| - 2.6°            | -0.014 | 0.0031  | -0.014 | 0.0037 | -0.0387 |
| - 1.6°            | 0.024  | 0.0038  | 0.024  | 0.0031 | -0.0345 |
| - 0.6°            | 0.071  | 0.0040  | 0.071  | 0.0032 | -0.0306 |
| 0.45°             | 0.113  | 0.0036  | 0.113  | 0.0045 | -0.0268 |
| 1.45°             | 0.149  | 0.0018  | 0.149  | 0.0056 | -0.0245 |
| 2.45°             | 0.196  | -0.0002 | 0.196  | 0.0084 | -0.0208 |
| 4.5°              | 0.276  | -0.0083 | 0.276  | 0.0133 | -0.0133 |
| 6.5°              | 0.367  | -0.0184 | 0.367  | 0.0234 | -0.0119 |

Table 28 (Contd)

LOCAL FORCE AND MOMENT COEFFICIENTS FROM INTEGRATED  
PRESSURE MEASUREMENTS

Wing BP/3

 $V = 250 \text{ ft/sec}, R = 3.2 \times 10^6$ 

| $\alpha$          | $C_N$  | $C_T$   | $C_L$  | $C_D$  | $C_m$   |
|-------------------|--------|---------|--------|--------|---------|
| Normal attitude   |        |         |        |        |         |
| - 6.35°           | -0.169 | -0.0021 | -0.168 | 0.0166 | -0.0438 |
| - 5.35°           | -0.126 | -0.0021 | -0.126 | 0.0097 | -0.0406 |
| - 4.3°            | -0.086 | 0.0005  | -0.086 | 0.0069 | -0.0378 |
| - 3.3°            | -0.039 | 0.0019  | -0.039 | 0.0042 | -0.0351 |
| - 2.3°            | -0.008 | 0.0018  | -0.008 | 0.0021 | -0.0330 |
| - 1.3°            | 0.042  | 0.0025  | 0.042  | 0.0015 | -0.0288 |
| - 0.25°           | 0.083  | 0.0029  | 0.083  | 0.0025 | -0.0265 |
| 0.75°             | 0.129  | 0.0008  | 0.129  | 0.0025 | -0.0223 |
| 1.75°             | 0.169  | -0.0004 | 0.169  | 0.0048 | -0.0201 |
| 3.8°              | 0.258  | -0.0086 | 0.258  | 0.0085 | -0.0160 |
| 5.8°              | 0.344  | -0.0187 | 0.344  | 0.0162 | -0.0130 |
| 7.85°             | 0.431  | -0.0333 | 0.431  | 0.0258 | -0.0061 |
| 9.9°              | 0.511  | -0.0482 | 0.512  | 0.0402 | -0.0030 |
| 11.9°             | 0.600  | -0.0667 | 0.601  | 0.0583 | -0.0006 |
| 13.95°            | 0.690  | -0.0893 | 0.692  | 0.0750 | 0.0027  |
| 15.95°            | 0.794  | -0.1223 | 0.797  | 0.1007 | 0.0033  |
| 18.0°             | 0.886  | -0.1476 | 0.888  | 0.1333 | 0.0013  |
| 20.0°             | 0.958  | -0.1837 | 0.963  | 0.1552 | 0.0040  |
| 22.05°            | 1.045  | -0.2178 | 1.050  | 0.1904 | 0.0032  |
| Inverted attitude |        |         |        |        |         |
| - 5.75°           | -0.144 | -0.0033 | -0.143 | 0.0111 | -0.0432 |
| - 4.75°           | -0.102 | 0.0012  | -0.101 | 0.0096 | -0.0413 |
| - 3.75°           | -0.059 | 0.0025  | -0.058 | 0.0063 | -0.0391 |
| - 2.7°            | -0.018 | 0.0035  | -0.018 | 0.0044 | -0.0365 |
| - 1.7°            | 0.018  | 0.0037  | 0.018  | 0.0031 | -0.0352 |
| - 0.7°            | 0.062  | 0.0037  | 0.062  | 0.0030 | -0.0305 |
| 0.3°              | 0.107  | 0.0030  | 0.107  | 0.0036 | -0.0273 |
| 1.35°             | 0.153  | 0.0010  | 0.153  | 0.0046 | -0.0242 |
| 2.35°             | 0.197  | 0.0012  | 0.197  | 0.0069 | -0.0222 |
| 4.4°              | 0.282  | -0.0084 | 0.282  | 0.0132 | -0.0175 |
| 6.4°              | 0.368  | -0.0212 | 0.368  | 0.0201 | -0.0131 |

Table 29

LOCAL FORCE AND MOMENT COEFFICIENTS FROM INTEGRATED  
PRESSURE MEASUREMENTS

Wing BP/4

 $V = 125 \text{ ft/sec. } R = 1.6 \times 10^6$ 

| $\alpha$          | $C_N$  | $C_T$   | $C_L$  | $C_D$  | $C_m$   |
|-------------------|--------|---------|--------|--------|---------|
| Normal attitude   |        |         |        |        |         |
| - 6.45°           | -0.113 | -0.0008 | -0.113 | 0.0119 | -0.0417 |
| - 4.40°           | -0.058 | 0.0017  | -0.058 | 0.0062 | -0.0373 |
| - 3.40°           | -0.034 | 0.0028  | -0.034 | 0.0049 | -0.0326 |
| - 2.40°           | -0.003 | 0.0038  | -0.003 | 0.0039 | -0.0282 |
| - 1.40°           | 0.031  | 0.0042  | 0.031  | 0.0034 | -0.0254 |
| - 0.40°           | 0.057  | 0.0047  | 0.057  | 0.0043 | -0.0215 |
| 0.60°             | 0.091  | 0.0033  | 0.091  | 0.0042 | -0.0210 |
| 1.60°             | 0.122  | 0.0010  | 0.122  | 0.0044 | -0.0154 |
| 3.65°             | 0.183  | -0.0036 | 0.183  | 0.0080 | -0.0091 |
| 5.65°             | 0.252  | -0.0118 | 0.252  | 0.0131 | -0.0052 |
| 9.70°             | 0.386  | -0.0329 | 0.386  | 0.0324 | 0.0025  |
| 13.70°            | 0.538  | -0.0660 | 0.538  | 0.0633 | 0.0059  |
| 17.75°            | 0.681  | -0.1025 | 0.679  | 0.1099 | 0.0051  |
| 21.80°            | 0.831  | -0.1562 | 0.830  | 0.1630 | 0.0039  |
| 25.80°            | 0.990  | -0.2113 | 0.983  | 0.2407 | -0.0076 |
| 27.85°            | 1.069  | -0.2478 | 1.061  | 0.2796 | -0.0137 |
| 28.85°            | 1.104  | -0.2784 | 1.102  | 0.2886 | -0.0193 |
| 29.85°            | 1.150  | -0.2986 | 1.146  | 0.3129 | -0.0203 |
| 30.35°            | 1.139  | -0.2778 | 1.123  | 0.3358 | -0.0262 |
| Inverted attitude |        |         |        |        |         |
| - 5.60°           | -0.099 | 0.0007  | -0.099 | 0.0104 | -0.0439 |
| - 4.60°           | -0.067 | 0.0013  | -0.067 | 0.0067 | -0.0412 |
| - 3.60°           | -0.037 | 0.0025  | -0.037 | 0.0048 | -0.0381 |
| - 2.60°           | -0.005 | 0.0024  | -0.005 | 0.0026 | -0.0330 |
| - 1.60°           | 0.012  | 0.0046  | 0.012  | 0.0043 | -0.0307 |
| - 0.60°           | 0.055  | 0.0037  | 0.055  | 0.0032 | -0.0246 |
| 0.40°             | 0.084  | 0.0028  | 0.084  | 0.0034 | -0.0215 |
| 1.45°             | 0.112  | 0.0009  | 0.112  | 0.0037 | -0.0188 |
| 2.45°             | 0.146  | 0.0003  | 0.146  | 0.0059 | -0.0129 |
| 4.45°             | 0.219  | -0.0050 | 0.218  | 0.0121 | 0.0073  |
| 6.45°             | 0.261  | -0.0137 | 0.261  | 0.0158 | 0.0041  |

Table 29 (Contd)

LOCAL FORCE AND MOMENT COEFFICIENTS FROM INTEGRATED  
PRESSURE MEASUREMENTS

Wing BP/4

V = 250 ft/sec. R =  $3.2 \times 10^6$ 

| $\alpha$          | $C_N$  | $C_T$   | $C_L$  | $C_D$  | $C_m$   |
|-------------------|--------|---------|--------|--------|---------|
| Normal attitude   |        |         |        |        |         |
| - 6.3°            | -0.128 | -0.0014 | -0.128 | 0.0127 | -0.0423 |
| - 4.3°            | -0.066 | 0.0023  | -0.066 | 0.0073 | -0.0361 |
| - 3.3°            | -0.037 | 0.0031  | -0.037 | 0.0052 | -0.0336 |
| - 2.3°            | -0.009 | 0.0044  | -0.009 | 0.0048 | -0.0294 |
| - 1.3°            | 0.023  | 0.0027  | 0.023  | 0.0022 | -0.0248 |
| - 0.3°            | 0.053  | 0.0033  | 0.053  | 0.0030 | -0.0223 |
| 0.75°             | 0.085  | 0.0027  | 0.085  | 0.0037 | -0.0184 |
| 1.75°             | 0.117  | 0.0019  | 0.117  | 0.0055 | -0.0153 |
| 3.75°             | 0.185  | -0.0049 | 0.185  | 0.0072 | -0.0103 |
| 5.75°             | 0.249  | -0.0119 | 0.249  | 0.0132 | -0.0058 |
| 9.8°              | 0.388  | -0.0345 | 0.388  | 0.0319 | 0.0001  |
| 13.85°            | 0.527  | -0.0642 | 0.527  | 0.0636 | 0.0063  |
| 17.85°            | 0.690  | -0.1117 | 0.691  | 0.1056 | 0.0052  |
| 21.9°             | 0.852  | -0.1590 | 0.849  | 0.1702 | -0.0008 |
| 25.95°            | 1.008  | -0.2234 | 1.004  | 0.2395 | -0.0062 |
| 27.95°            | 1.080  | -0.2566 | 1.074  | 0.2796 | -0.0142 |
| 28.95°            | 1.112  | -0.2724 | 1.105  | 0.3002 | -0.0152 |
| 30.0°             | 1.147  | -0.2861 | 1.137  | 0.3254 | -0.0204 |
| Inverted attitude |        |         |        |        |         |
| - 5.75°           | -0.114 | -0.0008 | -0.114 | 0.0106 | -0.0424 |
| - 4.75°           | -0.085 | -0.0004 | -0.085 | 0.0066 | -0.0394 |
| - 3.7°            | -0.049 | 0.0013  | -0.049 | 0.0045 | -0.0371 |
| - 2.7°            | -0.020 | 0.0023  | -0.020 | 0.0032 | -0.0331 |
| - 1.7°            | 0.008  | 0.0023  | 0.008  | 0.0021 | -0.0294 |
| - 0.7°            | 0.035  | 0.0029  | 0.035  | 0.0024 | -0.0268 |
| 0.3°              | 0.066  | 0.0022  | 0.066  | 0.0025 | -0.0216 |
| 1.3°              | 0.102  | 0       | 0.102  | 0.0023 | -0.0188 |
| 2.3°              | 0.138  | -0.0018 | 0.138  | 0.0054 | -0.0158 |
| 4.35°             | 0.204  | -0.0065 | 0.203  | 0.0089 | -0.0105 |
| 6.35°             | 0.268  | -0.0147 | 0.268  | 0.0150 | -0.0059 |

Table 30

LOCAL FORCE AND MOMENT COEFFICIENTS FROM INTEGRATED  
PRESSURE MEASUREMENTS

Wing BP/5

 $V = 125 \text{ ft/sec.}$   $R = 1.6 \times 10^6$ 

| $\alpha$          | $C_N$  | $C_T$   | $C_L$  | $C_D$  | $C_m$   |
|-------------------|--------|---------|--------|--------|---------|
| Normal attitude   |        |         |        |        |         |
| - 6.45°           | -0.060 | 0.0056  | -0.059 | 0.0123 | -0.0364 |
| - 4.4°            | -0.029 | 0.0031  | -0.029 | 0.0053 | -0.0314 |
| - 2.4°            | 0      | 0.0038  | 0      | 0.0038 | -0.0231 |
| - 1.4°            | 0.012  | 0.0048  | 0.012  | 0.0045 | -0.0192 |
| - 0.4°            | 0.024  | 0.0047  | 0.024  | 0.0045 | -0.0163 |
| 0.6°              | 0.039  | 0.0027  | 0.039  | 0.0031 | -0.0116 |
| 1.6°              | 0.056  | 0.0019  | 0.056  | 0.0034 | -0.0084 |
| 3.6°              | 0.083  | 0       | 0.083  | 0.0052 | -0.0020 |
| 5.6°              | 0.125  | -0.0040 | 0.125  | 0.0082 | -0.0010 |
| 9.6°              | 0.201  | -0.0144 | 0.200  | 0.0193 | 0.0063  |
| 13.6°             | 0.304  | -0.0289 | 0.302  | 0.0434 | 0.0013  |
| 17.65°            | 0.432  | -0.0452 | 0.426  | 0.0879 | -0.0144 |
| 21.65°            | 0.561  | -0.0677 | 0.546  | 0.1440 | -0.0296 |
| 25.65°            | 0.718  | -0.0918 | 0.687  | 0.2281 | -0.0569 |
| 29.7°             | 0.888  | -0.1186 | 0.830  | 0.3365 | -0.0793 |
| 33.7°             | 1.018  | -0.1525 | 0.932  | 0.4379 | -0.1081 |
| 35.7°             | 1.103  | -0.1731 | 0.997  | 0.5032 | -0.1288 |
| 37.7°             | 1.161  | -0.1893 | 1.034  | 0.5606 | -0.1384 |
| 37.9°             | 1.076  | -0.0906 | 0.905  | 0.5897 | -0.1384 |
| Inverted attitude |        |         |        |        |         |
| -17.6°            | -0.308 | 0.0123  | -0.290 | 0.1049 | -0.0293 |
| -13.6°            | -0.209 | 0.0129  | -0.200 | 0.0616 | -0.0322 |
| - 9.6°            | -0.118 | 0.0086  | -0.115 | 0.0281 | -0.0431 |
| - 7.6°            | -0.079 | 0.0047  | -0.079 | 0.0151 | -0.0402 |
| - 5.6°            | -0.051 | 0.0055  | -0.050 | 0.0105 | -0.0381 |
| - 3.6°            | -0.020 | 0.0060  | -0.019 | 0.0072 | -0.0326 |
| - 2.6°            | -0.007 | 0.0056  | -0.007 | 0.0059 | -0.0258 |
| - 1.6°            | 0.011  | 0.0045  | 0.011  | 0.0042 | -0.0241 |
| - 0.6°            | 0.025  | 0.0052  | 0.025  | 0.0049 | -0.0199 |
| 0.4°              | 0.039  | 0.0053  | 0.039  | 0.0055 | -0.0166 |
| 1.45°             | 0.050  | 0.0038  | 0.050  | 0.0050 | -0.0128 |
| 2.45°             | 0.067  | 0.0021  | 0.067  | 0.0049 | -0.0089 |
| 3.45°             | 0.082  | 0.0003  | 0.082  | 0.0082 | -0.0059 |
| 4.45°             | 0.105  | -0.0013 | 0.105  | 0.0069 | -0.0043 |
| 6.45°             | 0.141  | -0.0050 | 0.141  | 0.0108 | -0.0007 |

Table 30 (Contd)

LOCAL FORCE AND MOMENT COEFFICIENTS FROM INTEGRATED  
PRESSURE MEASUREMENTS

Wing BP/5

 $V = 250 \text{ ft/sec.}, R = 3.2 \times 10^6$ 

| $\alpha$          | $C_N$  | $C_T$   | $C_L$  | $C_D$  | $C_m$   |
|-------------------|--------|---------|--------|--------|---------|
| Normal attitude   |        |         |        |        |         |
| - 6.35°           | -0.059 | 0.0038  | -0.058 | 0.0104 | -0.0349 |
| - 4.35°           | -0.027 | 0.0050  | -0.027 | 0.0070 | -0.0294 |
| - 2.35°           | -0.001 | 0.0058  | 0      | 0.0058 | -0.0231 |
| - 1.35°           | 0.009  | 0.0048  | 0.009  | 0.0046 | -0.0182 |
| - 0.35°           | 0.022  | 0.0029  | 0.022  | 0.0028 | -0.0143 |
| 0.65°             | 0.040  | 0.0030  | 0.040  | 0.0035 | -0.0104 |
| 1.65°             | 0.057  | 0.0018  | 0.057  | 0.0034 | -0.0084 |
| 3.65°             | 0.089  | -0.0007 | 0.089  | 0.0049 | -0.0025 |
| 5.65°             | 0.125  | -0.0056 | 0.125  | 0.0068 | 0.0012  |
| 9.65°             | 0.207  | -0.0153 | 0.207  | 0.0197 | 0.0050  |
| 13.7°             | 0.302  | -0.0291 | 0.300  | 0.0431 | 0       |
| 17.7°             | 0.433  | -0.0456 | 0.427  | 0.0882 | -0.0115 |
| 21.7°             | 0.564  | -0.0651 | 0.548  | 0.1482 | -0.0310 |
| 25.7°             | 0.717  | -0.0895 | 0.684  | 0.2302 | -0.0550 |
| 29.75°            | 0.877  | -0.1190 | 0.820  | 0.3314 | -0.0797 |
| 31.75°            | 0.949  | -0.1320 | 0.877  | 0.3870 | -0.0910 |
| 33.75°            | 1.033  | -0.1563 | 0.946  | 0.4440 | -0.1059 |
| 33.75°            | 1.138  | -0.1649 | 1.020  | 0.5313 | -0.1301 |
| 37.25°            | 1.155  | -0.1777 | 1.027  | 0.5580 | -0.1318 |
| Inverted attitude |        |         |        |        |         |
| - 5.65°           | -0.056 | 0.0046  | -0.055 | 0.0100 | -0.0361 |
| - 3.65°           | -0.023 | 0.0049  | -0.022 | 0.0063 | -0.0297 |
| - 2.65°           | -0.007 | 0.0060  | -0.007 | 0.0063 | -0.0254 |
| - 1.65°           | 0.003  | 0.0060  | 0.003  | 0.0060 | -0.0226 |
| - 0.65°           | 0.021  | 0.0048  | 0.021  | 0.0045 | -0.0183 |
| 0.35°             | 0.034  | 0.0038  | 0.034  | 0.0040 | -0.0136 |
| 1.35°             | 0.050  | 0.0038  | 0.050  | 0.0050 | -0.0119 |
| 2.35°             | 0.068  | 0.0019  | 0.068  | 0.0047 | -0.0086 |
| 3.35°             | 0.083  | 0       | 0.083  | 0.0049 | -0.0062 |
| 4.35°             | 0.105  | -0.0010 | 0.104  | 0.0070 | -0.0045 |
| 6.4°              | 0.142  | -0.0046 | 0.142  | 0.0113 | -0.0013 |

Table 31

BALANCE MEASUREMENTS OF LIFT, DRAG ANDPITCHING MOMENTWing BF/1 $V = 125 \text{ ft/sec, } R = 1.6 \times 10^6$  $V = 250 \text{ ft/sec, } R = 3.2 \times 10^6$ 

| $\alpha$ | $\bar{C}_L$ | $\bar{C}_D$ | $\bar{C}_m$ |
|----------|-------------|-------------|-------------|
| - 6.25°  | -0.245      | 0.0276      | -0.0361     |
| - 4.15°  | -0.122      | 0.0114      | -0.0325     |
| - 3.05°  | -0.054      | 0.0081      | -0.0312     |
| - 2.0°   | 0.002       | 0.0070      | -0.0298     |
| - 0.95°  | 0.067       | 0.0071      | -0.0289     |
| 0.15°    | 0.124       | 0.0066      | -0.0271     |
| 2.3°     | 0.265       | 0.0114      | -0.0256     |
| 4.45°    | 0.400       | 0.0192      | -0.0245     |
| 6.6°     | 0.549       | 0.0334      | -0.0260     |
| 8.75°    | 0.669       | 0.0488      | -0.0263     |
| 10.9°    | 0.799       | 0.0654      | -0.0270     |
| 13.05°   | 0.928       | 0.0902      | -0.0285     |
| 15.15°   | 1.044       | 0.1155      | -0.0301     |
| 16.25°   | 1.105       | 0.1307      | -0.0310     |
| 17.3°    | 1.147       | 0.1437      | -0.0322     |
| 17.5°    | 1.147       | -           | -0.0324     |
| 17.6°    | 1.088       | -           | -0.0541     |

| $\alpha$                               | $\bar{C}_L$ | $\bar{C}_D$ | $\bar{C}_m$ |
|--|-------------|-------------|-------------|
| No tests at higher<br>Reynold's number |             |             |             |

No "inverted attitude" tests

Table 32BALANCE MEASUREMENTS OF LIFT, DRAG AND  
PITCHING MOMENTWing BF/2 $V = 125 \text{ ft/sec, } R = 1.6 \times 10^6$  $V = 250 \text{ ft/sec, } R = 3.2 \times 10^6$ 

| $\alpha$ | $\bar{C}_L$ | $\bar{C}_D$ | $\bar{C}_m$ |
|----------|-------------|-------------|-------------|
| - 6.15°  | -0.195      | 0.0252      | -0.0325     |
| - 4.05°  | -0.094      | 0.0121      | -0.0292     |
| - 3.05°  | -0.052      | 0.0088      | -0.0275     |
| - 2.0°   | -0.006      | 0.0074      | -0.0258     |
| - 0.95°  | 0.042       | 0.0074      | -0.0245     |
| 0.05°    | 0.093       | 0.0079      | -0.0230     |
| 2.15°    | 0.190       | 0.0113      | -0.0204     |
| 4.2°     | 0.292       | 0.0175      | -0.0186     |
| 6.25°    | 0.394       | 0.0278      | -0.0182     |
| 8.35°    | 0.507       | 0.0435      | -0.0215     |
| 10.4°    | 0.614       | 0.0616      | -0.0226     |
| 12.5°    | 0.716       | 0.0827      | -0.0247     |
| 14.55°   | 0.824       | 0.1081      | -0.0269     |
| 16.6°    | 0.912       | 0.1337      | -0.0301     |
| 18.7°    | 1.009       | 0.1655      | -0.0340     |
| 19.3°    | 1.033       | 0.1753      | -0.0366     |
| 19.5°    | 1.037       | 0.1781      | -0.0372     |

| $\alpha$ | $\bar{C}_L$ | $\bar{C}_D$ | $\bar{C}_m$ |
|----------|-------------|-------------|-------------|
| - 5.1°   | -0.137      | 0.0154      | -0.0312     |
| - 4.05°  | -0.091      | 0.0104      | -0.0292     |
| - 2.0°   | 0.004       | 0.0066      | -0.0256     |
| 0.05°    | 0.103       | 0.0086      | -0.0229     |
| 2.15°    | 0.203       | 0.0121      | -0.0208     |
| 4.2°     | 0.307       | 0.0194      | -0.0194     |
| 6.25°    | 0.408       | 0.0305      | -0.0186     |
| 8.35°    | 0.516       | 0.0453      | -0.0194     |
| 10.4°    | 0.624       | 0.0641      | -0.0213     |
| 12.5°    | 0.728       | 0.0853      | -0.0242     |
| 14.55°   | 0.835       | 0.1113      | -0.0272     |
| 16.6°    | 0.934       | 0.1394      | -0.0297     |
| 18.7°    | 1.029       | 0.1716      | -0.0348     |
| 19.75°   | 1.070       | 0.1879      | -0.0375     |

No "inverted attitude" tests



Table 33

BALANCE MEASUREMENTS OF LIFT, DRAG AND  
PITCHING MOMENT

Wing BF/3

$V = 125 \text{ ft/sec}, R = 1.6 \times 10^6$

$V = 250 \text{ ft/sec}, R = 3.2 \times 10^6$

| $\alpha$ | $\bar{C}_L$ | $\bar{C}_D$ | $\bar{C}_m$ |
|----------|-------------|-------------|-------------|
| - 4.0°   | -0.054      | 0.0123      | -0.0297     |
| - 3.0°   | -0.023      | 0.0111      | -0.0277     |
| - 2.0°   | 0.009       | 0.0105      | -0.0256     |
| - 1.0°   | 0.040       | 0.0111      | -0.0235     |
| 0.05°    | 0.071       | 0.0117      | -0.0213     |
| 1.15°    | 0.106       | 0.0135      | -0.0194     |
| 2.05°    | 0.131       | 0.0124      | -0.0181     |
| 4.0°     | 0.201       | 0.0185      | -0.0166     |
| 6.0°     | 0.275       | 0.0275      | -0.0160     |
| 8.05°    | 0.350       | 0.0394      | -0.0161     |
| 10.05°   | 0.434       | 0.0560      | -0.0199     |
| 12.1°    | 0.514       | 0.0752      | -0.0241     |
| 14.15°   | 0.596       | 0.0987      | -0.0287     |
| 16.15°   | 0.680       | 0.1261      | -0.0345     |
| 18.2°    | 0.767       | 0.1590      | -0.0420     |
| 20.25°   | 0.853       | 0.1942      | -0.0507     |
| 22.25°   | 0.942       | 0.2354      | -0.0611     |
| 24.3°    | 1.021       | 0.2802      | -0.0714     |
| 24.8°    | 1.035       | 0.2904      | -0.0750     |

| $\alpha$ | $\bar{C}_L$ | $\bar{C}_D$ | $\bar{C}_m$ |
|----------|-------------|-------------|-------------|
| - 3.95°  | -0.053      | 0.0115      | -0.0297     |
| - 3.0°   | -0.023      | 0.0108      | -0.0279     |
| - 2.0°   | 0.008       | 0.0106      | -0.0258     |
| - 1.0°   | 0.041       | 0.0108      | -0.0236     |
| 0.05°    | 0.068       | 0.0116      | -0.0219     |
| 2.05°    | 0.137       | 0.0139      | -0.0184     |
| 4.1°     | 0.210       | 0.0204      | -0.0170     |
| 6.1°     | 0.282       | 0.0297      | -0.0167     |
| 8.15°    | 0.357       | 0.0423      | -0.0175     |
| 10.15°   | 0.439       | 0.0583      | -0.0199     |
| 12.2°    | 0.521       | 0.0779      | -0.0235     |
| 14.25°   | 0.611       | 0.1029      | -0.0300     |
| 16.25°   | 0.699       | 0.1314      | -0.0365     |
| 18.3°    | 0.791       | 0.1649      | -0.0452     |
| 20.35°   | 0.882       | 0.2031      | -0.0543     |
| 22.35°   | 0.973       | 0.2477      | -0.0649     |
| 24.4°    | 1.055       | 0.3022      | -0.0744     |
| 24.9°    | 1.078       | 0.3062      | -0.0769     |
| 25.4°    | 1.093       | 0.3164      | -0.0791     |

Table 34

BALANCE MEASUREMENTS OF LIFT, DRAG AND  
PITCHING MOMENT

Wing BF/4

$V = 125 \text{ ft/sec.}, R = 1.6 \times 10^6$

$V = 250 \text{ ft/sec.}, R = 3.2 \times 10^6$

| $\alpha$ | $\bar{C}_L$ | $\bar{C}_D$ | $\bar{C}_m$ |
|----------|-------------|-------------|-------------|
| - 4.3°   | -0.050      | 0.0126      | -0.0276     |
| - 3.7°   | -0.036      | 0.0110      | -0.0266     |
| - 3.3°   | -0.025      | 0.0118      | -0.0258     |
| - 2.7°   | -0.012      | 0.0100      | -0.0245     |
| - 2.3°   | -0.001      | 0.0114      | -0.0236     |
| - 1.7°   | 0.013       | 0.0102      | -0.0224     |
| - 1.3°   | 0.022       | 0.0118      | -0.0218     |
| - 0.7°   | 0.036       | 0.0105      | -0.0201     |
| - 0.3°   | 0.045       | 0.0122      | -0.0194     |
| 0.3°     | 0.060       | 0.0110      | -0.0180     |
| 0.7°     | 0.068       | 0.0124      | -0.0170     |
| 1.3°     | 0.084       | 0.0116      | -0.0159     |
| 1.75°    | 0.093       | 0.0135      | -0.0157     |
| 2.75°    | 0.120       | 0.0160      | -0.0146     |
| 3.75°    | 0.147       | 0.0188      | -0.0141     |
| 5.75°    | 0.204       | 0.0260      | -0.0141     |
| 7.75°    | 0.264       | 0.0370      | -0.0150     |
| 11.8°    | 0.393       | 0.0673      | -0.0226     |
| 15.85°   | 0.532       | 0.1125      | -0.0344     |
| 19.9°    | 0.693       | 0.1801      | -0.0572     |
| 23.95°   | 0.863       | 0.2698      | -0.0861     |
| 25.95°   | 0.932       | 0.3188      | -0.0990     |
| 27.95°   | 1.010       | 0.3728      | -0.1118     |
| 28.4°    | 1.022       | 0.3835      | -0.1123     |

| $\alpha$ | $\bar{C}_L$ | $\bar{C}_D$ | $\bar{C}_m$ |
|----------|-------------|-------------|-------------|
| - 4.25°  | -0.049      | 0.0114      | -0.0276     |
| - 3.8°   | -0.038      | 0.0106      | -0.0268     |
| - 3.25°  | -0.022      | 0.0103      | -0.0259     |
| - 2.8°   | -0.013      | 0.0099      | -0.0247     |
| - 2.2°   | 0.001       | 0.0099      | -0.0240     |
| - 1.8°   | 0.011       | 0.0098      | -0.0224     |
| - 1.2°   | 0.026       | 0.0102      | -0.0214     |
| - 0.75°  | 0.034       | 0.0101      | -0.0203     |
| - 0.2°   | 0.050       | 0.0110      | -0.0193     |
| 0.25°    | 0.061       | 0.0109      | -0.0182     |
| 0.8°     | 0.075       | 0.0120      | -0.0173     |
| 1.8°     | 0.101       | 0.0130      | -0.0159     |
| 2.8°     | 0.126       | 0.0149      | -0.0150     |
| 3.8°     | 0.154       | 0.0179      | -0.0146     |
| 5.85°    | 0.213       | 0.0256      | -0.0147     |
| 7.85°    | 0.272       | 0.0363      | -0.0156     |
| 11.9°    | 0.404       | 0.0672      | -0.0227     |
| 15.95°   | 0.552       | 0.1141      | -0.0362     |
| 19.95°   | 0.714       | 0.1828      | -0.0574     |
| 24.0°    | 0.880       | 0.2708      | -0.0845     |
| 26.05°   | 0.962       | 0.3216      | -0.0965     |
| 28.05°   | 1.035       | 0.3741      | -0.1090     |

Table 35

BALANCE MEASUREMENTS OF LIFT, DRAG AND  
PITCHING MOMENT

Wing BF/5

$V = 125 \text{ ft/sec.}, R = 1.6 \times 10^6$

$V = 250 \text{ ft/sec.}, R = 3.2 \times 10^6$

| $\alpha$ | $\bar{C}_L$ | $\bar{C}_D$ | $\bar{C}_m$ |
|----------|-------------|-------------|-------------|
| - 4.45°  | -0.027      | 0.0111      | -0.0198     |
| - 3.5°   | -0.017      | 0.0114      | -0.0187     |
| - 2.5°   | -0.006      | 0.0110      | -0.0166     |
| - 1.5°   | 0.009       | 0.0111      | -0.0150     |
| - 0.5°   | 0.020       | 0.0110      | -0.0139     |
| 0.5°     | 0.032       | 0.0111      | -0.0125     |
| 1.6°     | 0.044       | 0.0108      | -0.0107     |
| 2.6°     | 0.060       | 0.0127      | -0.0101     |
| 3.6°     | 0.074       | 0.0143      | -0.0101     |
| 5.6°     | 0.108       | 0.0197      | -0.0090     |
| 7.6°     | 0.145       | 0.0234      | -0.0138     |
| 9.6°     | 0.183       | 0.0375      | -0.0195     |
| 13.6°    | 0.275       | 0.0635      | -0.0323     |
| 17.6°    | 0.390       | 0.1154      | -0.0572     |
| 21.65°   | 0.511       | 0.1806      | -0.0866     |
| 25.65°   | 0.632       | 0.2650      | -0.1197     |
| 29.65°   | 0.756       | 0.3702      | -0.1550     |
| 33.7°    | 0.890       | 0.5056      | -0.1986     |
| 37.7°    | 0.988       | 0.6920      | -0.2451     |
| 41.7°    | 1.086       | 0.8864      | -0.2618     |
| 43.7°    | 1.100       | 0.9467      | -0.2612     |
| 45.7°    | 1.073       | 0.9771      | -0.2477     |
| 47.7°    | 1.021       | 1.0139      | -0.2339     |

| $\alpha$ | $\bar{C}_L$ | $\bar{C}_D$ | $\bar{C}_m$ |
|----------|-------------|-------------|-------------|
| - 4.4°   | -0.026      | 0.0131      | -0.0198     |
| - 3.5°   | -0.014      | 0.0123      | -0.0183     |
| - 2.5°   | -0.003      | 0.0121      | -0.0170     |
| - 1.5°   | 0.010       | 0.0121      | -0.0143     |
| - 0.5°   | 0.022       | 0.0123      | -0.0139     |
| 0.5°     | 0.033       | 0.0126      | -0.0129     |
| 1.6°     | 0.047       | 0.0139      | -0.0107     |
| 2.6°     | 0.063       | 0.0151      | -0.0102     |
| 3.6°     | 0.077       | 0.0164      | -0.0103     |
| 5.6°     | 0.111       | 0.0224      | -0.0114     |
| 7.6°     | 0.147       | 0.0302      | -0.0140     |
| 9.6°     | 0.186       | 0.0402      | -0.0180     |
| 13.6°    | 0.277       | 0.0673      | -0.0319     |
| 17.65°   | 0.382       | 0.1135      | -0.0539     |
| 21.65°   | 0.507       | 0.1804      | -0.0825     |
| 25.65°   | 0.631       | 0.2641      | -0.1156     |
| 29.65°   | 0.765       | 0.3755      | -0.1549     |

Table 36

BALANCE MEASUREMENTS OF LIFT, DRAG AND  
PITCHING MOMENT

Wing CF/1

$V = 125 \text{ ft/sec.}, R = 1.6 \times 10^6$

$V = 250 \text{ ft/sec.}, R = 3.2 \times 10^6$

| $\alpha$ | $\bar{C}_L$ | $\bar{C}_D$ | $\bar{C}_m$ |
|----------|-------------|-------------|-------------|
| - 6.85°  | -0.361      | 0.0266      | -0.0131     |
| - 5.9°   | -0.302      | 0.0228      | -0.0063     |
| - 4.7°   | -0.229      | 0.0133      | -0.0094     |
| - 3.75°  | -0.178      | 0.0118      | -           |
| - 2.6°   | -0.105      | 0.0082      | -0.0064     |
| - 1.6°   | -0.049      | 0.0086      | -           |
| - 0.4°   | 0.023       | 0.0069      | -0.0038     |
| 0.5°     | 0.076       | 0.0063      | -0.0020     |
| 2.7°     | 0.206       | 0.0091      | -           |
| 3.9°     | 0.286       | 0.0142      | 0.0004      |
| 4.8°     | 0.340       | 0.0166      | 0.0009      |
| 6.0°     | 0.418       | 0.0235      | 0.0009      |
| 7.0°     | 0.474       | 0.0258      | -           |
| 8.2°     | 0.556       | 0.0370      | -0.0018     |
| 9.1°     | 0.610       | 0.0404      | -0.0023     |
| 10.3°    | 0.684       | 0.0532      | -0.0026     |
| 11.3°    | 0.787       | 0.0560      | -           |
| 12.5°    | 0.820       | 0.0751      | -           |
| 13.4°    | 0.868       | 0.0780      | -0.0051     |
| 14.6°    | 0.943       | 0.0972      | -0.0043     |
| 15.5°    | 0.985       | 0.1005      | -           |
| 16.7°    | 1.053       | 0.1221      | -0.0049     |
| 17.65°   | 1.084       | 0.1257      | -0.0104     |

| $\alpha$ | $\bar{C}_L$ | $\bar{C}_D$ | $\bar{C}_m$ |
|----------|-------------|-------------|-------------|
| - 6.8°   | -0.364      | 0.0260      | -0.0128     |
| - 4.7°   | -0.242      | 0.0150      | -0.0095     |
| - 3.8°   | -0.181      | 0.0125      | -0.0077     |
| - 2.6°   | -0.113      | 0.0089      | -0.0066     |
| - 1.6°   | -0.049      | 0.0083      | -0.0052     |
| - 0.4°   | 0.022       | 0.0079      | -0.0041     |
| 0.5°     | 0.081       | 0.0071      | -0.0023     |
| 1.7°     | 0.159       | 0.0092      | -0.0015     |
| 2.7°     | 0.217       | 0.0101      | -0.0005     |
| 3.9°     | 0.288       | 0.0155      | 0           |
| 4.8°     | 0.351       | 0.0171      | 0.0006      |
| 6.05°    | 0.440       | 0.0262      | 0.0006      |
| 7.0°     | 0.493       | 0.0277      | 0.0010      |
| 9.1°     | 0.631       | 0.0419      | -0.0007     |
| 11.3°    | 0.775       | 0.0605      | -0.0021     |
| 13.45°   | 0.914       | 0.0827      | -0.0040     |
| 15.6°    | 1.035       | 0.1062      | -0.0063     |
| 17.7°    | 1.147       | 0.1336      | -0.0085     |

Table 37

BALANCE MEASUREMENTS OF LIFT, DRAG AND  
PITCHING MOMENT

Wing CF/2

$R = 3.2 \times 10^6$

$V = 125 \text{ ft/sec. } R = 1.6 \times 10^6$

$V = 250 \text{ ft/sec}$

| $\bar{C}_D$ | $\bar{C}_m$ |
|-------------|-------------|
| -           | -           |
| 0.0137      | -           |
| 0.0129      | -0.0078     |
| 0.0092      | -           |
| 0.0088      | -0.0051     |
| 0.0081      | -           |
| 0.0083      | -0.0019     |
| 0.0098      | -           |
| 0.0103      | 0.0010      |
| 0.0157      | -           |
| 0.0164      | 0.0029      |
| 0.0261      | 0.0034      |
| 0.0386      | 0.0031      |
| 0.0546      | 0.0014      |
| 0.0754      | -0.0026     |
| 0.0992      | -0.0059     |
| 0.1284      | -0.0107     |
| 0.1572      | -0.0156     |
| 0.1744      | -0.0185     |
| 0.1902      | -0.0210     |

| $\alpha$ | $\bar{C}_L$ | $\bar{C}_D$ | $\bar{C}_m$ |
|----------|-------------|-------------|-------------|
| - 8.5°   | -0.358      | 0.0363      | -           |
| - 6.5°   | -0.274      | 0.0229      | -           |
| - 5.9°   | -0.238      | 0.0198      | -0.0101     |
| - 4.4°   | -0.166      | 0.0122      | -           |
| - 3.8°   | -0.139      | 0.0119      | -0.0082     |
| - 2.3°   | -0.064      | 0.0081      | -           |
| - 1.7°   | -0.042      | 0.0082      | -0.0054     |
| - 0.3°   | 0.033       | 0.0080      | -           |
| 0.3°     | 0.053       | -           | -0.0019     |
| 1.8°     | 0.129       | 0.0088      | -           |
| 2.4°     | 0.152       | 0.0085      | 0.0012      |
| 3.9°     | 0.220       | 0.0156      | -           |
| 4.5°     | 0.253       | 0.0153      | 0.0029      |
| 6.5°     | 0.353       | 0.0240      | 0.0038      |
| 8.6°     | 0.461       | 0.0349      | 0.0006      |
| 10.7°    | 0.568       | 0.0532      | -0.0019     |
| 12.7°    | 0.670       | 0.0721      | -0.0030     |
| 14.8°    | 0.769       | 0.0941      | -0.0060     |
| 16.9°    | 0.872       | 0.1201      | -0.0106     |
| 18.9°    | 0.962       | 0.1487      | -0.0166     |
| 19.5°    | 0.987       | 0.1568      | -0.0188     |
| 19.6°    | 0.622       | -           | -           |

| $\alpha$ | $\bar{C}_L$ |
|----------|-------------|
| - 6.45°  | -0.279      |
| - 4.4°   | -0.176      |
| - 3.8°   | -0.152      |
| - 2.3°   | -0.075      |
| - 1.8°   | -0.052      |
| - 0.2°   | 0.025       |
| 0.3°     | 0.049       |
| 1.8°     | 0.127       |
| 2.4°     | 0.153       |
| 3.9°     | 0.230       |
| 4.4°     | 0.253       |
| 6.5°     | 0.365       |
| 8.6°     | 0.473       |
| 10.65°   | 0.580       |
| 12.7°    | 0.695       |
| 14.8°    | 0.802       |
| 16.9°    | 0.917       |
| 18.95°   | 1.013       |
| 20.0°    | 1.063       |
| 21.0°    | 1.100       |

Table 38

BALANCE MEASUREMENTS OF LIFT, DRAG AND  
PITCHING MOMENT

Wing CF/3

$V = 125 \text{ ft/sec.}, R = 1.6 \times 10^6$

$V = 250 \text{ ft/sec.}, R = 3.2 \times 10^6$

| $\alpha$ | $\bar{C}_L$ | $\bar{C}_D$ | $\bar{C}_m$ |
|----------|-------------|-------------|-------------|
| - 6.25°  | -0.173      | 0.0148      | -0.0124     |
| - 5.85°  | -0.158      | 0.0134      | -0.0112     |
| - 4.85°  | -0.125      | 0.0117      | -0.0115     |
| - 4.25°  | -0.103      | 0.0084      | -0.0106     |
| - 3.85°  | -0.093      | 0.0090      | -0.0103     |
| - 3.2°   | -0.073      | 0.0062      | -0.0092     |
| - 2.8°   | -0.0059     | 0.0067      | -0.0083     |
| - 2.2°   | -0.042      | 0.0056      | -0.0068     |
| - 1.8°   | -0.032      | 0.0054      | -0.0063     |
| - 1.2°   | -0.008      | 0.0045      | -0.0051     |
| - 0.8°   | 0           | 0.0048      | -0.0035     |
| - 0.2°   | 0.019       | 0.0044      | -0.0025     |
| 0.2°     | 0.031       | 0.0051      | -0.0017     |
| 1.85°    | 0.080       | 0.0054      | 0.0023      |
| 2.25°    | 0.090       | 0.0063      | 0.0026      |
| 4.25°    | 0.162       | 0.0090      | 0.0044      |
| 6.3°     | 0.230       | 0.0181      | 0.0054      |
| 8.3°     | 0.301       | 0.0275      | 0.0049      |
| 10.35°   | 0.380       | 0.0433      | 0.0017      |
| 12.4°    | 0.465       | 0.0620      | -0.0042     |
| 14.4°    | 0.546       | 0.0783      | -0.0090     |
| 16.45°   | 0.638       | 0.1111      | -0.0164     |
| 18.5°    | 0.720       | 0.1403      | -0.0247     |
| 19.5°    | 0.764       | 0.1563      | -0.0295     |
| 20.5°    | 0.805       | 0.1737      | -0.0344     |
| 21.5°    | 0.845       | 0.1920      | -0.0387     |
| 22.55°   | 0.885       | 0.2113      | -0.0439     |
| 23.55°   | 0.920       | 0.2311      | -0.0501     |

| $\alpha$ | $\bar{C}_L$ | $\bar{C}_D$ | $\bar{C}_m$ |
|----------|-------------|-------------|-------------|
| - 6.25°  | -0.177      | 0.0192      | -0.0125     |
| - 4.25°  | -0.108      | 0.0115      | -0.0107     |
| - 2.2°   | -0.041      | 0.0084      | -0.0070     |
| - 1.8°   | -0.034      | 0.0084      | -0.0064     |
| - 1.2°   | -0.011      | 0.0079      | -0.0049     |
| - 0.8°   | 0.008       | 0.0083      | -0.0036     |
| - 0.2°   | 0.023       | 0.0079      | -0.0022     |
| 0.2°     | 0.034       | 0.0080      | -0.0013     |
| 1.2°     | 0.068       | 0.0085      | 0.0014      |
| 1.85°    | 0.085       | 0.0091      | 0.0021      |
| 2.25°    | 0.094       | 0.0095      | 0.0027      |
| 4.25°    | 0.164       | 0.0145      | 0.0047      |
| 6.3°     | 0.239       | 0.0227      | 0.0053      |
| 8.3°     | 0.316       | 0.0335      | 0.0049      |
| 10.35°   | 0.398       | 0.0482      | 0.0026      |
| 12.4°    | 0.491       | 0.0684      | -0.0017     |
| 14.4°    | 0.571       | 0.0896      | -0.0069     |
| 16.45°   | 0.652       | 0.1144      | -0.0131     |
| 18.5°    | 0.755       | 0.1472      | -0.0219     |
| 20.5°    | 0.834       | 0.1827      | -0.0306     |
| 22.55°   | 0.921       | 0.2276      | -0.0405     |
| 23.55°   | 0.967       | 0.2431      | -0.0459     |
| 24.6°    | 1.009       | 0.2589      | -0.0522     |

Table 39

BALANCE MEASUREMENTS OF LIFT, DRAG AND  
PITCHING MOMENT

Wing CF/4

$V = 125 \text{ ft/sec}, R = 1.6 \times 10^6$

$V = 250 \text{ ft/sec}, R = 3.2 \times 10^6$

| $\alpha$ | $\bar{C}_L$ | $\bar{C}_D$ | $\bar{C}_m$ |
|----------|-------------|-------------|-------------|
| - 6.05°  | -0.126      | 0.0133      | -0.0111     |
| - 4.0°   | -0.073      | 0.0081      | -0.0097     |
| - 3.0°   | -0.048      | 0.0053      | -0.0081     |
| - 2.0°   | -0.026      | 0.0049      | -0.0059     |
| - 1.0°   | -0.006      | 0.0042      | -0.0033     |
| 0        | 0.012       | 0.0031      | -0.0012     |
| 1.0°     | 0.034       | 0.0044      | 0.0013      |
| 2.0°     | 0.061       | 0.0055      | 0.0028      |
| 3.0°     | 0.079       | 0.0054      | 0.0042      |
| 4.05°    | 0.113       | 0.0094      | 0.0054      |
| 6.05°    | 0.175       | 0.0170      | 0.0056      |
| 8.05°    | 0.237       | 0.0270      | 0.0042      |
| 10.1°    | 0.300       | 0.0382      | 0.0013      |
| 12.1°    | 0.365       | 0.0542      | -0.0032     |
| 14.1°    | 0.434       | 0.0730      | -0.0099     |
| 16.15°   | 0.502       | 0.0942      | -0.0170     |
| 18.15°   | 0.575       | 0.1252      | -0.0272     |
| 20.15°   | 0.652       | 0.1580      | -0.0376     |
| 22.2°    | 0.726       | 0.1938      | -0.0497     |
| 24.2°    | 0.803       | 0.2349      | -0.0636     |
| 25.25°   | 0.838       | 0.2579      | -0.0687     |
| 26.25°   | 0.877       | 0.2825      | -0.0785     |
| 27.25°   | 0.914       | 0.3060      | -0.0840     |
| 28.25°   | 0.948       | 0.3299      | -0.0934     |
| 29.25°   | 0.981       | 0.3628      | -0.1029     |

| $\alpha$ | $\bar{C}_L$ | $\bar{C}_D$ | $\bar{C}_m$ |
|----------|-------------|-------------|-------------|
| - 3.0°   | -0.049      | 0.0087      |             |
| - 2.0°   | -0.027      | 0.0080      |             |
| - 1.0°   | -0.003      | 0.0073      |             |
| 0°       | 0.016       | 0.0073      |             |
| 1.0°     | 0.039       | 0.0075      |             |
| 2.0°     | 0.060       | 0.0087      |             |
| 4.05°    | 0.119       | 0.0131      |             |
| 6.05°    | 0.183       | 0.0201      |             |
| 8.05°    | 0.238       | 0.0286      |             |
| 10.1°    | 0.307       | 0.0413      |             |
| 12.1°    | 0.378       | 0.0582      |             |
| 14.15°   | 0.452       | 0.0793      |             |
| 16.15°   | 0.521       | 0.1023      |             |
| 18.15°   | 0.602       | 0.1331      |             |
| 20.2°    | 0.679       | 0.1664      |             |
| 23.2°    | 0.795       | 0.2248      |             |
| 24.25°   | 0.836       | 0.2483      |             |

Table 40

BALANCE MEASUREMENTS OF LIFT, DRAG AND  
PITCHING MOMENT

Wing CF/5

$V = 125 \text{ ft/sec.}, R = 1.6 \times 10^6$

$V = 250 \text{ ft/sec.}, R = 3.2 \times 10^6$

| $\alpha$ | $\bar{C}_L$ | $\bar{C}_D$ | $\bar{C}_m$ |
|----------|-------------|-------------|-------------|
| - 6.2°   | -0.073      | 0.0084      | -0.0024     |
| - 4.2°   | -0.043      | 0.0057      | -0.0040     |
| - 3.2°   | -0.032      | 0.0037      | -0.0025     |
| - 2.8°   | -0.027      | 0.0087      | -           |
| - 2.2°   | -0.016      | 0.0056      | 0           |
| - 1.8°   | -0.014      | 0.0087      | -           |
| - 1.2°   | -0.005      | 0.0043      | 0.0016      |
| - 0.8°   | -0.005      | 0.0087      | -           |
| - 0.2°   | 0.008       | 0.0053      | 0.0031      |
| 0.2°     | 0.008       | 0.0076      | -           |
| 1.2°     | 0.027       | 0.0076      | -           |
| 1.8°     | 0.027       | 0.0053      | 0.0064      |
| 2.2°     | 0.038       | 0.0084      | -           |
| 3.2°     | 0.048       | 0.0092      | -           |
| 3.8°     | 0.054       | 0.0053      | 0.0072      |
| 4.2°     | 0.065       | 0.0097      | -           |
| 5.8°     | 0.086       | 0.0118      | 0.0071      |
| 7.8°     | 0.118       | 0.0186      | 0.0048      |
| 9.8°     | 0.161       | 0.0270      | -0.0006     |
| 11.85°   | 0.204       | 0.0386      | -0.0106     |
| 13.85°   | 0.258       | 0.0555      | -0.0181     |
| 15.85°   | 0.304       | 0.0723      | -0.0261     |
| 17.85°   | 0.354       | 0.0951      | -0.0377     |
| 19.85°   | 0.405       | 0.1228      | -0.0491     |
| 21.85°   | 0.456       | 0.1524      | -0.0659     |
| 23.85°   | 0.501       | 0.1798      | -0.0762     |
| 25.9°    | 0.563       | 0.2226      | -0.0960     |
| 27.9°    | 0.622       | 0.2665      | -0.1163     |
| 29.9°    | 0.678       | 0.3118      | -0.1314     |
| 31.9°    | 0.731       | 0.3678      | -0.1574     |

| $\alpha$ | $\bar{C}_L$ | $\bar{C}_D$ | $\bar{C}_m$ |
|----------|-------------|-------------|-------------|
| - 3.2°   | -0.033      | 0.0103      | -0.0052     |
| - 2.8°   | -0.026      | 0.0104      | -0.0066     |
| - 2.2°   | -0.020      | 0.0098      | -0.0035     |
| - 1.8°   | -0.013      | 0.0102      | -0.0049     |
| - 1.2°   | -0.008      | 0.0099      | -0.0018     |
| - 0.8°   | -0.003      | 0.0098      | -0.0029     |
| - 0.2°   | 0.005       | 0.0093      | 0           |
| 0.2°     | 0.009       | 0.0098      | 0.0010      |
| 1.2°     | 0.021       | 0.0103      | 0.0004      |
| 1.8°     | 0.028       | 0.0104      | 0.0029      |
| 2.2°     | 0.033       | 0.0107      | 0.0020      |
| 3.8°     | 0.056       | 0.0127      | 0.0032      |
| 5.8°     | 0.089       | 0.0169      | 0.0028      |
| 7.8°     | 0.126       | 0.0227      | 0.0004      |
| 9.8°     | 0.165       | 0.0313      | -0.0039     |
| 11.8°    | 0.210       | 0.0427      | -0.0102     |
| 13.8°    | 0.254       | 0.0561      | -0.0174     |
| 15.8°    | 0.311       | 0.0768      | -0.0305     |
| 17.85°   | 0.364       | 0.0995      | -0.0403     |
| 19.85°   | 0.424       | 0.1288      | -0.0552     |
| 21.85°   | 0.486       | 0.1636      | -0.0730     |
| 23.85°   | 0.536       | 0.1959      | -0.0860     |



Table 41  
BOUNDARY LAYER TRANSITION POSITION AT  
CENTRE SECTION: B SERIES WINGS

| $V = 125 \text{ ft/sec}; R = 1.6 \times 10^6$ |               |               | $V = 250 \text{ ft/sec}; R = 3.2 \times 10^6$ |               |               |
|---|---------------|---------------|---|---------------|---------------|
| $\alpha$                                      | $x_T/c$       |               | $\alpha$                                      | $x_T/c$       |               |
|   | Upper surface | Lower surface |   | Upper surface | Lower surface |
| BF/1  |               |               |   |               |               |
| $-4.15^\circ$                                 | 0.72          | 0.010         | $-2.0^\circ$                                  | 0.52          | 0.010         |
| $-3.05^\circ$                                 | 0.68          | 0.010         | $-0.95^\circ$                                 | 0.49          | -             |
| $-2.0^\circ$                                  | 0.67          | 0.010         | $0.15^\circ$                                  | 0.45          | 0.53          |
| $-0.95^\circ$                                 | 0.59          | -             | $1.2^\circ$                                   | 0.42          | 0.59          |
| $0.15^\circ$                                  | 0.56          | 0.71          | $2.3^\circ$                                   | 0.42          | 0.64          |
| $1.2^\circ$                                   | 0.49          | 0.72          | $3.35^\circ$                                  | 0.31          | 0.70          |
| $2.3^\circ$                                   | 0.46          | 0.80          | $4.45^\circ$                                  | 0.21          | 0.71          |
| $3.35^\circ$                                  | 0.42          | 0.88          | $5.55^\circ$                                  | 0.15          | 0.85          |
| $4.45^\circ$                                  | 0.38          | -             | $6.6^\circ$                                   | 0.13          | 1.00          |
| $5.55^\circ$                                  | 0.30          | -             | $7.7^\circ$                                   | 0.10          | -             |
| $6.6^\circ$                                   | 0.19          | -             | $9.75^\circ$                                  | 0.063         | -             |
| $7.7^\circ$                                   | 0.15          | -             | $9.8^\circ$                                   | 0.063         | -             |
| $8.75^\circ$                                  | 0.13          | -             | $10.9^\circ$                                  | 0.031         | -             |
| $9.8^\circ$                                   | 0.094         | -             |   |               |               |
| $11.95^\circ$                                 | 0.024         |               |   |               |               |
| BF/2  |               |               |   |               |               |
| No measurements                               |               |               |   |               |               |

Table 41 (Contd)

BOUNDARY LAYER TRANSITION POSITION AT  
CENTRE SECTION: B SERIES WINGS

| $V = 125 \text{ ft/sec}; R = 1.6 \times 10^6$ |               |               | $V = 250 \text{ ft/sec}; R = 3.2 \times 10^6$ |               |               |
|---|---------------|---------------|---|---------------|---------------|
| $\alpha$                                      | $X_T/C$       |               | $\alpha$                                      | $X_T/C$       |               |
|   | Upper surface | Lower surface |   | Upper surface | Lower surface |
| BF/3  |               |               |   |               |               |
| - 4.1°  | 0.69          | 0.01          | - 3.1°  | 0.52          | Leading edge  |
| - 2.1°  | 0.62          | 0.01          | - 2.1°  | 0.51          | "             |
| - 0.05°                                       | 0.57          | -             | - 1.1°  | 0.47          | "             |
| 1.95°   | 0.48          | 0.71          | - 0.05°                                       | 0.47          | "             |
| 4.0°  | 0.43          | 0.80          | 0.95°   | 0.44          | "             |
| 6.0°  | 0.40          | 0.88          | 1.95°   | 0.43          | 0.54          |
| 8.05°   | 0.25          | 0.96          | 4.0°  | 0.38          | 0.65          |
| 10.05°  | 0.15          | 1.00          | 6.0°  | 0.20          | 0.72          |
| 12.1°   | 0.13          | -             | 8.05°   | 0.16          | 0.75          |
| 14.15°  | 0.083         | -             | 10.1°   | 0.11          | 0.83          |
| 16.15°  | 0.052         | -             | 12.1°   | 0.083         | 0.96          |
|   |               |               | 14.15°  | 0.063         | 1.00          |
| BF/4  |               |               |   |               |               |
| - 4.3°  | 0.67          | Leading edge  | - 4.25°                                       | 0.62          | Leading edge  |
| - 2.3°  | 0.62          | "             | - 2.2°  | 0.55          | "             |
| - 0.3°  | 0.56          | "             | - 0.2°  | 0.49          | "             |
| 1.75°   | 0.50          | 0.71          | 1.8°  | 0.46          | 0.62          |
| 3.75°   | 0.46          | 0.75          | 3.8°  | 0.40          | 0.67          |
| 5.75°   | 0.41          | 0.79          | 5.85°   | 0.33          | 0.67          |
| 7.75°   | 0.33          | 0.90          | 7.85°   | 0.22          | 0.75          |
| 9.8°  | 0.21          | 1.00          | 9.85°   | 0.14          | 0.80          |
| 13.8°   | 0.13          | -             | 11.9°   | 0.10          | 0.83          |
| 17.85°  | 0.061         | -             | 15.95°  | 0.042         | 1.00          |
|   |               |               | 17.95°  | 0.031         | -             |
| BF/5  |               |               |   |               |               |
| - 4.45°                                       | 0.70          | Leading edge  | - 4.4°  | 0.58          | Leading edge  |
| - 2.45°                                       | 0.60          | "             | - 0.4°  | 0.48          | "             |
| - 0.45°                                       | 0.54          | 0.58          | 3.6°  | 0.42          | 0.58          |
| 1.6°  | 0.50          | 0.71          | 7.6°  | 0.27          | 0.67          |
| 3.6°  | 0.46          | 0.75          | 9.6°  | 0.19          | 0.69          |
| 7.6°  | 0.35          | 0.92          | 13.6°   | 0.11          | 0.75          |
| 9.6°  | 0.29          | 0.96          | 15.6°   | 0.10          | 0.79          |
| 13.6°   | 0.15          | 1.00          | 17.65°  | 0.063         | 1.00          |
| 17.6°   | 0.13          | -             |   |               |               |
| 19.6°   | 0.083         | -             |   |               |               |
| 21.65°  | 0.063         | -             |   |               |               |

Table 42  
BOUNDARY LAYER TRANSITION POSITION AT  
CENTRE SECTION: C SERIES WINGS

| $V = 125 \text{ ft/sec}; R = 1.6 \times 10^6$ |                   |               | $V = 250 \text{ ft/sec}; R = 3.2 \times 10^6$ |                   |               |
|---|-------------------|---------------|---|-------------------|---------------|
| $\alpha$                                      | $x_T/C$           |               | $\alpha$                                      | $x_T/C$           |               |
|   | Upper surface     | Lower surface |   | Upper surface     | Lower surface |
| CF/1  |                   |               |   |                   |               |
| No measurements                               |                   |               |   |                   |               |
| CF/2  |                   |               |   |                   |               |
| No measurements                               |                   |               |   |                   |               |
| CF/3  |                   |               |   |                   |               |
| - 3.85°                                       | 0.71              | Leading edge  | - 1.8°  | 0.48              | Leading edge  |
| - 1.8°  | 0.64              | "             | 0.2°  | 0.43              | 0.54          |
| 0.2°  | 0.57              | 0.64          | 2.25°   | 0.33              | 0.56          |
| 1.2°  | 0.53              | 0.69          | 4.25°   | 0.18              | 0.62          |
| 2.25°   | 0.48              | 0.72          | 6.3°  | 0.12              | 0.74          |
| 3.25°   | 0.46              | 0.77          | 8.3°  | 0.07 <sub>3</sub> | 0.81          |
| 4.25°   | 0.43              | 0.77          | 10.35°  | 0.06 <sub>3</sub> | 0.84          |
| 5.25°   | 0.34              | 0.82          | 12.4°   | 0.03 <sub>1</sub> | 0.89          |
| 6.3°  | 0.26              | 0.87          |   |                   |               |
| 7.3°  | 0.19              | 0.91          |   |                   |               |
| 8.3°  | 0.15              | 0.95          |   |                   |               |
| 9.35°   | 0.10              | 0.97          |   |                   |               |
| 10.35°  | 0.06 <sub>3</sub> | 1.00          |   |                   |               |
| 11.35°  | 0.05 <sub>2</sub> | 1.00          |   |                   |               |

Table 42 (Contd)

BOUNDARY LAYER TRANSITION POSITION AT  
CENTRE SECTION: C SERIES WINGS

| $V = 125 \text{ ft/sec}; R = 1.6 \times 10^6$ |                   |               | $V = 250 \text{ ft/sec}; R = 3.2 \times 10^6$ |                   |               |
|---|-------------------|---------------|---|-------------------|---------------|
| $\alpha$                                      | $X_T/C$           |               | $\alpha$                                      | $X_T/C$           |               |
|   | Upper surface     | Lower surface |   | Upper surface     | Lower surface |
| $CF/4$  |                   |               |   |                   |               |
| - 4.0°  | 0.68              | Leading edge  | - 2.0°  | 0.49              | Leading edge  |
| - 2.0°  | 0.65              | " "           | 0°  | 0.45              | 0.53          |
| 0°  | 0.58              | 0.65          | 1.0°  | 0.39              | 0.56          |
| 1.0°  | 0.55              | 0.69          | 2.0°  | 0.39              | 0.59          |
| 2.0°  | 0.50              | 0.71          | 3.0°  | 0.35              | 0.59          |
| 3.0°  | 0.45              | 0.77          | 4.05°   | 0.21              | 0.64          |
| 4.05°   | 0.43              | 0.80          | 6.05°   | 0.17              | 0.71          |
| 5.05°   | 0.38              | 0.83          | 7.05°   | 0.11              | 0.73          |
| 6.05°   | 0.30              | 0.88          | 8.05°   | 0.09 <sub>4</sub> | 0.76          |
| 7.05°   | 0.19              | 0.91          | 9.1°  | 0.07 <sub>3</sub> | 0.79          |
| 8.05°   | 0.14              | 0.97          | 10.1°   | 0.06 <sub>2</sub> | 0.82          |
| 10.1°   | 0.07 <sub>3</sub> | 1.00          |   |                   |               |
| 12.1°   | 0.05 <sub>2</sub> | -             |   |                   |               |
| $CF/5$  |                   |               |   |                   |               |
| - 2.2°  | 0.62              | Leading edge  | - 2.2°  | 0.51              | Leading edge  |
| - 0.2°  | 0.54              | 0.70          | - 0.2°  | 0.48              | 0.56          |
| 1.8°  | 0.50              | 0.74          | 1.8°  | 0.42              | 0.59          |
| 3.8°  | 0.45              | 0.79          | 3.8°  | 0.38              | 0.65          |
| 5.8°  | 0.38              | 0.85          | 4.8°  | 0.28              | 0.65          |
| 6.8°  | 0.31              | 0.88          | 5.8°  | 0.20              | 0.64          |
| 7.8°  | 0.24              | 0.89          | 7.8°  | 0.14              | 0.72          |
| 9.8°  | 0.16              | 0.97          | 9.8°  | 0.08 <sub>3</sub> | 0.75          |
| 10.85°  | 0.13              | 1.00          | 11.8°   | 0.06 <sub>3</sub> | 0.81          |
| 11.85°  | 0.12              | -             |   |                   |               |
| 13.85°  | 0.06 <sub>7</sub> | -             |   |                   |               |
| 15.85°  | 0.05 <sub>4</sub> | -             |   |                   |               |

Table 43

ZERO LIFT ANGLES OF BF AND CF SERIES WINGS

| $\alpha_0$ |        |        |        |        |        |        |        |        |        |        |
|------------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
|            | BF/1   | BF/2   | BF/3   | BF/4   | BF/5   | CF/1   | CF/2   | CF/3   | CF/4   | CF/5   |
| Calc.      | -1.96° | -2.04° | -2.21° | -2.32° | -2.52° | -0.76° | -0.78° | -0.80° | -0.82° | -0.84° |
| Exp.       | -2.1°  | -2.0°  | -2.2°  | -2.3°  | -2.2°  | -0.8°  | -0.8°  | -0.8°  | -0.7°  | -0.6°  |

Table 44

ZERO LIFT ANGLES AT CENTRE SECTION OF BP SERIES WINGS

| $\alpha_0$ |        |        |        |        |        |        |
|------------|--------|--------|--------|--------|--------|--------|
|            | BP/0   | BP/1   | BP/2   | BP/3   | BP/4   | BP/5   |
| Calc.      | -1.92° | -1.96° | -2.04° | -2.21° | -2.32° | -2.52° |
| Exp.       | -2.1°  | -2.2°  | -2.3°  | -2.2°  | -2.2°  | -2.2°  |

Table 45

## CALCULATED PRESSURE COEFFICIENTS ON WINGS OF SYMMETRICAL SECTION

Wing AP/1

| X/c    | $\alpha_e = 0^\circ$<br>$C_N = 0$ | $\alpha_e = 2^\circ$<br>$C_N = 0.212$ |        | $\alpha_e = 5^\circ$<br>$C_N = 0.527$ |        | $\alpha_e = 8^\circ$<br>$C_N = 0.838$ |       |
|--------|-----------------------------------|---------------------------------------|--------|---------------------------------------|--------|---------------------------------------|-------|
|        | $C_p$                             | $C_p$                                 |        | $C_p$                                 |        | $C_p$                                 |       |
|        |                                   | U.S.                                  | L.S.   | U.S.                                  | L.S.   | U.S.                                  | L.S.  |
| 0.0096 | 0.050                             | -0.703                                | 0.586  | -2.231                                | 0.979  | -4.221                                | 0.875 |
| 0.0381 | -0.215                            | -0.635                                | 0.146  | -1.373                                | 0.570  | -2.233                                | 0.852 |
| 0.0843 | -0.277                            | -0.551                                | -0.027 | -1.003                                | 0.300  | -1.500                                | 0.568 |
| 0.1464 | -0.302                            | -0.498                                | -0.116 | -0.811                                | 0.140  | -1.143                                | 0.367 |
| 0.2222 | -0.311                            | -0.460                                | -0.167 | -0.690                                | 0.038  | -0.928                                | 0.228 |
| 0.3087 | -0.308                            | -0.423                                | -0.194 | -0.598                                | -0.028 | -0.775                                | 0.130 |
| 0.4025 | -0.246                            | -0.333                                | -0.159 | -0.463                                | -0.029 | -0.591                                | 0.098 |
| 0.5000 | -0.182                            | -0.249                                | -0.115 | -0.316                                | -0.013 | -0.438                                | 0.089 |
| 0.5975 | -0.121                            | -0.171                                | -0.068 | -0.243                                | 0.012  | -0.310                                | 0.094 |
| 0.6913 | -0.064                            | -0.102                                | -0.024 | -0.155                                | 0.039  | -0.202                                | 0.105 |
| 0.7778 | -0.016                            | -0.044                                | 0.015  | -0.082                                | 0.063  | -0.114                                | 0.116 |
| 0.8536 | 0.026                             | 0.006                                 | 0.048  | -0.020                                | 0.085  | -0.041                                | 0.127 |
| 0.9157 | 0.067                             | 0.054                                 | 0.083  | 0.038                                 | 0.110  | 0.027                                 | 0.142 |
| 0.9619 | 0.118                             | 0.110                                 | 0.127  | 0.103                                 | 0.146  | 0.100                                 | 0.169 |
| 0.9904 | 0.196                             | 0.194                                 | 0.201  | 0.193                                 | 0.211  | 0.198                                 | 0.226 |

Table 46

CALCULATED PRESSURE COEFFICIENTS ON WINGS OF SYMMETRICAL SECTIONWing AP/2

| x/c    | $\alpha_e = 0^\circ$<br>$C_N = 0$ | $\alpha_e = 3^\circ$<br>$C_N = 0.267$ |        | $\alpha_e = 7^\circ$<br>$C_N = 0.615$ |        | $\alpha_e = 12^\circ$<br>$C_N = 1.033$ |        |
|--------|-----------------------------------|---------------------------------------|--------|---------------------------------------|--------|--|--------|
|        | $C_p$                             | $C_p$                                 |        | $C_p$                                 |        | $C_p$                                  |        |
|        |                                   | U.S.                                  | L.S.   | U.S.                                  | L.S.   | U.S.                                   | L.S.   |
| 0.0096 | 0.052                             | -0.783                                | 0.868  | -2.903                                | 0.917  | -6.632                                 | -0.208 |
| 0.0381 | -0.212                            | -0.815                                | 0.276  | -1.790                                | 0.735  | -3.253                                 | 0.992  |
| 0.0843 | -0.274                            | -0.699                                | 0.060  | -1.277                                | 0.433  | -2.082                                 | 0.772  |
| 0.1464 | -0.298                            | -0.562                                | -0.052 | -0.936                                | 0.243  | -1.431                                 | 0.552  |
| 0.2222 | -0.307                            | -0.503                                | -0.125 | -0.777                                | -0.141 | -1.114                                 | -0.376 |
| 0.3087 | -0.304                            | -0.451                                | -0.157 | -0.648                                | 0.034  | -0.886                                 | 0.260  |
| 0.4025 | -0.242                            | -0.352                                | -0.131 | -0.493                                | 0.019  | -0.658                                 | 0.203  |
| 0.5000 | -0.179                            | -0.260                                | -0.093 | -0.363                                | 0.024  | -0.476                                 | 0.174  |
| 0.5975 | -0.117                            | -0.178                                | -0.051 | -0.251                                | 0.041  | -0.329                                 | 0.163  |
| 0.6913 | -0.061                            | -0.106                                | -0.011 | -0.157                                | 0.062  | -0.207                                 | 0.161  |
| 0.7778 | -0.013                            | -0.042                                | 0.020  | -0.080                                | 0.079  | -0.111                                 | 0.161  |
| 0.8536 | 0.028                             | 0.006                                 | 0.056  | -0.016                                | 0.100  | -0.030                                 | 0.165  |
| 0.9157 | 0.069                             | 0.055                                 | 0.089  | 0.044                                 | 0.122  | 0.044                                  | 0.174  |
| 0.9619 | 0.120                             | 0.112                                 | 0.132  | 0.110                                 | 0.155  | 0.120                                  | 0.195  |
| 0.9904 | 0.198                             | 0.196                                 | 0.204  | 0.201                                 | 0.219  | 0.218                                  | 0.248  |

Table 47

CALCULATED PRESSURE COEFFICIENTS ON WINGS OF SYMMETRICAL SECTIONWing AP/3

| x/c    | $\alpha_e = 0^\circ$ | $\alpha_e = 3^\circ$ |        | $\alpha_e = 7^\circ$ |        | $\alpha_e = 12^\circ$ |       |
|--------|----------------------|----------------------|--------|----------------------|--------|-----------------------|-------|
|        | $C_N = 0$            | $C_N = 0.216$        |        | $C_N = 0.499$        |        | $C_N = 0.839$         |       |
|        | $C_p$                | $C_p$                |        | $C_p$                |        | $C_p$                 |       |
|        |                      | U.S.                 | L.S.   | U.S.                 | L.S.   | U.S.                  | L.S.  |
| 0.0096 | 0.057                | -1.024               | 0.733  | -3.075               | 0.992  | -6.558                | 0.278 |
| 0.0381 | -0.205               | -0.708               | 0.216  | -1.497               | 0.642  | -2.651                | 0.944 |
| 0.0843 | -0.265               | -0.562               | 0.006  | -0.992               | 0.325  | -1.571                | 0.643 |
| 0.1464 | -0.288               | -0.487               | -0.097 | -0.761               | 0.142  | -1.109                | 0.410 |
| 0.2222 | -0.296               | -0.438               | -0.154 | -0.626               | 0.031  | -0.853                | 0.251 |
| 0.3087 | -0.291               | -0.396               | -0.184 | -0.530               | -0.038 | -0.683                | 0.143 |
| 0.4025 | -0.230               | -0.305               | -0.150 | -0.398               | -0.039 | -0.498                | 0.106 |
| 0.5000 | -0.167               | -0.222               | -0.108 | -0.286               | -0.022 | -0.350                | 0.094 |
| 0.5975 | -0.107               | -0.146               | -0.062 | -0.190               | 0.005  | -0.229                | 0.098 |
| 0.6913 | -0.052               | -0.081               | -0.019 | -0.109               | 0.033  | -0.130                | 0.109 |
| 0.7778 | -0.006               | -0.026               | 0.018  | -0.043               | 0.059  | -0.050                | 0.121 |
| 0.8536 | 0.033                | 0.020                | 0.051  | 0.012                | 0.082  | 0.015                 | 0.133 |
| 0.9157 | 0.073                | 0.066                | 0.085  | 0.064                | 0.109  | 0.075                 | 0.151 |
| 0.9619 | 0.122                | 0.119                | 0.130  | 0.123                | 0.148  | 0.139                 | 0.181 |
| 0.9904 | 0.200                | 0.200                | 0.204  | 0.207                | 0.216  | 0.227                 | 0.242 |



Table 48

CALCULATED PRESSURE COEFFICIENTS ON WINGS OF SYMMETRICAL SECTIONWing AP/4

|        | $\alpha_e = 0^\circ$ | $\alpha_e = 3^\circ$ |        | $\alpha_e = 7^\circ$ |        | $\alpha_e = 12^\circ$ |       |
|--------|----------------------|----------------------|--------|----------------------|--------|-----------------------|-------|
|        | $C_N = 0$            | $C_N = 0.176$        |        | $C_N = 0.408$        |        | $C_N = 0.686$         |       |
|        | $C_P$                | $C_P$                |        | $C_P$                |        | $C_P$                 |       |
|        |                      | U.S.                 | L.S.   | U.S.                 | L.S.   | U.S.                  | L.S.  |
| 0.0096 | 0.060                | -0.922               | 0.698  | -2.749               | 1.000  | -5.811                | 0.191 |
| 0.0381 | -0.200               | -0.629               | 0.170  | -1.287               | 0.562  | -2.229                | 0.881 |
| 0.0813 | -0.258               | -0.503               | -0.029 | -0.848               | 0.248  | -1.301                | 0.541 |
| 0.1464 | -0.279               | -0.438               | -0.122 | -0.651               | 0.079  | -0.914                | 0.313 |
| 0.2222 | -0.284               | -0.395               | -0.171 | -0.537               | -0.019 | -0.703                | 0.169 |
| 0.3087 | -0.278               | -0.358               | -0.194 | -0.456               | -0.076 | -0.563                | 0.076 |
| 0.4025 | -0.217               | -0.273               | -0.155 | -0.339               | -0.066 | -0.404                | 0.054 |
| 0.5000 | -0.155               | -0.195               | -0.110 | -0.239               | -0.042 | -0.277                | 0.054 |
| 0.5975 | -0.097               | -0.125               | -0.064 | -0.154               | -0.011 | -0.174                | 0.067 |
| 0.6913 | -0.047               | -0.065               | -0.021 | -0.082               | 0.020  | -0.088                | 0.084 |
| 0.7778 | -0.002               | -0.015               | 0.016  | -0.024               | 0.049  | -0.020                | 0.101 |
| 0.8536 | 0.036                | 0.027                | 0.048  | 0.025                | 0.074  | 0.036                 | 0.118 |
| 0.9157 | 0.074                | 0.070                | 0.083  | 0.072                | 0.103  | 0.088                 | 0.139 |
| 0.9619 | 0.122                | 0.121                | 0.128  | 0.127                | 0.143  | 0.146                 | 0.174 |
| 0.9904 | 0.199                | 0.200                | 0.203  | 0.209                | 0.214  | 0.229                 | 0.239 |

Table 49

## CALCULATED PRESSURE COEFFICIENTS ON WINGS OF SYMMETRICAL SECTION

Wing AP/5

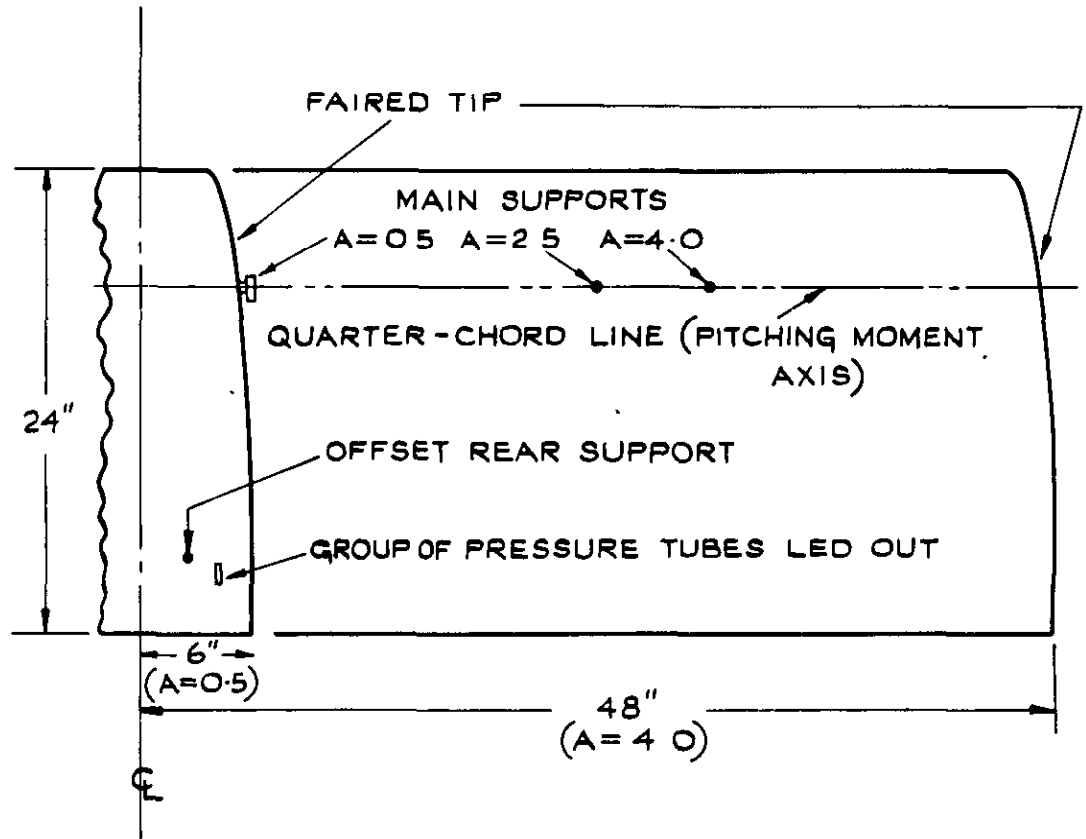
| X/C    | $\alpha_e = 0^\circ$ | $\alpha_e = 4^\circ$ |        | $\alpha_e = 10^\circ$ |        | $\alpha_e = 16^\circ$ |       |
|--------|----------------------|----------------------|--------|-----------------------|--------|-----------------------|-------|
|        | $C_N = 0$            | $C_N = 0.149$        |        | $C_N = 0.367$         |        | $C_N = 0.567$         |       |
|        | $C_p$                | $C_p$                |        | $C_p$                 |        | $C_p$                 |       |
|        |                      | U.S.                 | L.S.   | U.S.                  | L.S.   | U.S.                  | L.S.  |
| 0.0096 | 0.062                | -0.938               | 0.709  | -3.058                | 0.988  | -5.838                | 0.432 |
| 0.0381 | -0.192               | -0.571               | 0.147  | -1.204                | 0.558  | -1.890                | 0.842 |
| 0.0843 | -0.240               | -0.438               | -0.045 | -0.734                | 0.232  | -1.017                | 0.481 |
| 0.1464 | -0.248               | -0.369               | -0.122 | -0.534                | 0.074  | -0.672                | 0.269 |
| 0.2222 | -0.244               | -0.323               | -0.155 | -0.420                | -0.009 | -0.489                | 0.147 |
| 0.3087 | -0.234               | -0.287               | -0.169 | -0.345                | -0.056 | -0.375                | 0.073 |
| 0.4025 | -0.175               | -0.210               | -0.129 | -0.241                | -0.041 | -0.246                | 0.064 |
| 0.5000 | -0.121               | -0.144               | -0.087 | -0.158                | -0.018 | -0.147                | 0.070 |
| 0.5975 | -0.073               | -0.087               | -0.047 | -0.090                | 0.009  | -0.068                | 0.084 |
| 0.6913 | -0.030               | -0.039               | -0.011 | -0.034                | 0.035  | -0.006                | 0.100 |
| 0.7778 | 0.004                | 0                    | 0.019  | 0.011                 | 0.058  | 0.044                 | 0.116 |
| 0.8536 | 0.036                | 0.033                | 0.045  | 0.049                 | 0.079  | 0.084                 | 0.131 |
| 0.9157 | 0.068                | 0.069                | 0.076  | 0.087                 | 0.105  | 0.125                 | 0.153 |
| 0.9619 | 0.114                | 0.116                | 0.120  | 0.136                 | 0.145  | 0.174                 | 0.188 |
| 0.9904 | 0.190                | 0.194                | 0.195  | 0.213                 | 0.216  | 0.250                 | 0.254 |

SYMBOLS

|                        |   |
|------------------------|---|
| A                      | aspect ratio  |
| c                      | chord   |
| t/c                    | thickness/chord ratio   |
| $X_T$                  | chordwise position of boundary layer transition                                       |
| h                      | height of tip vortex sheet  |
| $\alpha$               | angle of incidence  |
| $\alpha_i$             | induced incidence at wing due to trailing vortices                                    |
| $\alpha_{io}$          | half of the incidence induced by the trailing vortices at a great distance downstream |
| $\alpha_e$             | effective incidence   |
| $\alpha_o$             | zero lift angle   |
| $\alpha_B$             | reduction in incidence due to boundary layer  |
| $C_N, \bar{C}_N$       | local and total normal force coefficient  |
| $C_L, \bar{C}_L$       | local and total lift coefficient  |
| $C_T, \bar{C}_T$       | local and total tangential force coefficient  |
| $C_D, \bar{C}_D$       | local and total drag coefficient  |
| $C_{Do}, \bar{C}_{Do}$ | local and total profile drag coefficient  |
| $C_{Di}, \bar{C}_{Di}$ | local and total vortex drag coefficient   |
| $C_m, \bar{C}_m$       | local and total pitching moment coefficient   |
| $C_{mo}, \bar{C}_{mo}$ | local and total pitching moment coefficient at zero lift                              |
| $C_p$                  | pressure coefficient  |
| $\Delta C_p$           | local loading coefficient at a point on the wing                                      |
| a                      | sectional lift slope = $\partial C_L / \partial \alpha_e$                             |
| k                      | boundary layer reduction factor   |
| m                      | camber line parameter   |
| n                      | parameter used in loading calculations  |

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| 5          | G. G. Brebner                             | The application of camber and twist to swept wings in incompressible flow<br>A.R.C. C.P. No. 171, March 1952   |
| 6          | G. G. Brebner<br>J. A. Bagley             | Pressure and boundary layer measurements on a two-dimensional wing at low speed<br>A.R.C. R. & M. 2886, February 1952  |
| 7          | D. H. Peckham                             | Low speed wind tunnel tests to determine the effects of taper on low aspect-ratio wings at zero incidence<br>A.R.C. C.P. No. 571, August 1960                              |
| 8          | H. Multhopp                               | Methods for calculating the lift distribution of wings (Subsonic lifting - surface theory)<br>A.R.C. R. & M. 2884, January 1950  |
| 9          | W. Mangler<br>J. Rotta                    | Aerofoils with tip plates.<br>M.O.S. A.V.A. Monograph F, 1.6, R. & T. 1023, 1947   |
| 10         | D. Kettle<br>D. Küchemann                 | The effect of endplates on swept wings<br>A.R.C. C.P. 104, June 1951   |
| 11         | J. Weber<br>D. Küchemann<br>G. G. Brebner | Low speed tests on 45° sweptback wings<br>A.R.C. R. & M. 2882, May 1951  |



CHORDWISE POSITIONS OF PRESSURE HOLES

| $\frac{x}{c}$ | Value |
|---------------|-------|
| $\frac{x}{c}$ | = 0   |
|               | 0.005 |
|               | 0.015 |
|               | 0.030 |
|               | 0.050 |
|               | 0.075 |
|               | 0.100 |
|               | 0.200 |
|               | 0.300 |
|               | 0.400 |
|               | 0.500 |
|               | 0.650 |
|               | 0.750 |
|               | 0.850 |
|               | 0.950 |

FIG. 1 SKETCH OF MODELS

$\Delta\alpha_1$  = CORRECTION FOR  
TUNNEL PITCH

$\Delta\alpha_2$  = CORRECTION FOR  
ASYMMETRY OR DATUM  
LINE ERROR

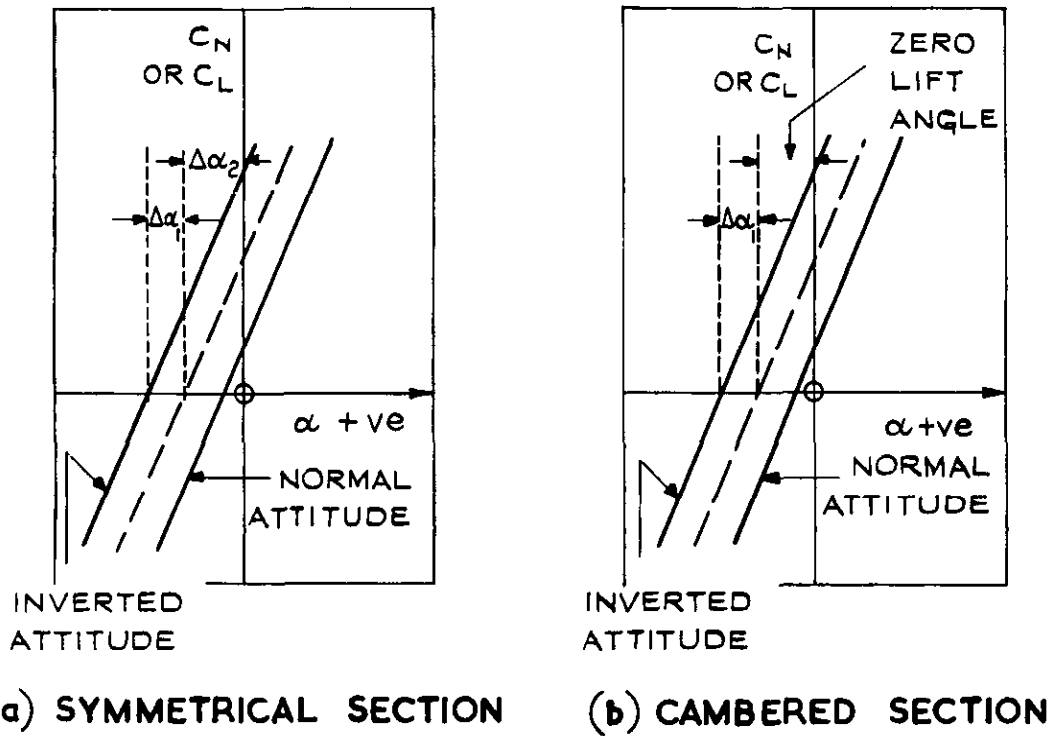
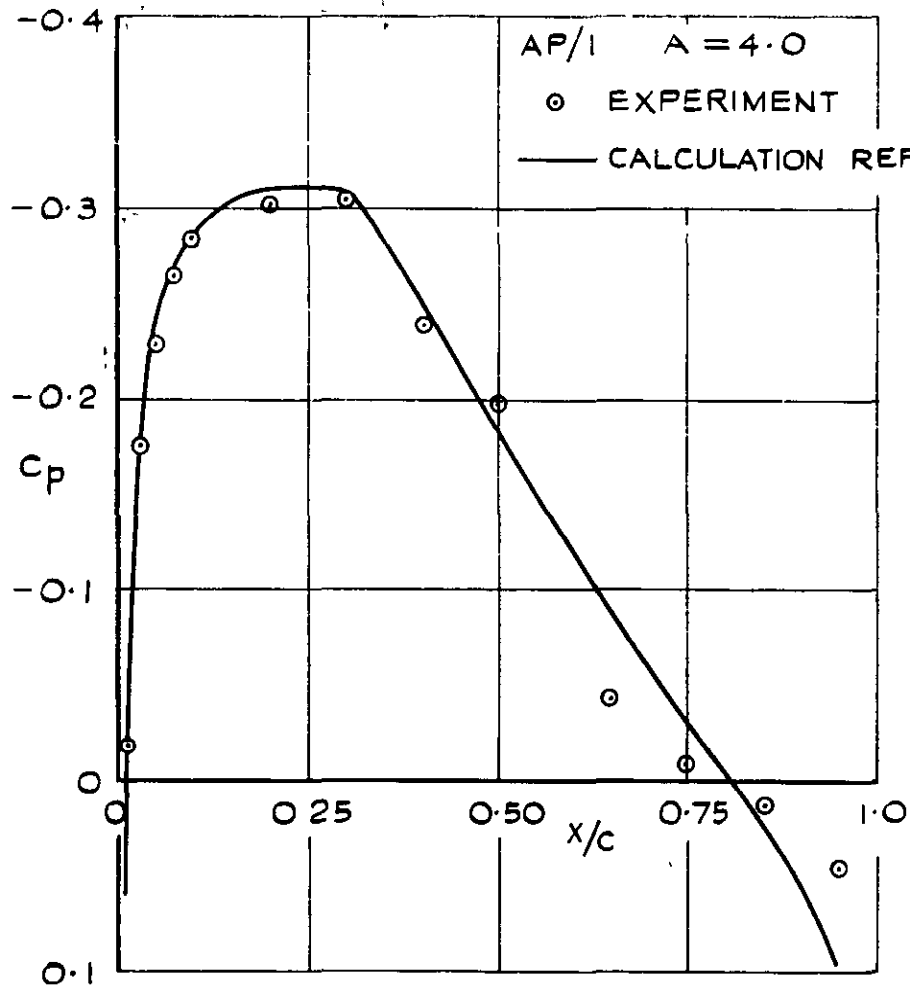
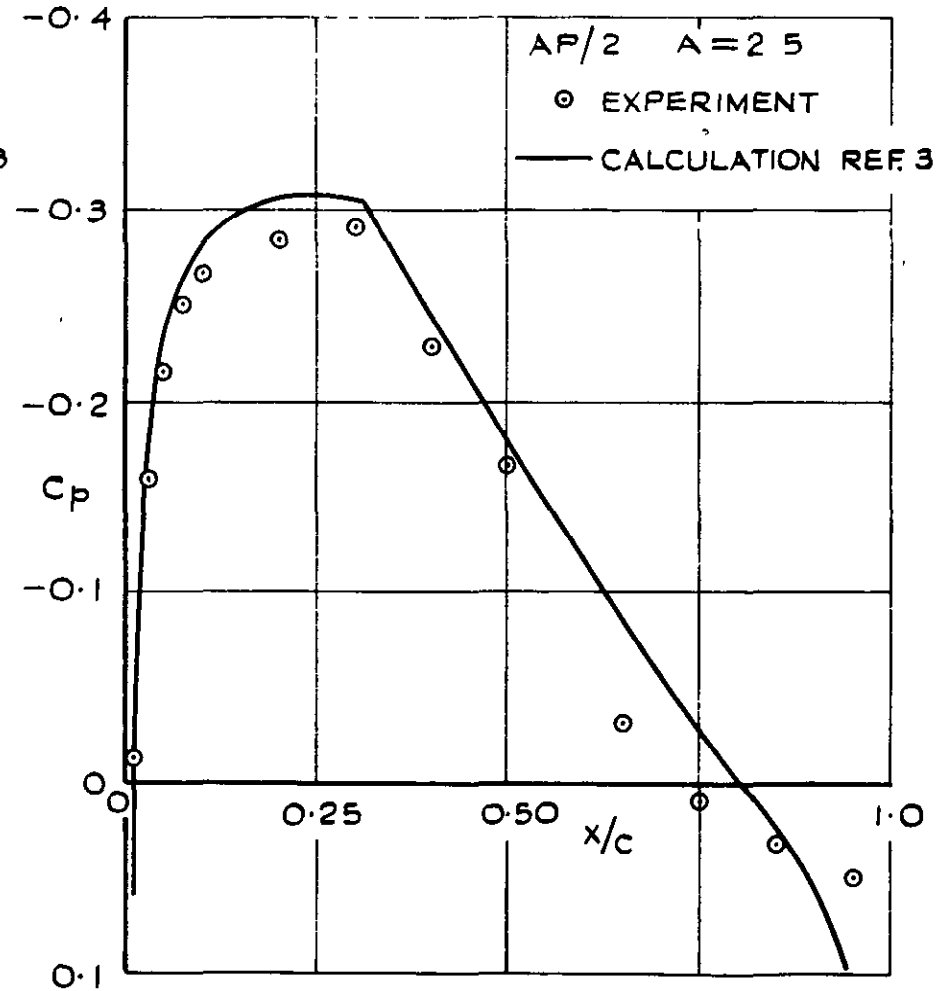


FIG. 2. METHOD OF CORRECTING INCIDENCE FOR  
TUNNEL PITCH AND DATUM LINE ERROR

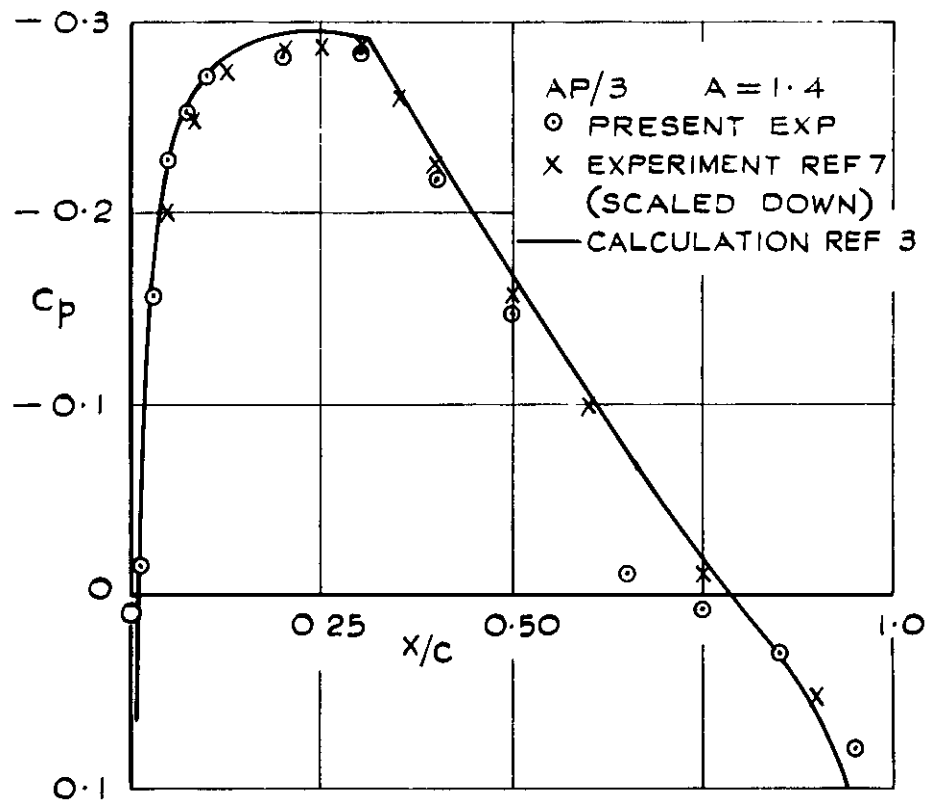


(a) AP/1

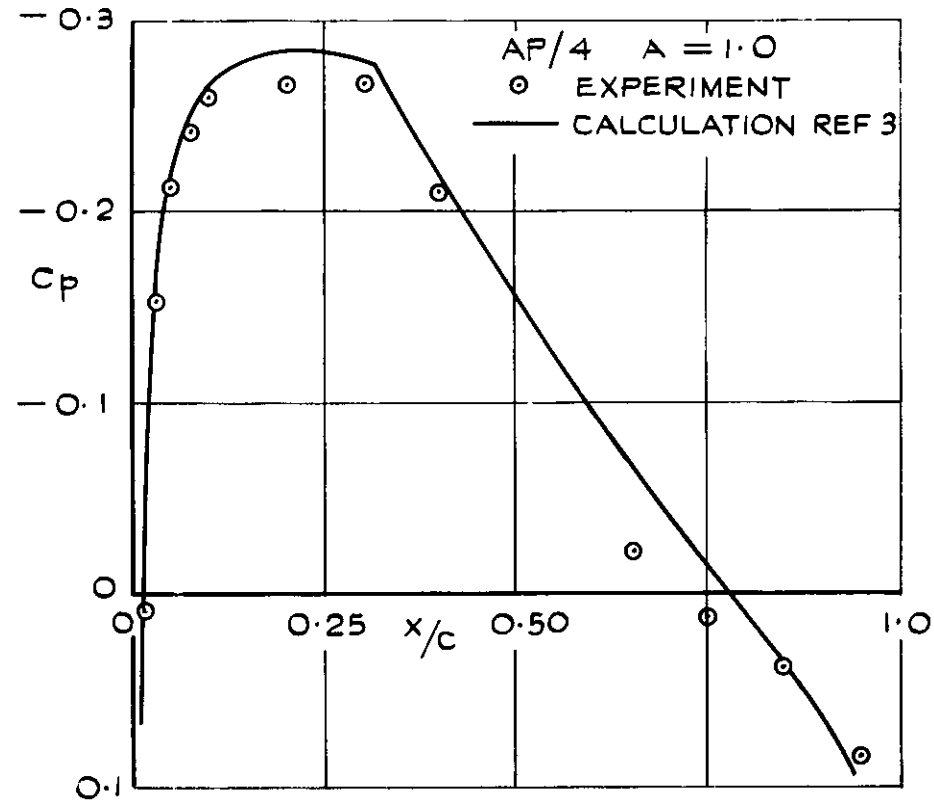


(b) AP/2

FIG. 3 ZERO LIFT PRESSURE DISTRIBUTION AT THE CENTRE SECTION OF AP WINGS



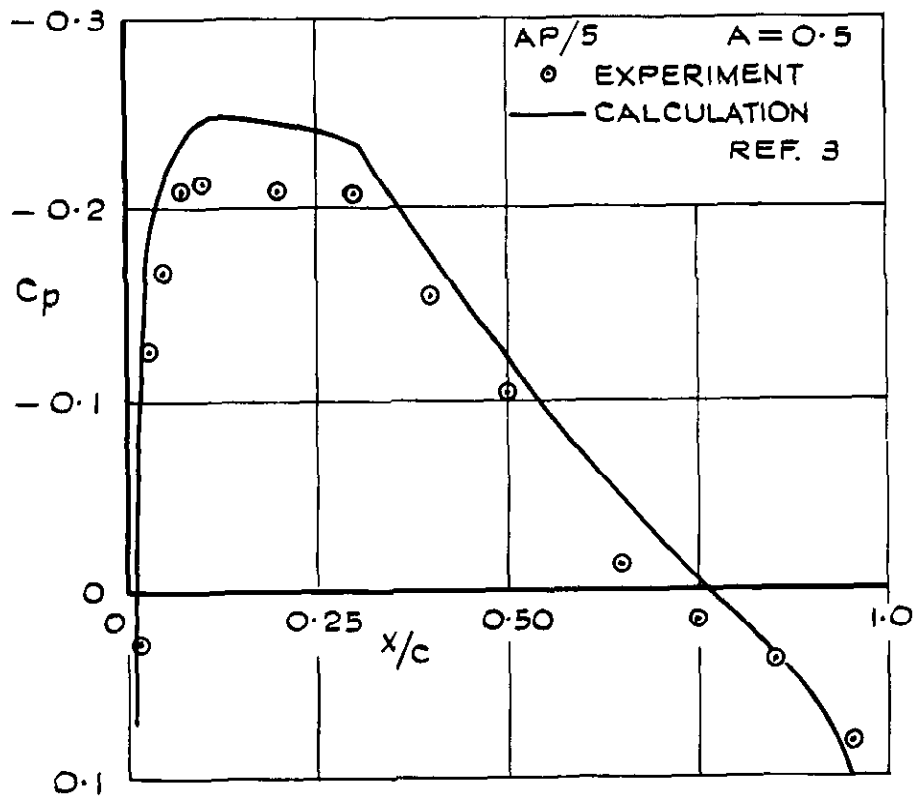
(c) AP/3



(d) AP/4

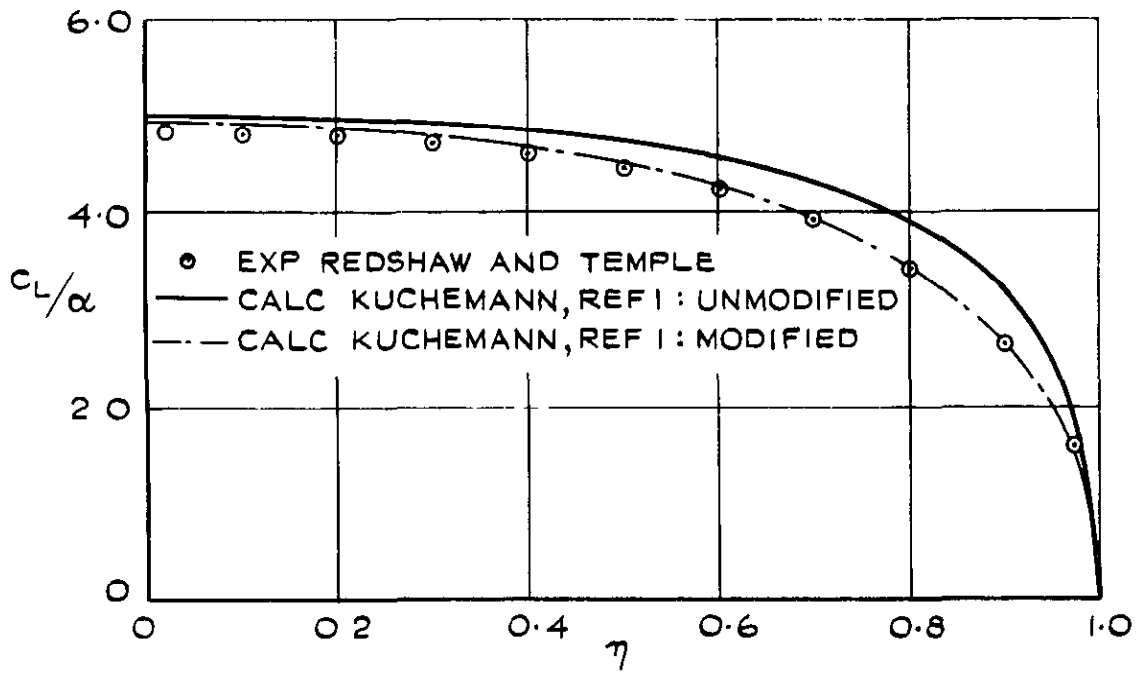
FIG. 3 (CONTD)



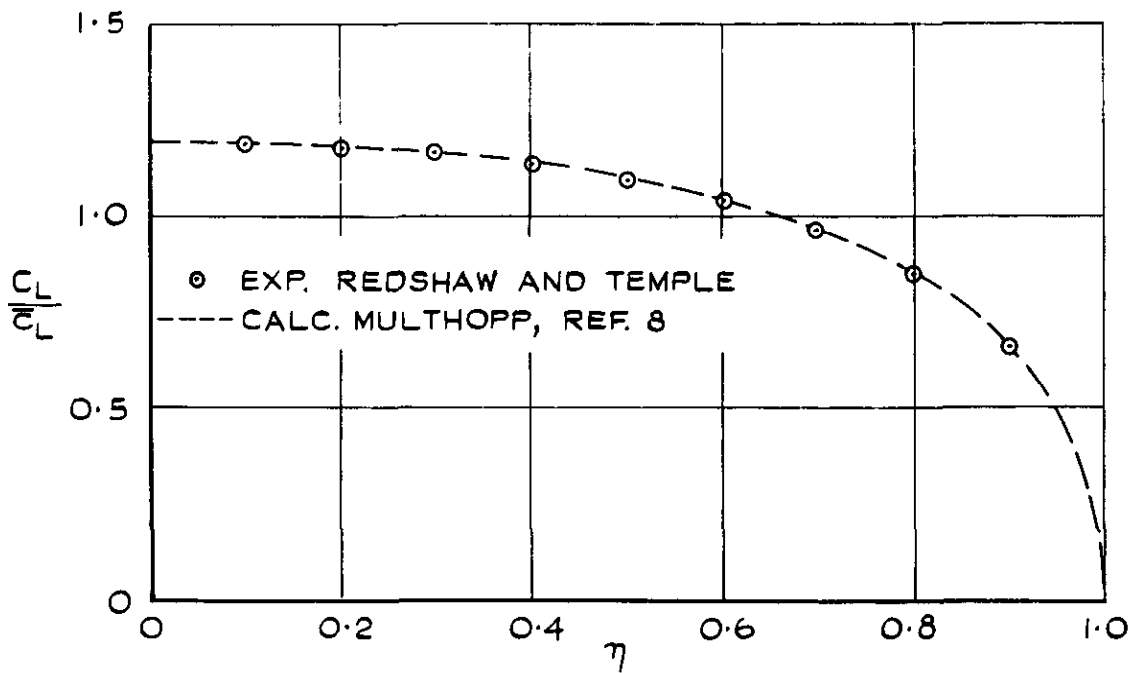


(e)  $AP/5$

FIG. 3 (CONT'D)

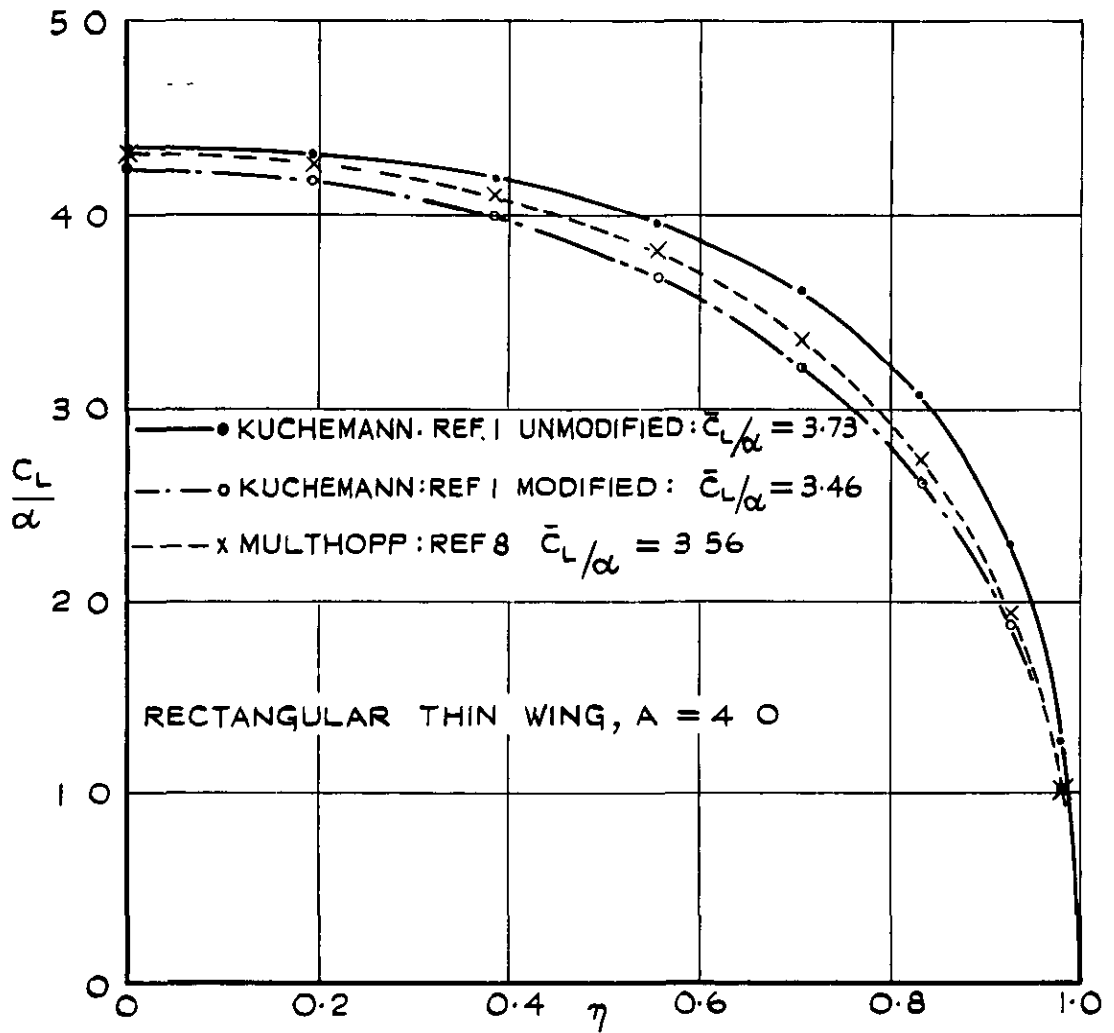


(a)

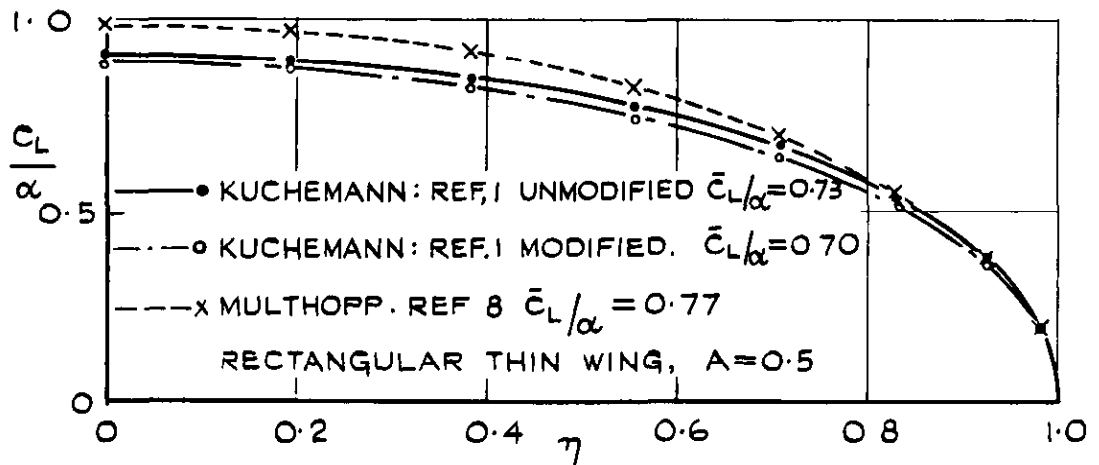


(b)

FIG.4 EXPERIMENTAL AND CALCULATED SPANWISE LIFT DISTRIBUTION ON A THIN RECTANGULAR WING OF ASPECT RATIO 6



(a) ASPECT RATIO = 4.0



(b) ASPECT RATIO = 0.5

FIG. 5 CALCULATED SPANWISE LIFT DISTRIBUTIONS ON TWO THIN RECTANGULAR WINGS

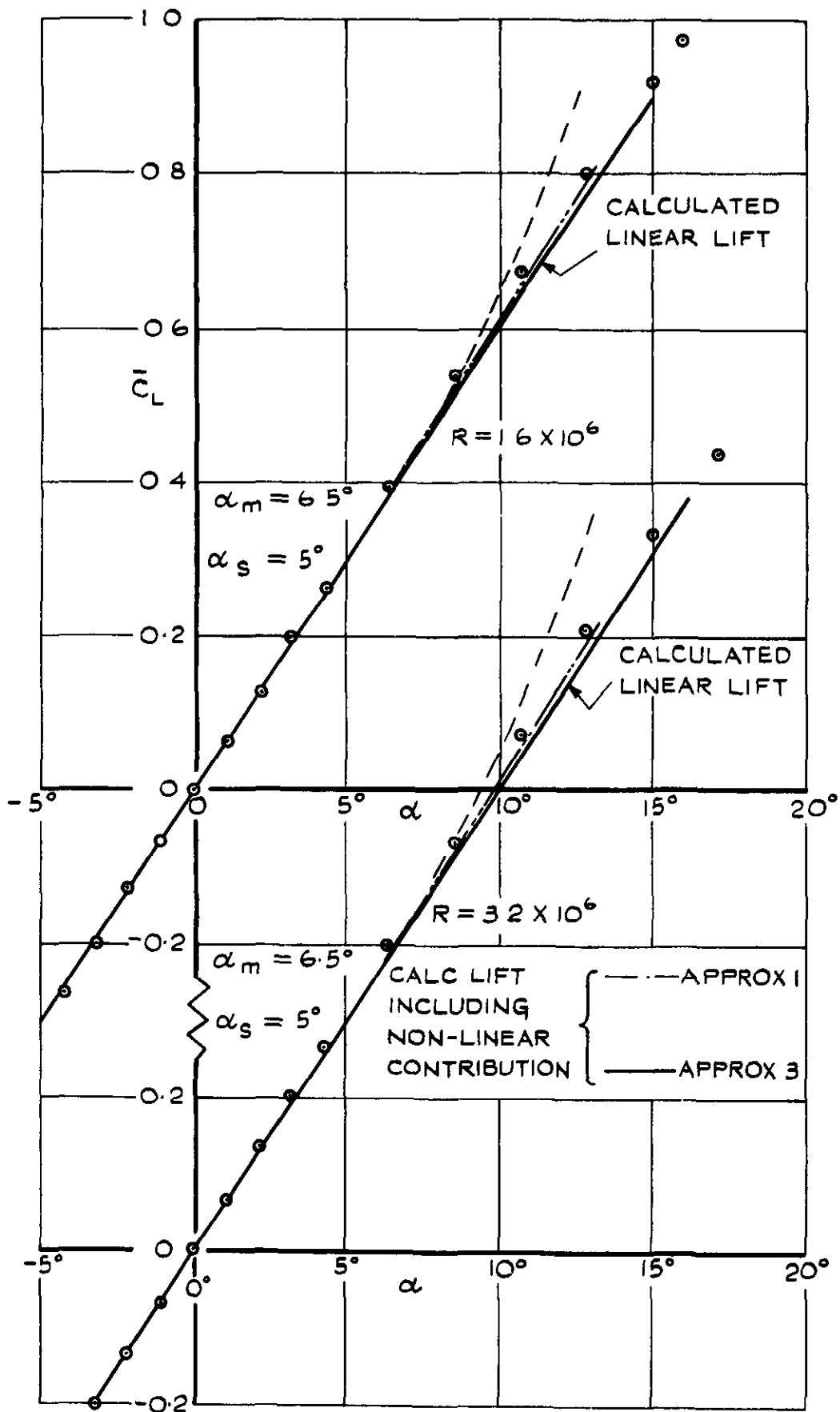


FIG. 6 LIFT v INCIDENCE, WING AF/1

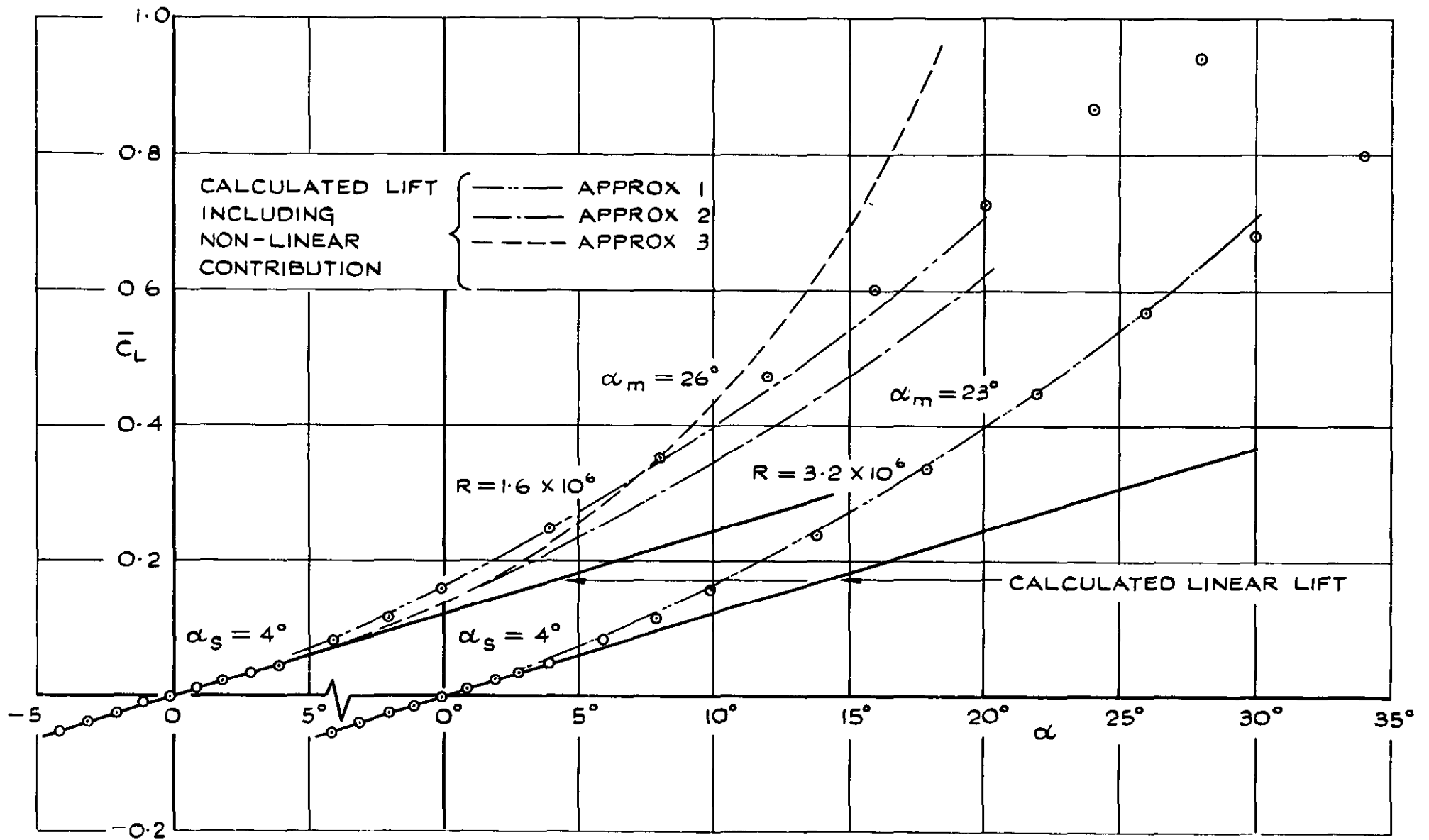


FIG.7 LIFT v INCIDENCE, WING AF/5

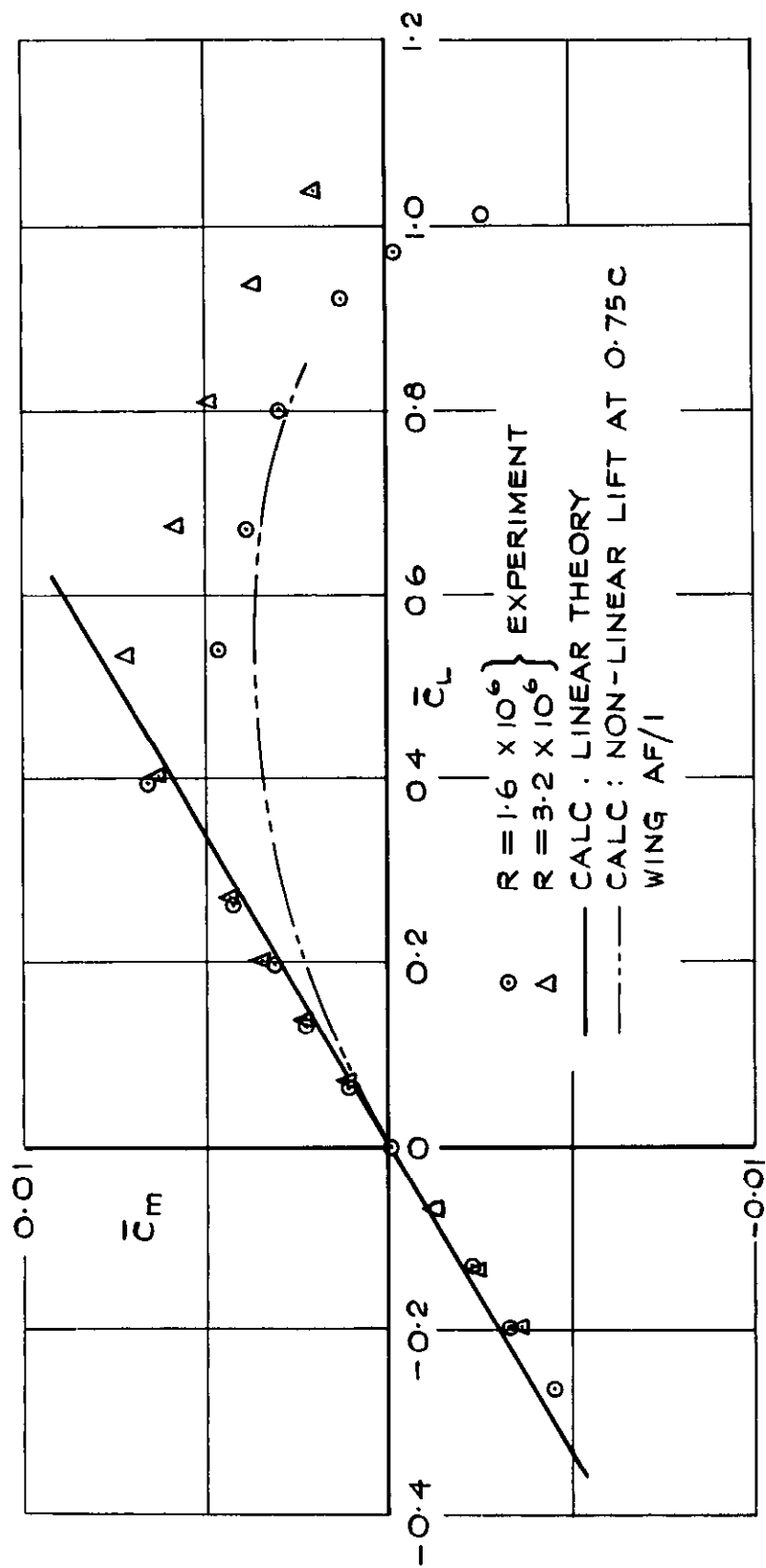


FIG.8 PITCHING MOMENT, WING AF/I

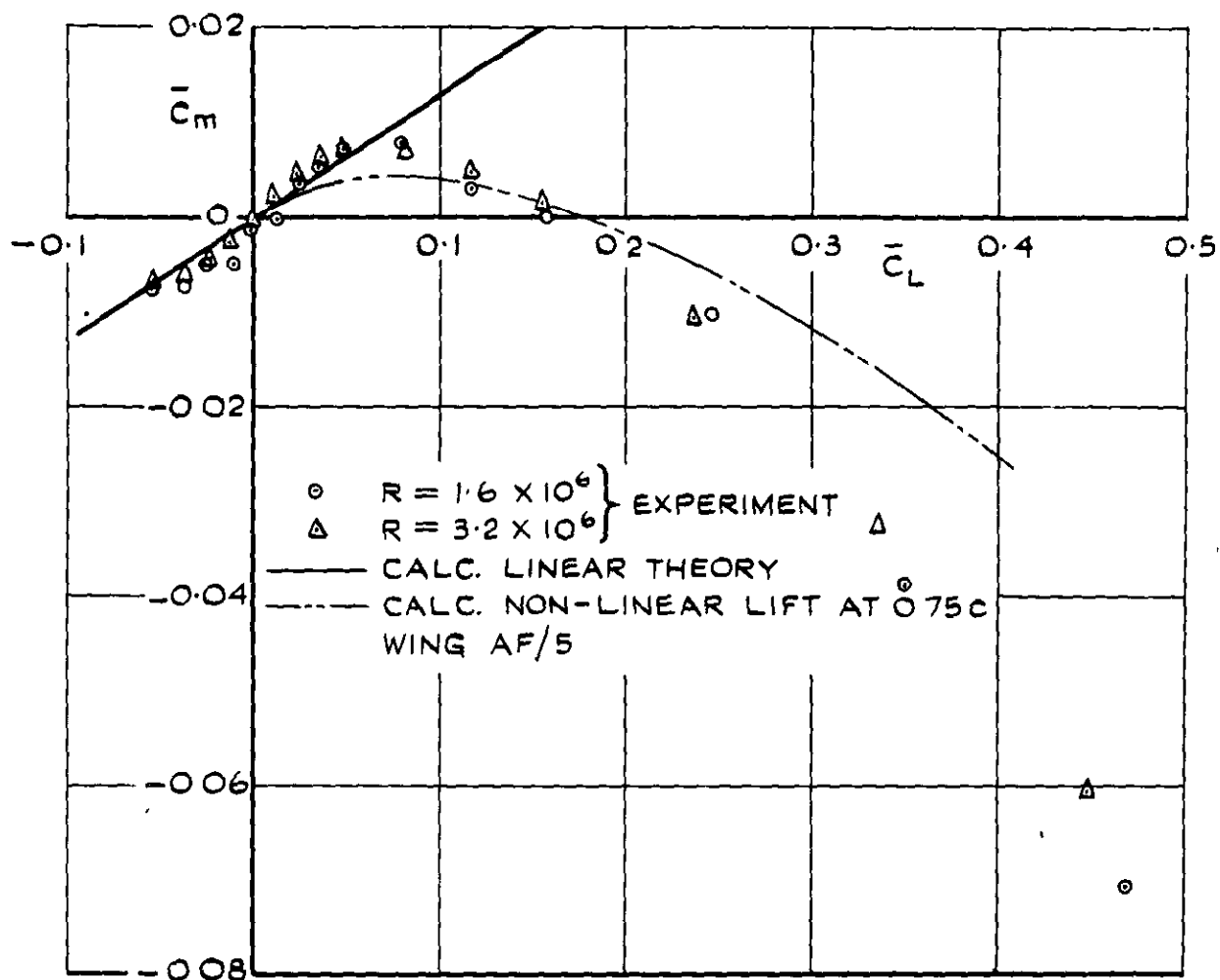


FIG. 9 PITCHING MOMENT, WING AF/5

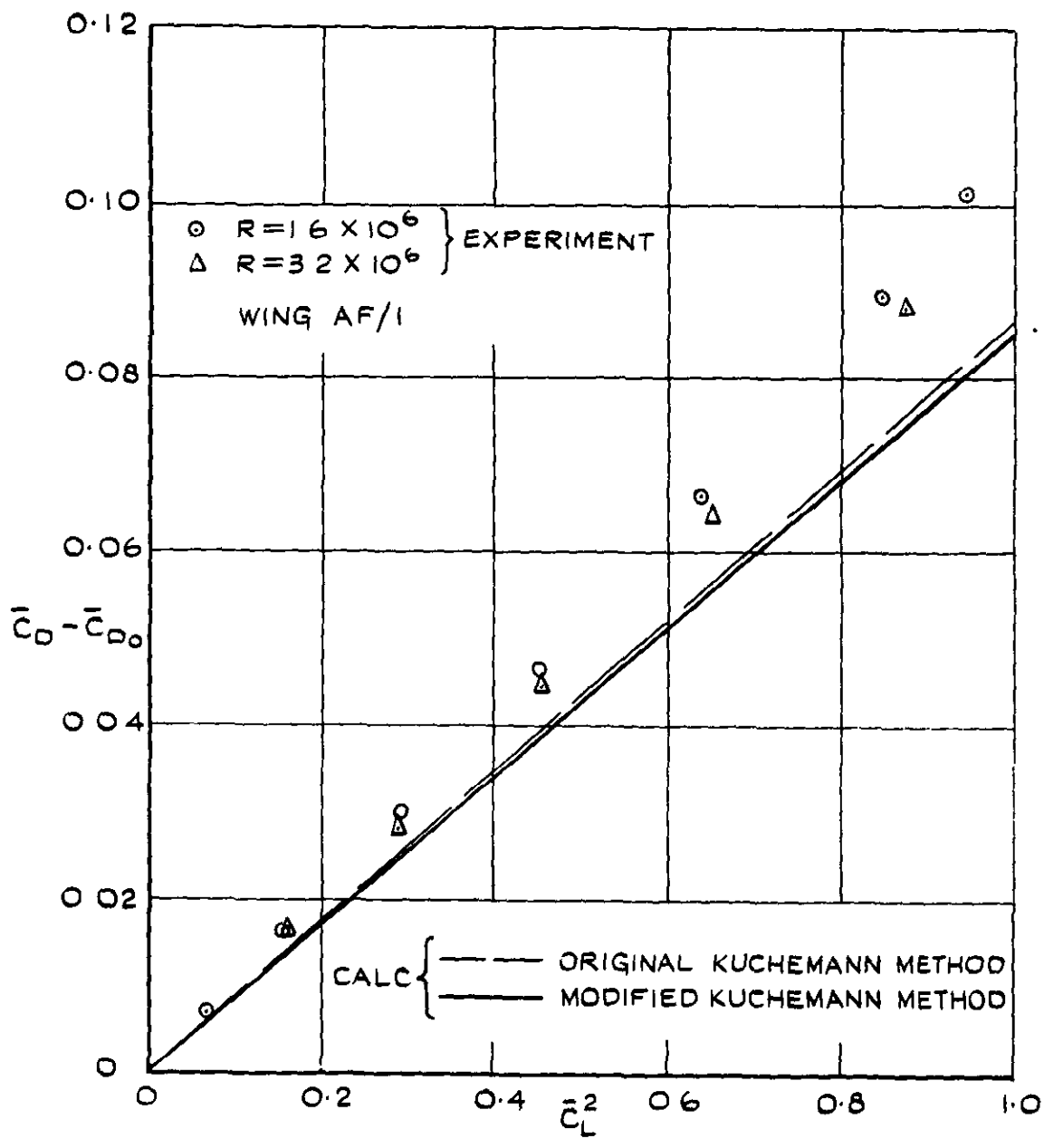


FIG. 10 DRAG DUE TO LIFT AND BOUNDARY LAYER, WING AF/1



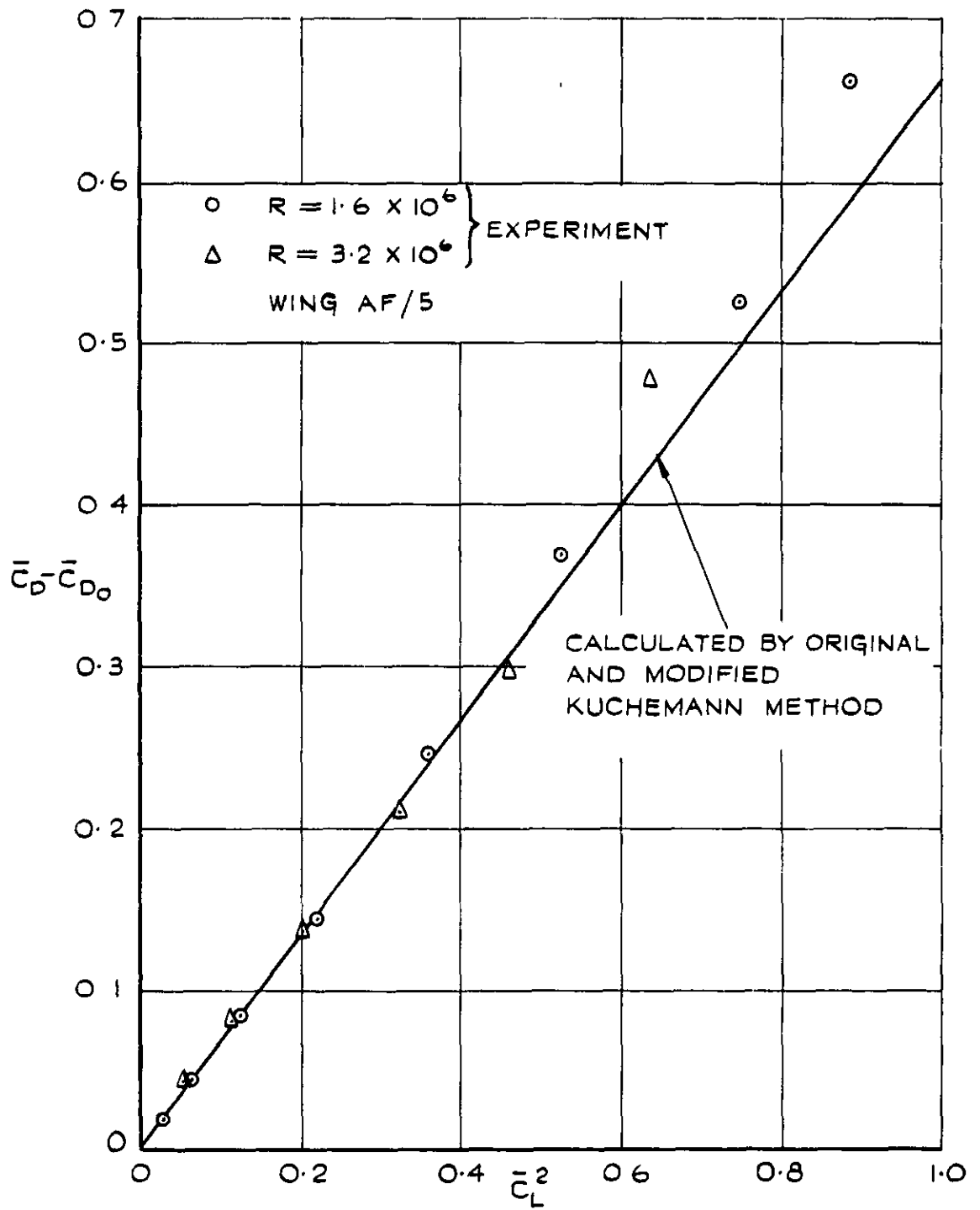


FIG. 11 DRAG DUE TO LIFT AND BOUNDARY LAYER, WING AF/5

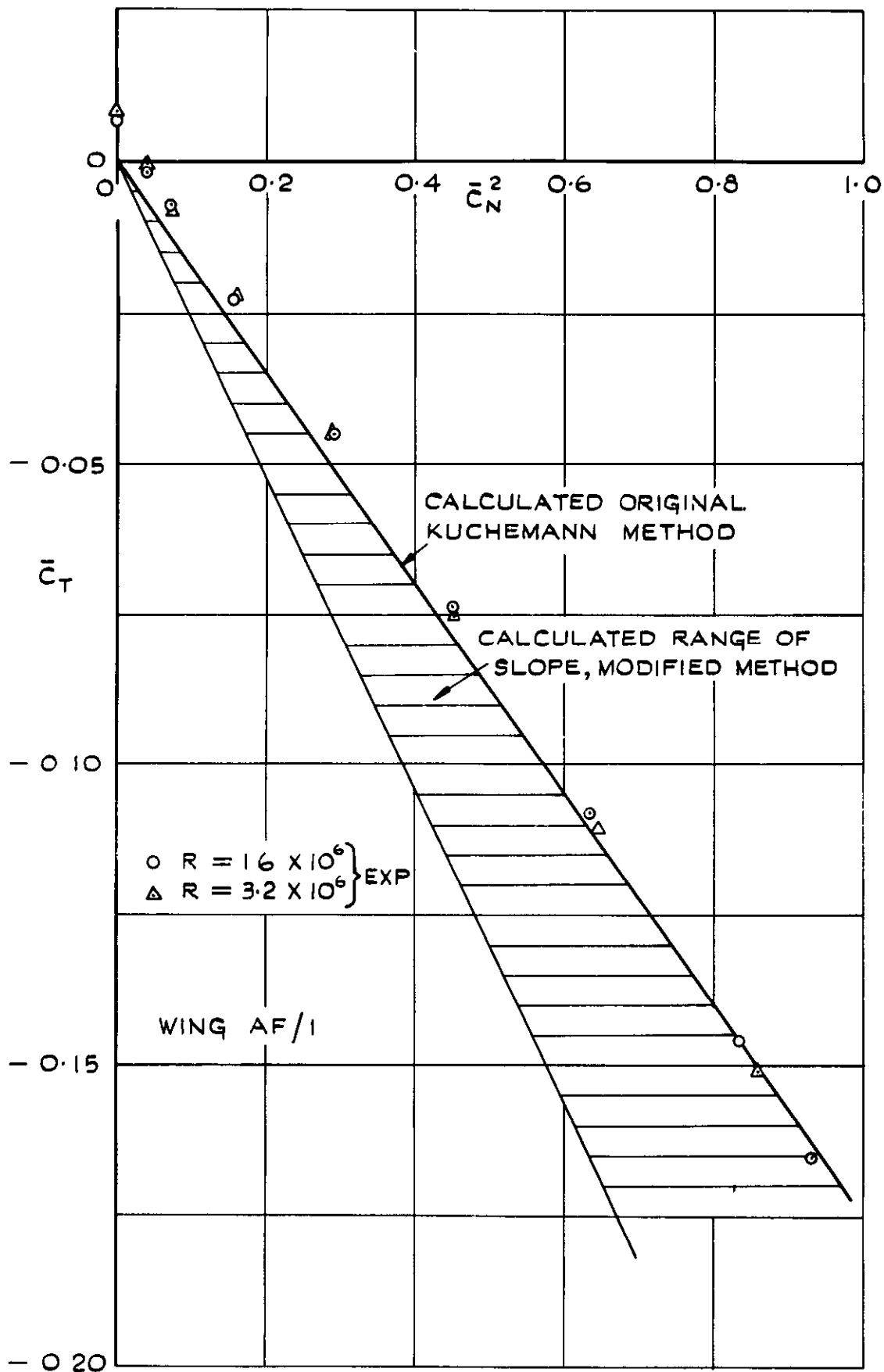


FIG. 12  $\bar{C}_N^2$  v  $\bar{C}_T$ , WING AF/1

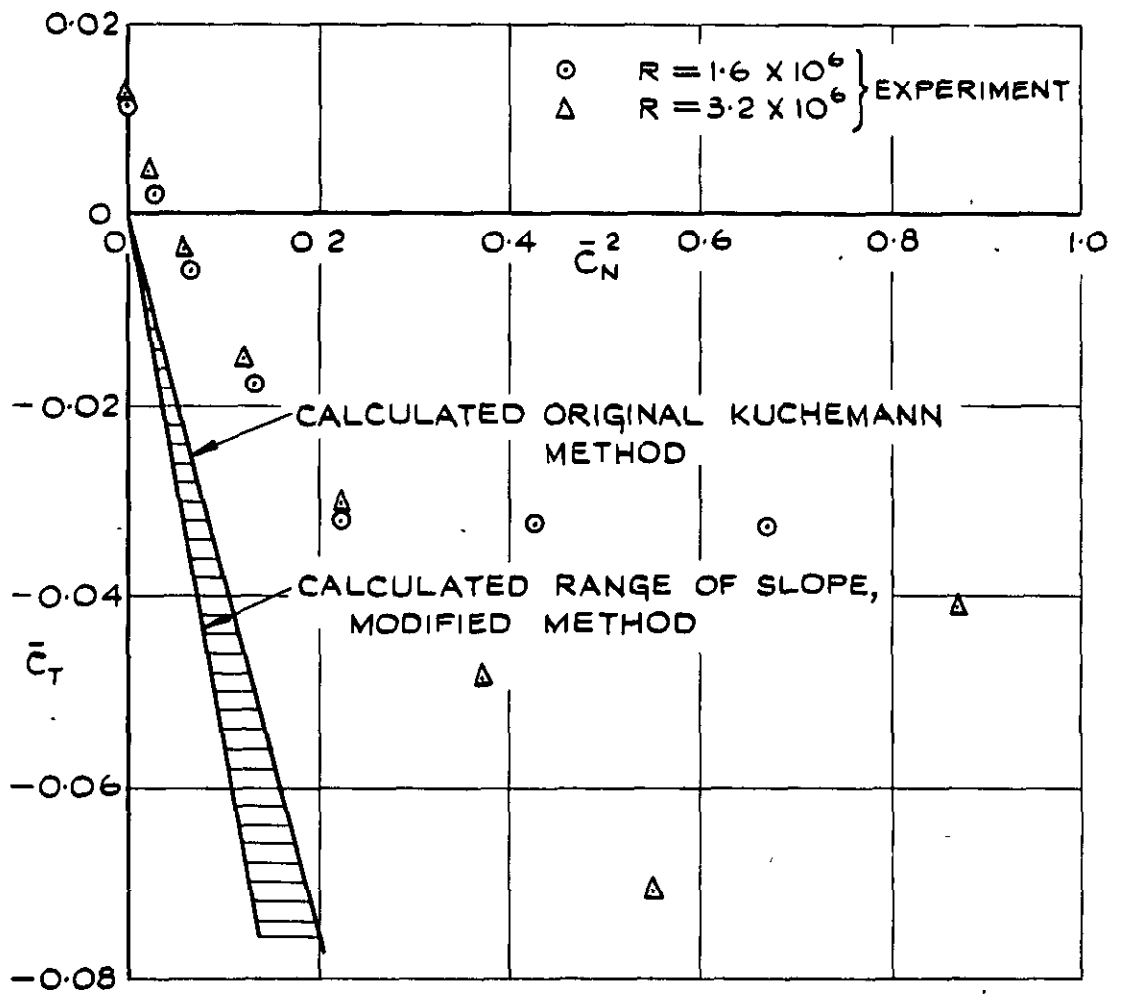


FIG. 13  $\bar{C}_N^2$  v  $\bar{C}_T$ , WING AF/5

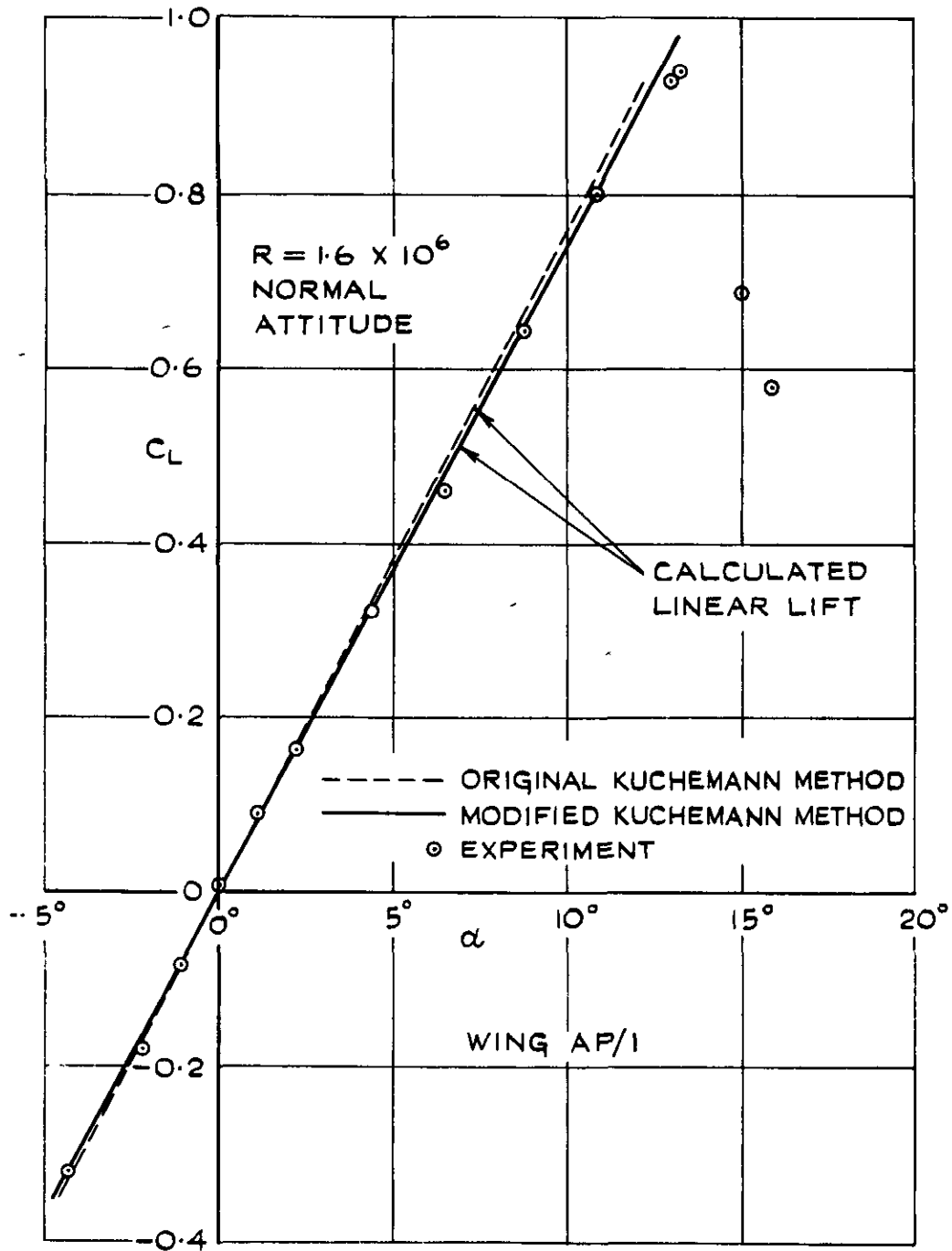


FIG.14 LOCAL LIFT AT CENTRE LINE v  
 INCIDENCE, WING AP/1

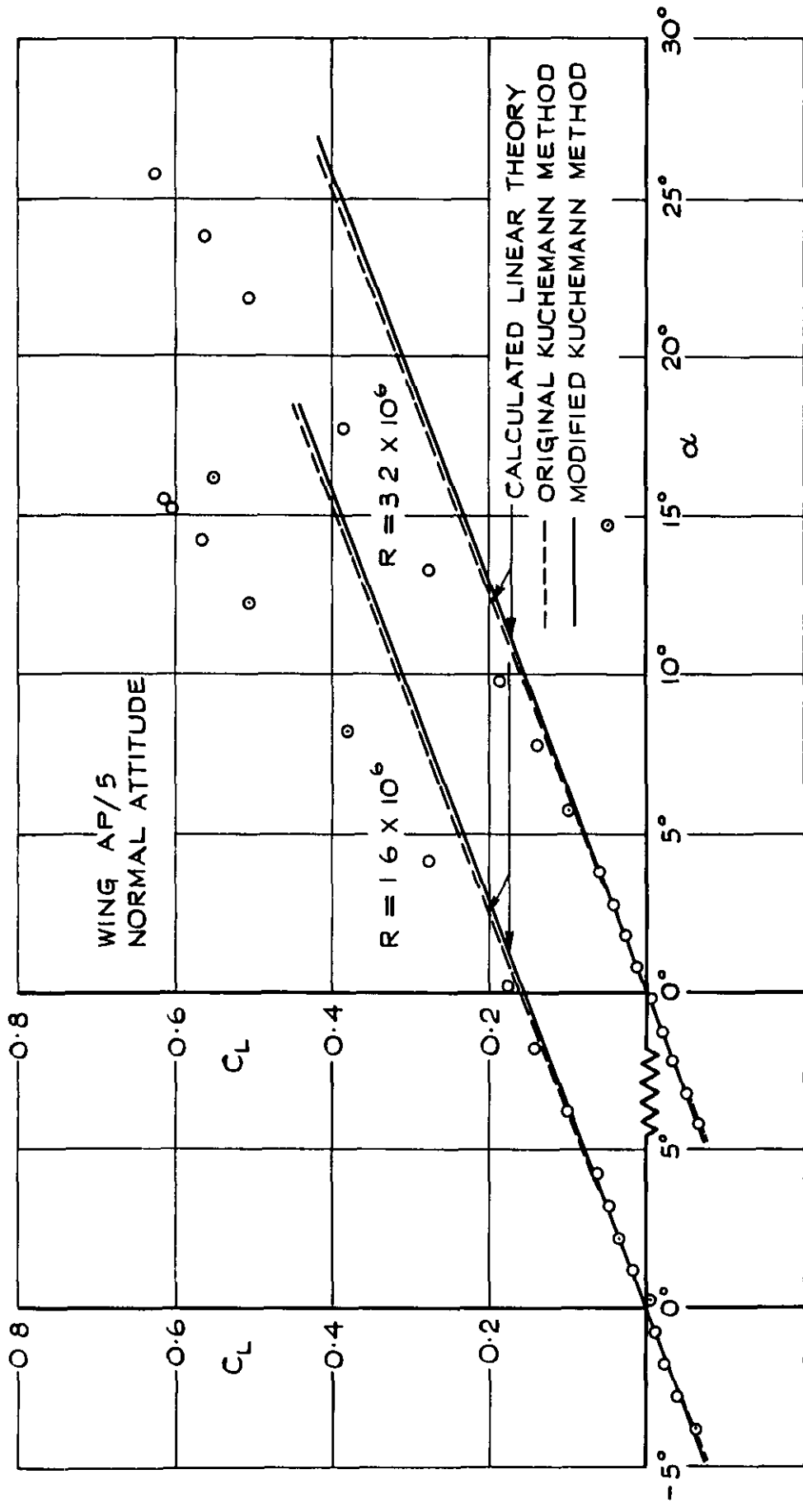


FIG. 15 LOCAL LIFT AT CENTRE SECTION v INCIDENCE, WING AP/5

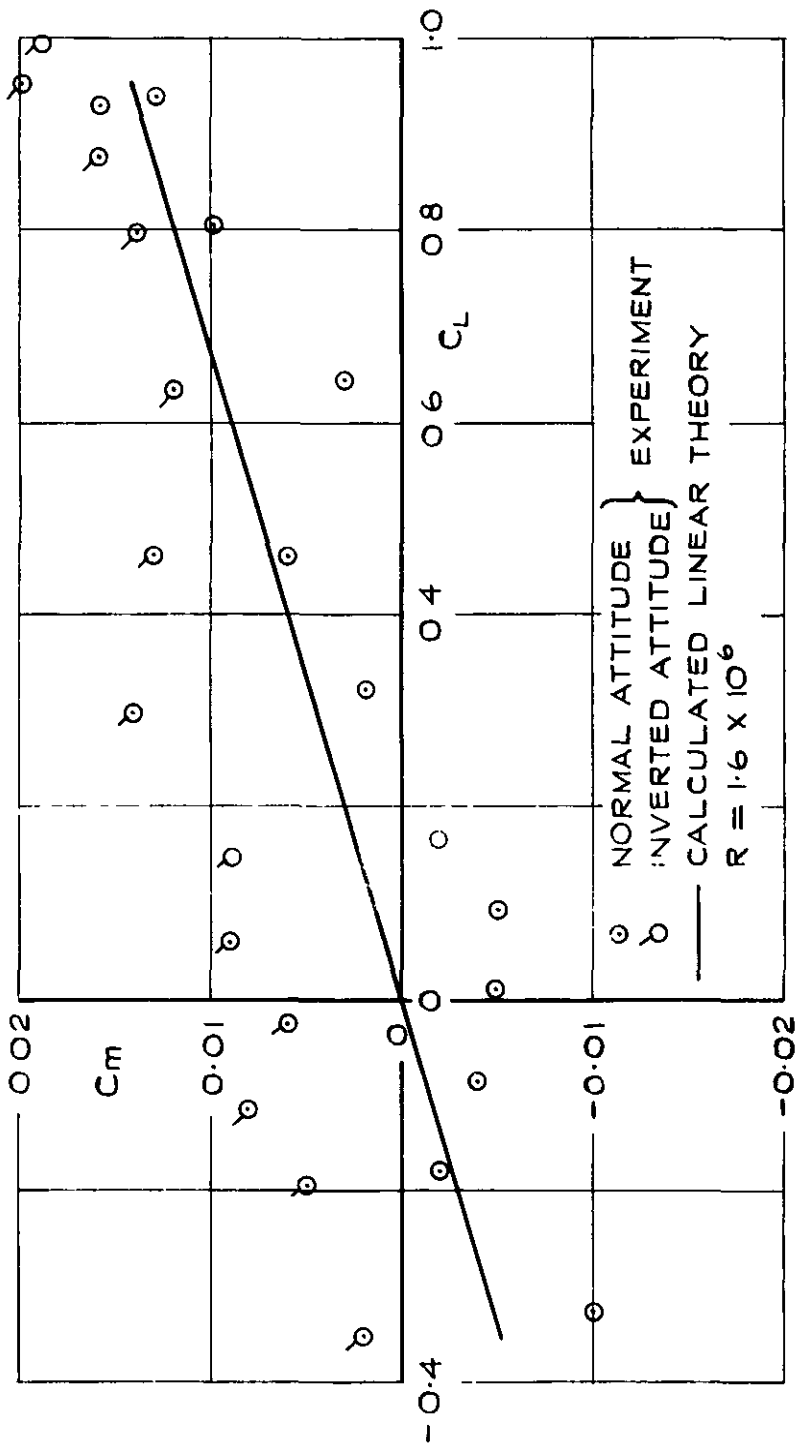


FIG. 16 LOCAL PITCHING MOMENT AT CENTRE SECTION, WING AP/I

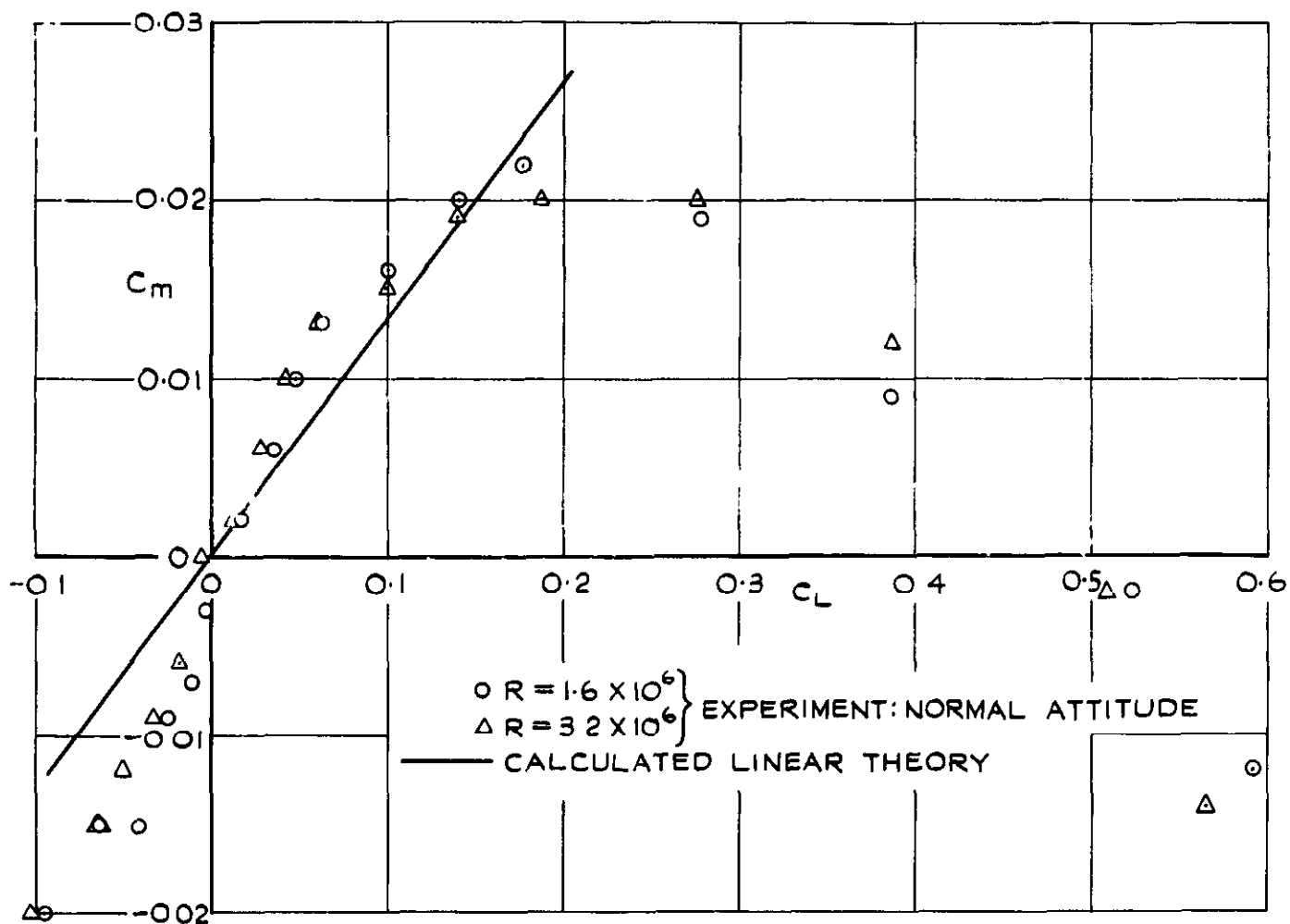


FIG. 17 LOCAL PITCHING MOMENT AT CENTRE SECTION, WING AP/5

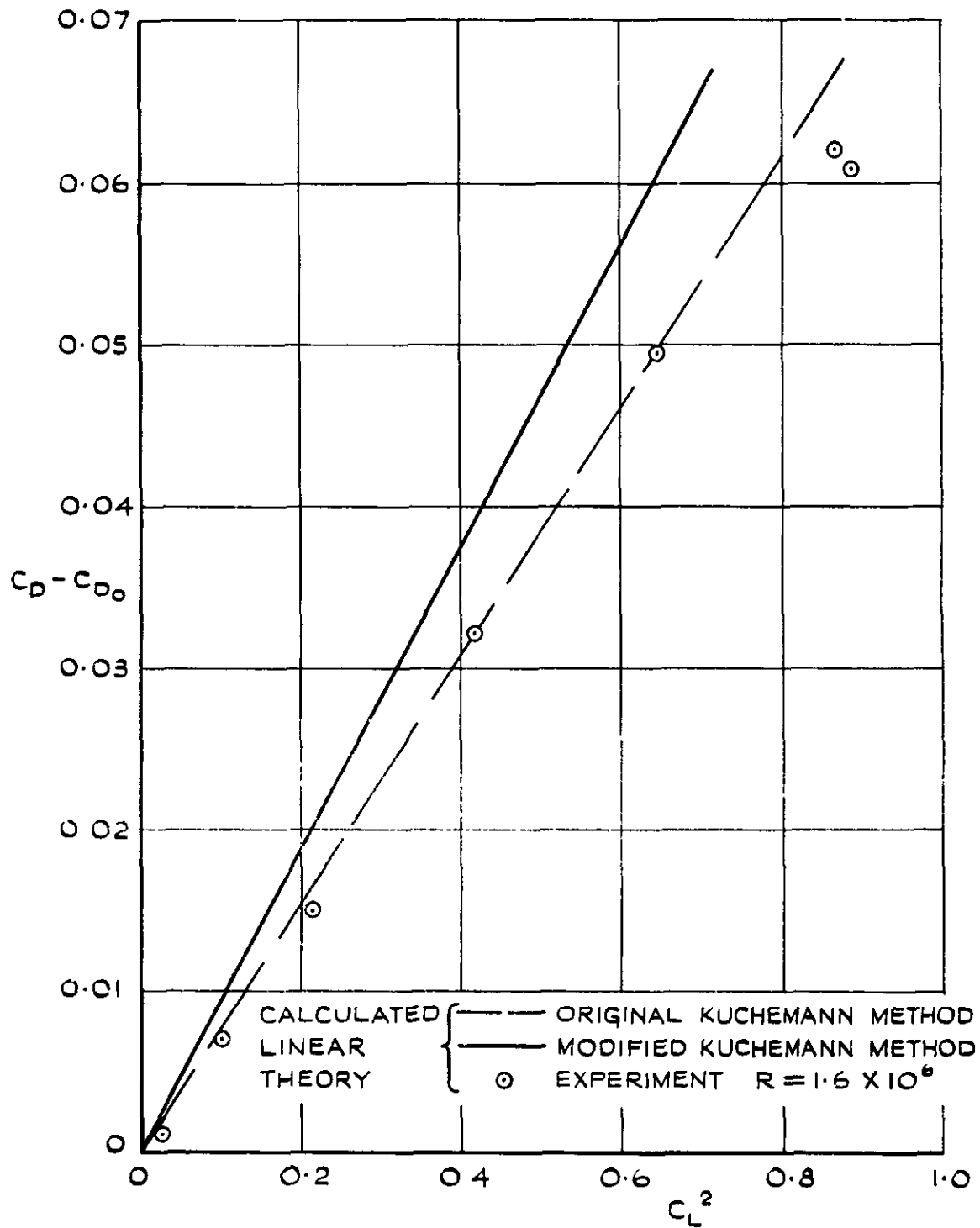


FIG.18 LOCAL DRAG DUE TO LIFT AND BOUNDARY LAYER, WING AP/1



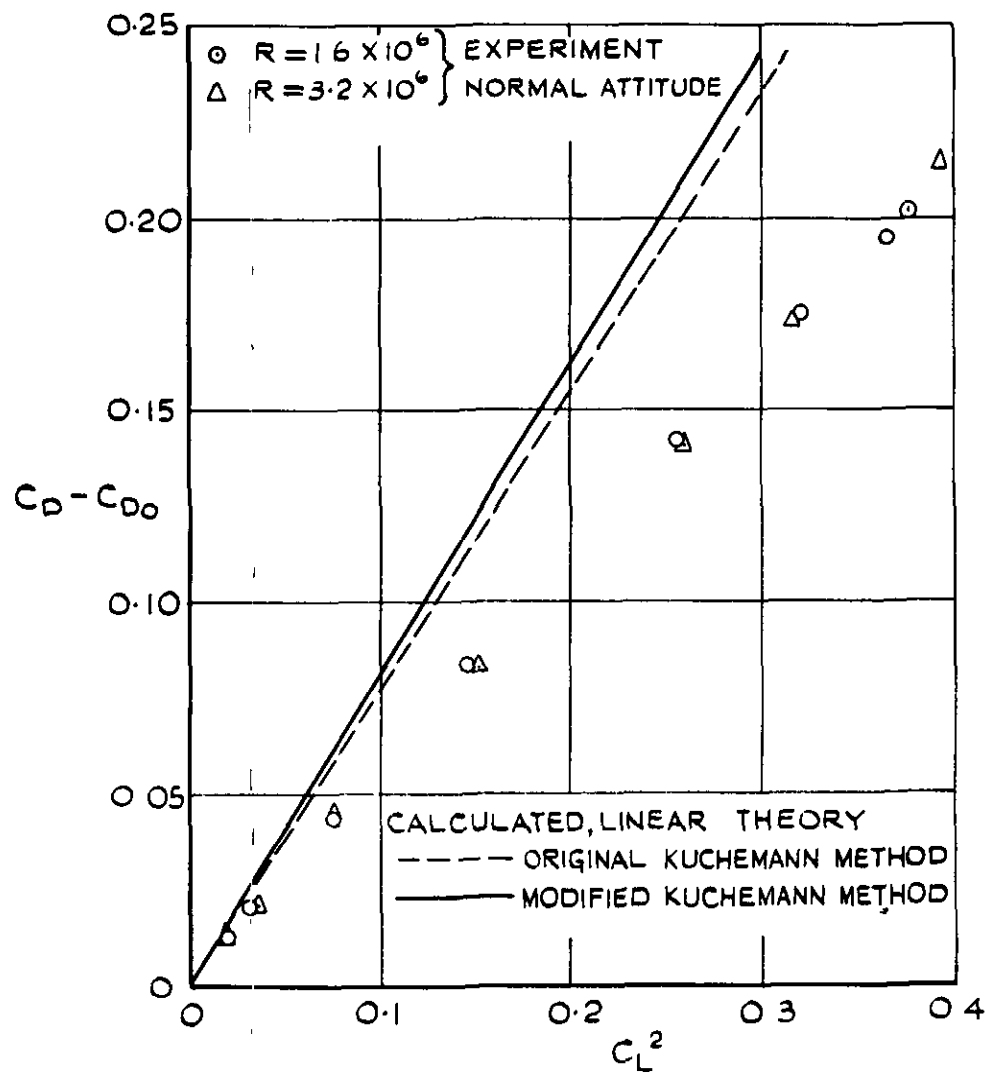


FIG. 19 LOCAL DRAG DUE TO LIFT AND BOUNDARY LAYER, WING AP/5

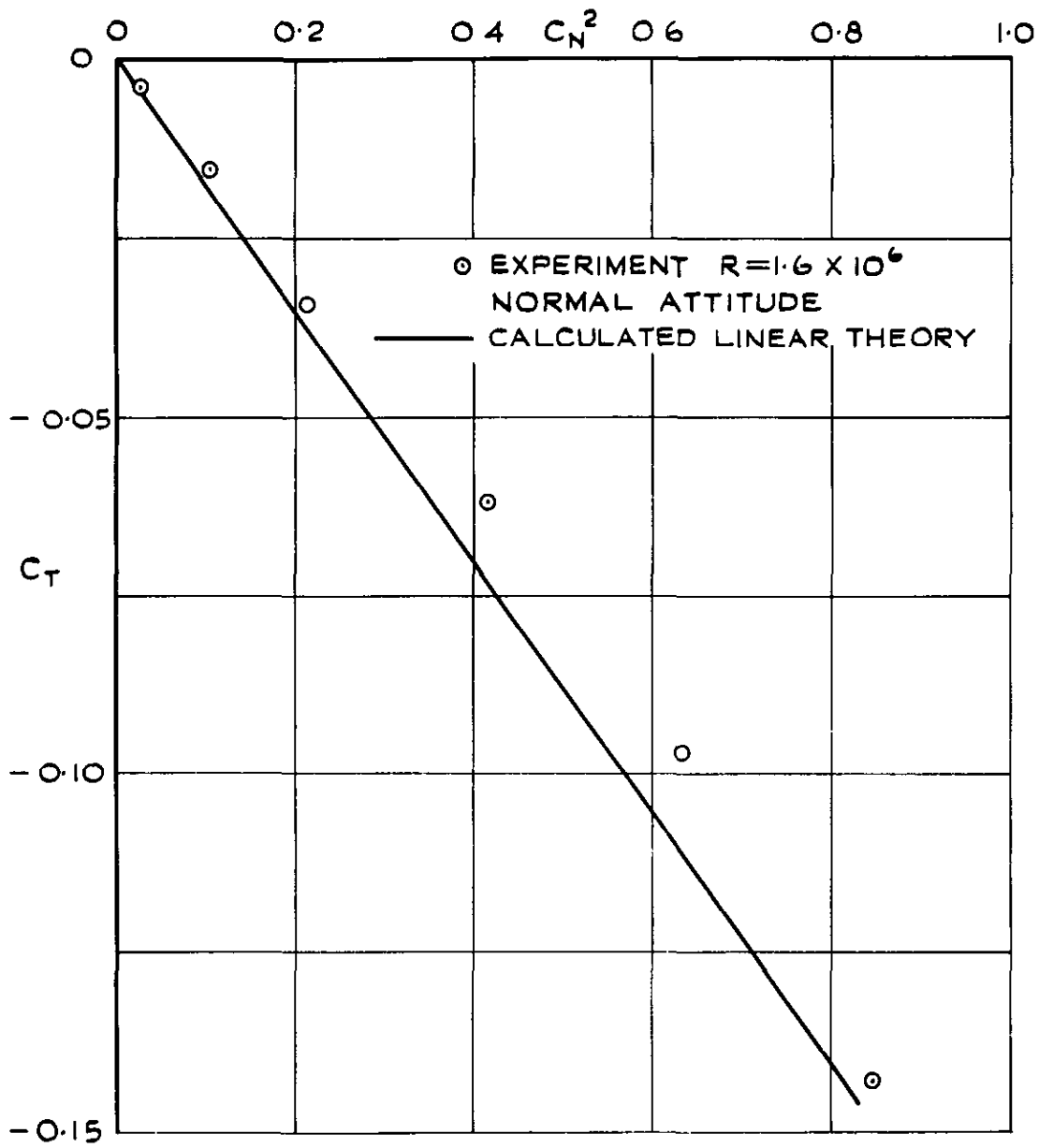


FIG. 20  $C_N^2$  v  $C_T$  AT CENTRE SECTION,  
 WING AP/1

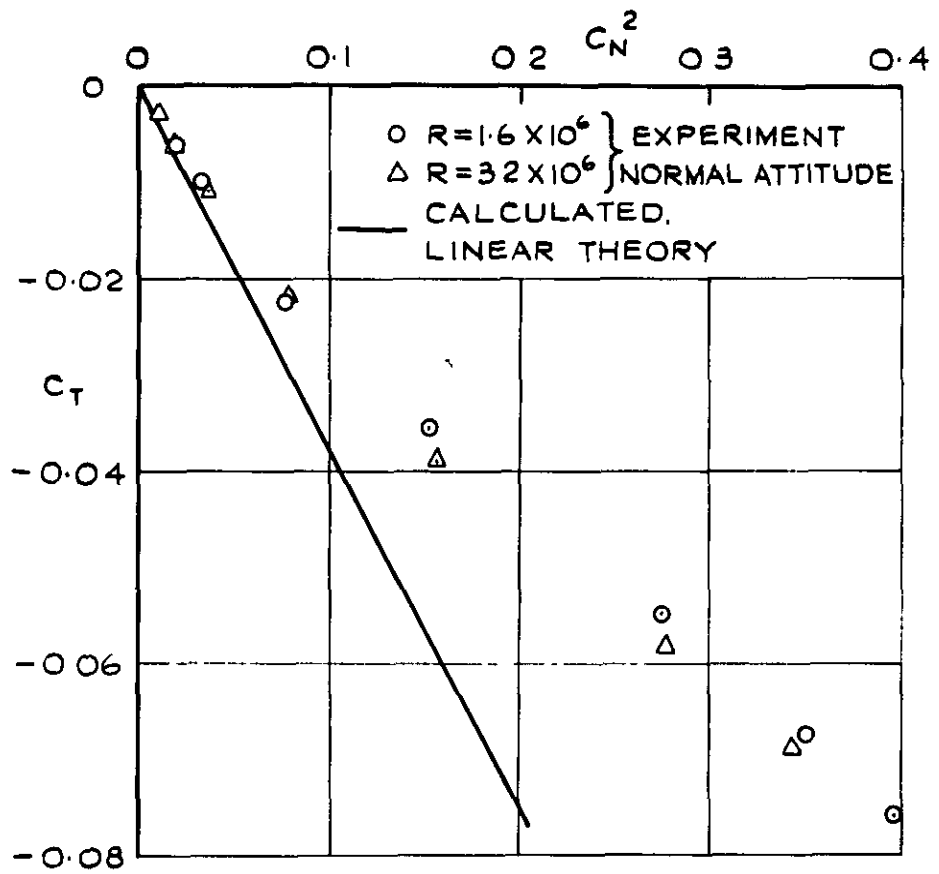


FIG. 21  $C_N^2$  v  $C_T$  AT CENTRE SECTION,  
 WING AP/5

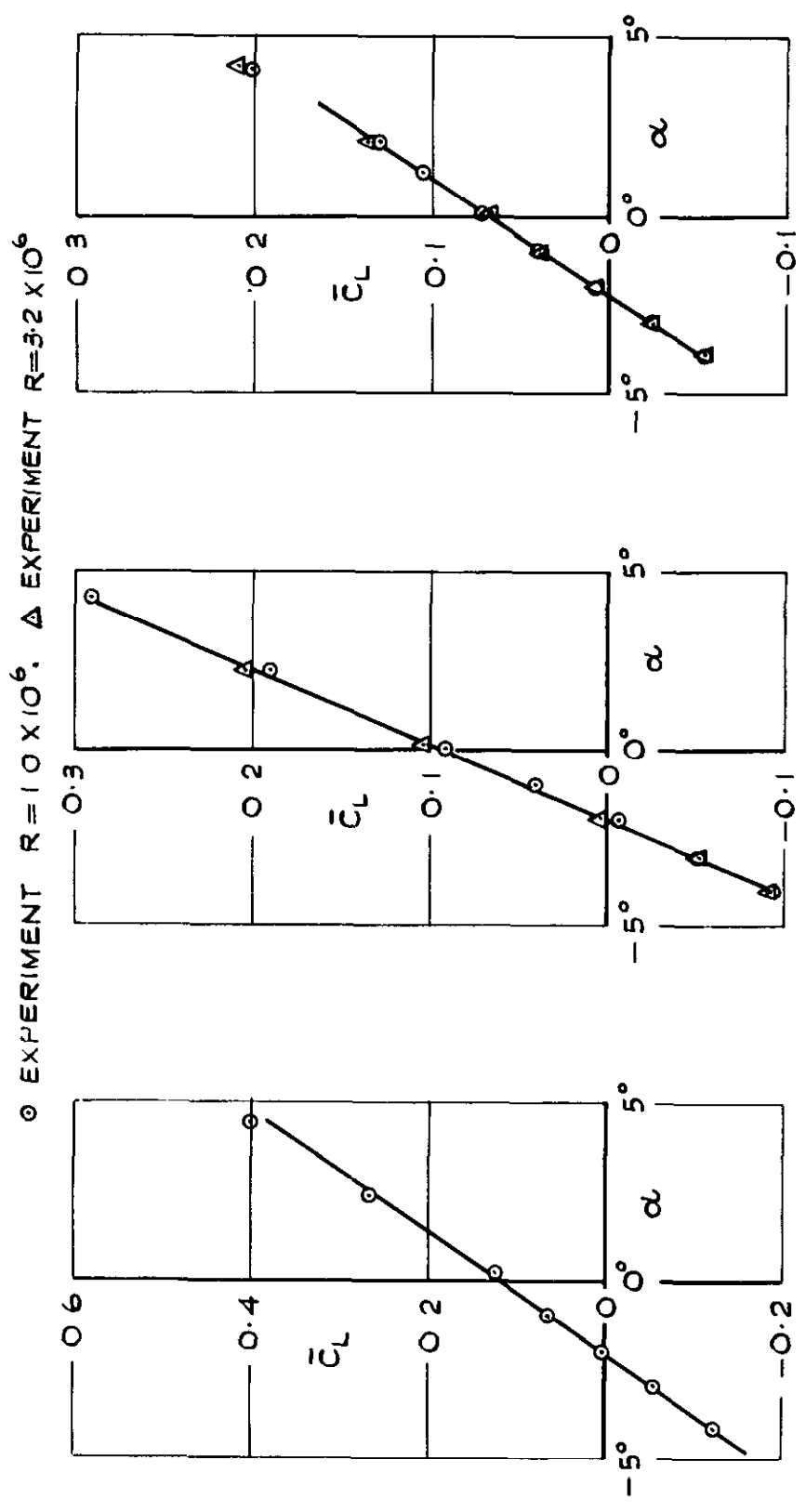
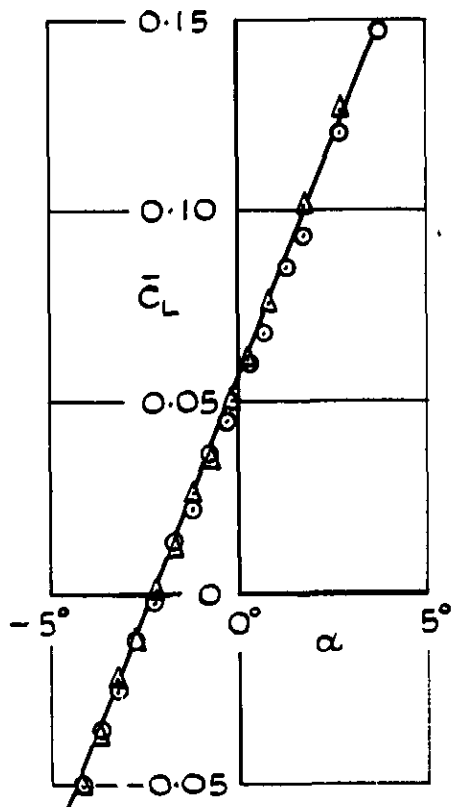


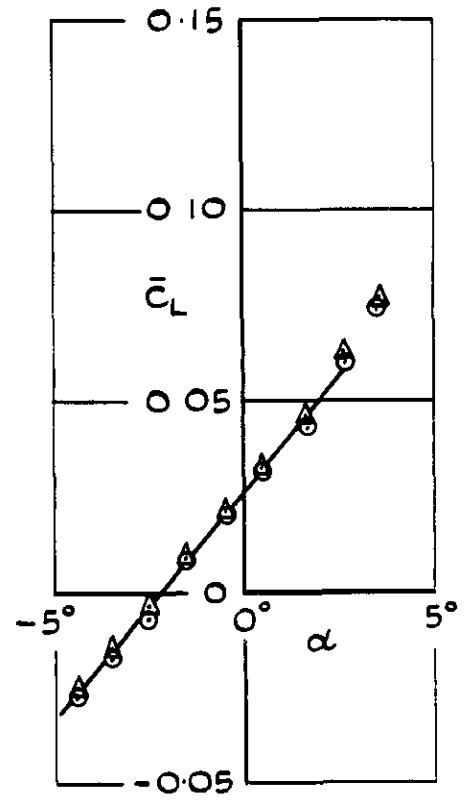
FIG. 22  $\bar{C}_L$  v  $\alpha$ , AND EXPERIMENTAL ZERO LIFT ANGLE; BF SERIES

○ EXPERIMENT,  $R = 1.6 \times 10^6$

△ EXPERIMENT,  $R = 3.2 \times 10^6$

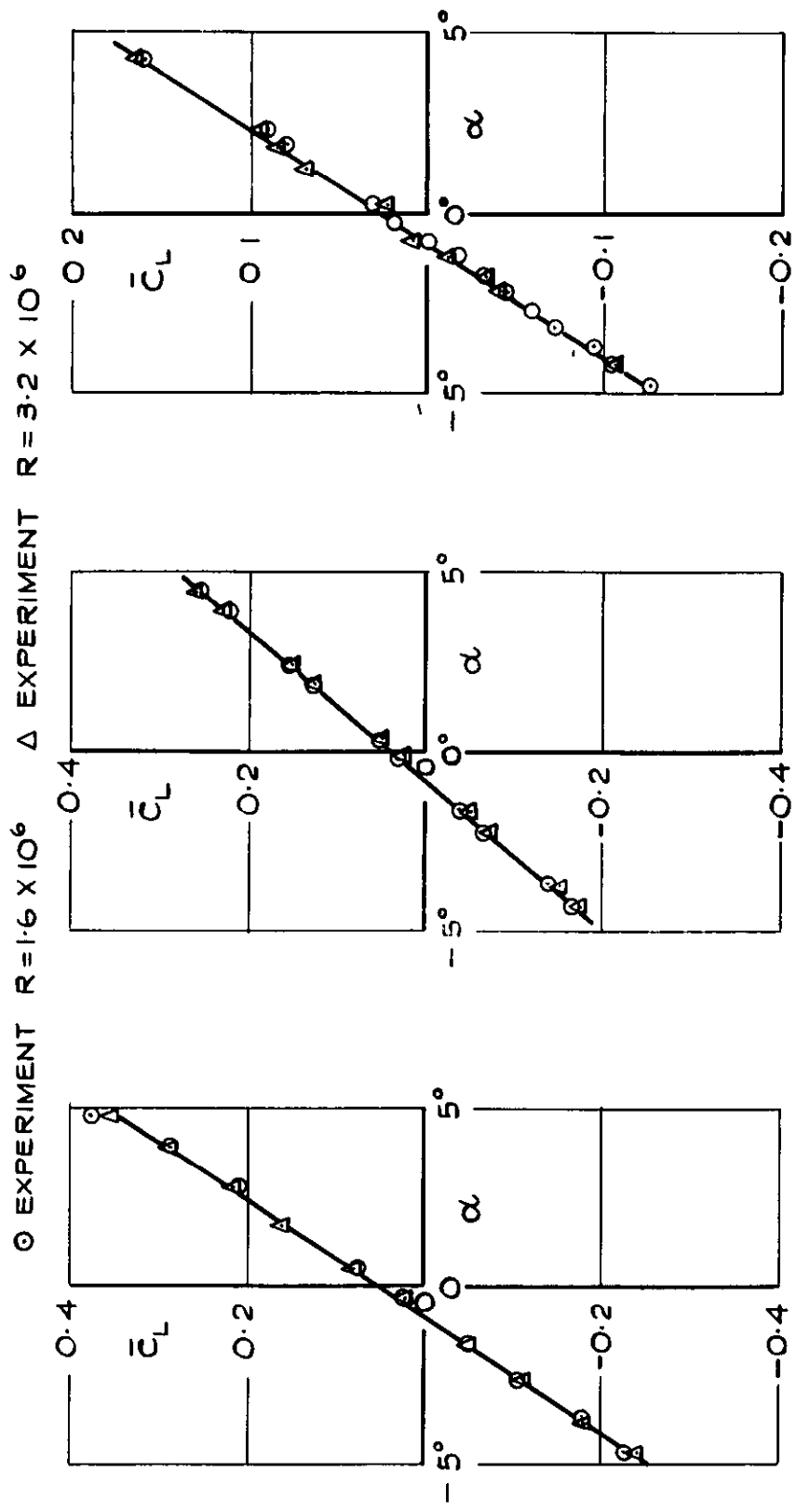


(d) WING BF/4



(e) WING BF/5

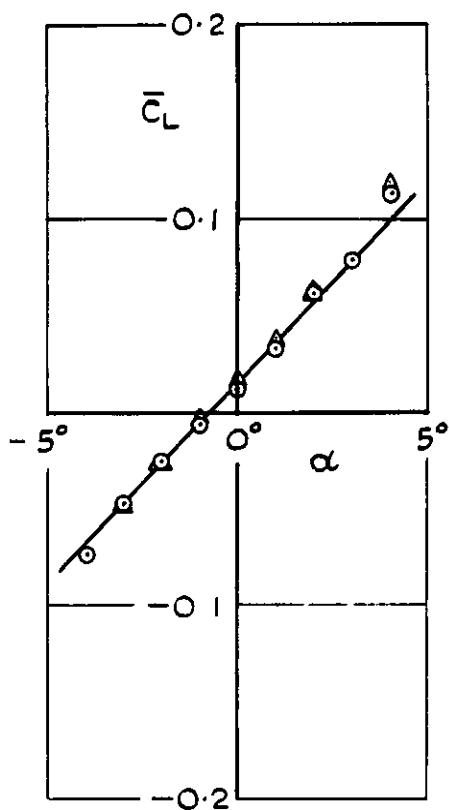
FIG. 22 (CONTD)



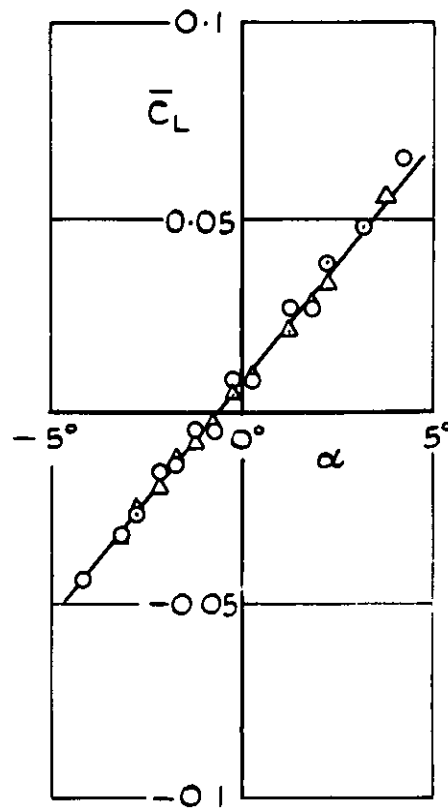
(a) WING CF/1 (b) WING CF/2 (c) WING CF/3

FIG. 23  $\bar{C}_L$  v  $\alpha$ , AND EXPERIMENTAL ZERO LIFT ANGLE; CF SERIES

⊙ EXPERIMENT  $R = 1.6 \times 10^6$      $\Delta$  EXPERIMENT  $R = 3.2 \times 10^6$



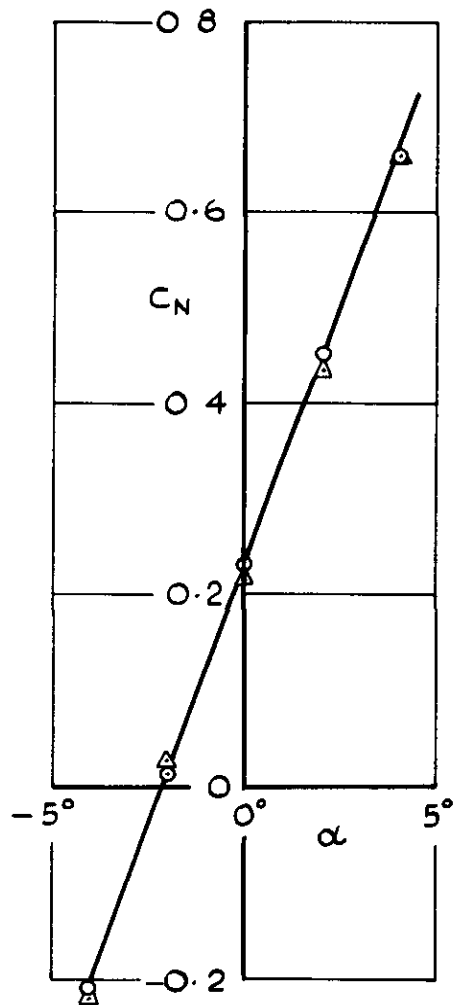
(d) WING CF/4



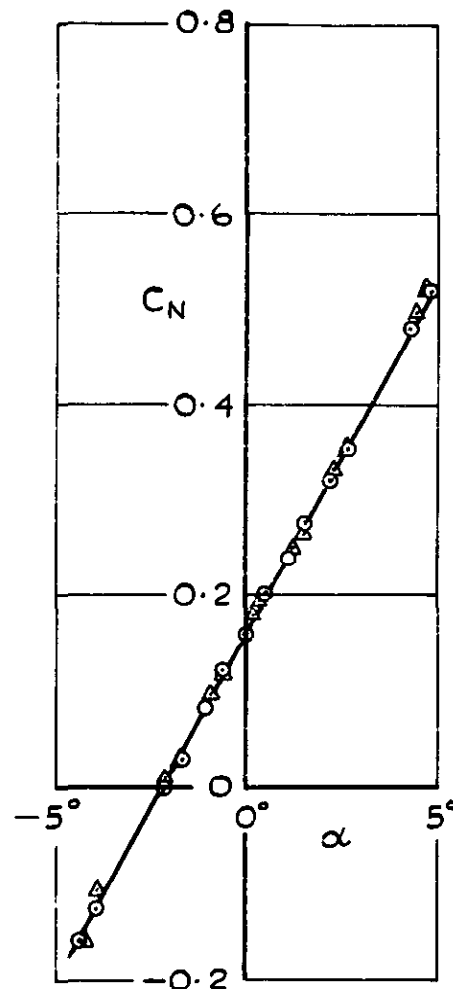
(e) WING CF/5

FIG. 23 (CONTD)

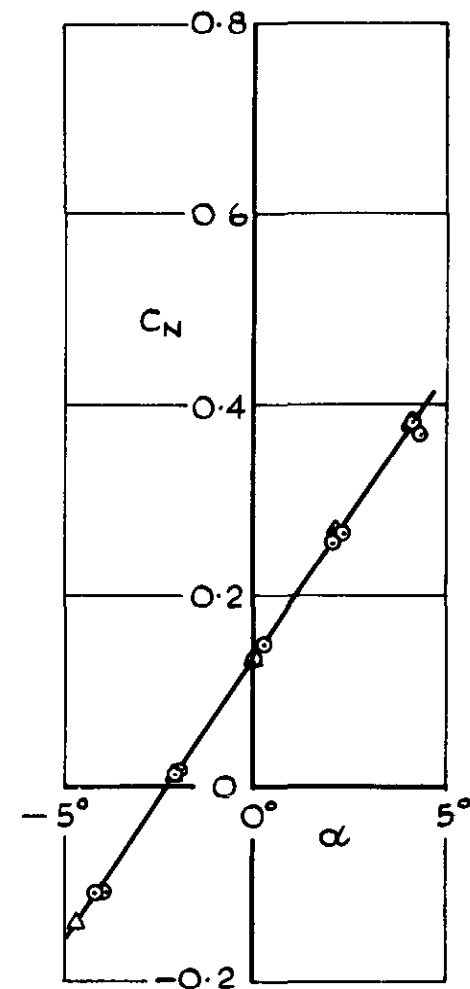
○ EXPERIMENT  $R = 1.6 \times 10^6$     Δ EXPERIMENT  $R = 3.2 \times 10^6$



(a) WING BP/0



(b) WING BP/1

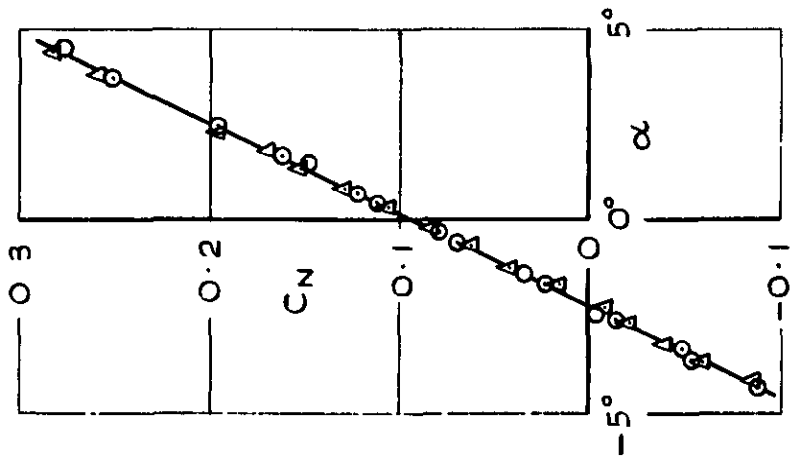


(c) WING BP/2

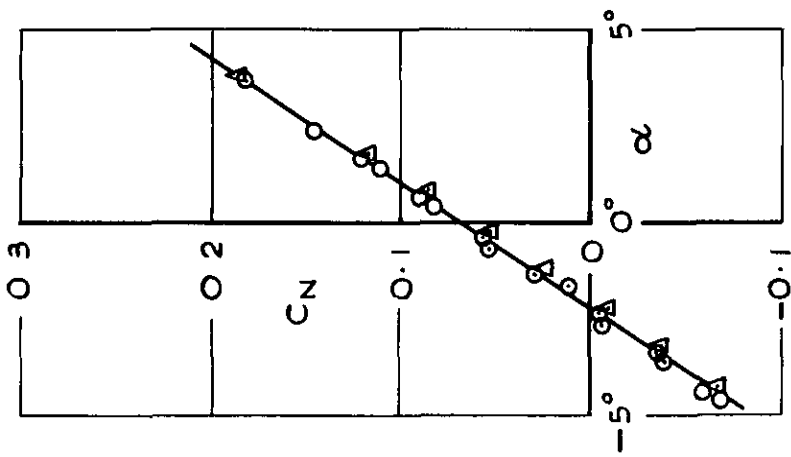
FIG. 24  $C_N$  v  $\alpha$ , AND EXPERIMENTAL ZERO LIFT ANGLE; BP SERIES



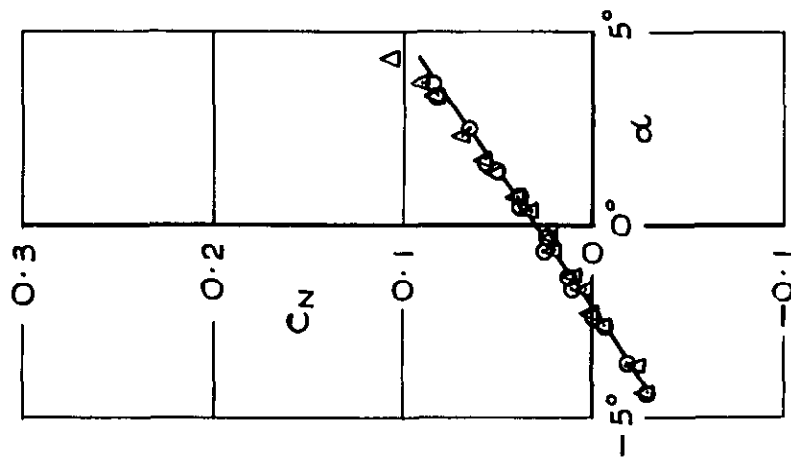
○ EXPERIMENT  $R = 1.0 \times 10^6$     △ EXPERIMENT  $R = 3.2 \times 10^6$



(d) WING BP/3



(e) WING BP/4



(f) WING BP/5

FIG. 24 (CONTD)

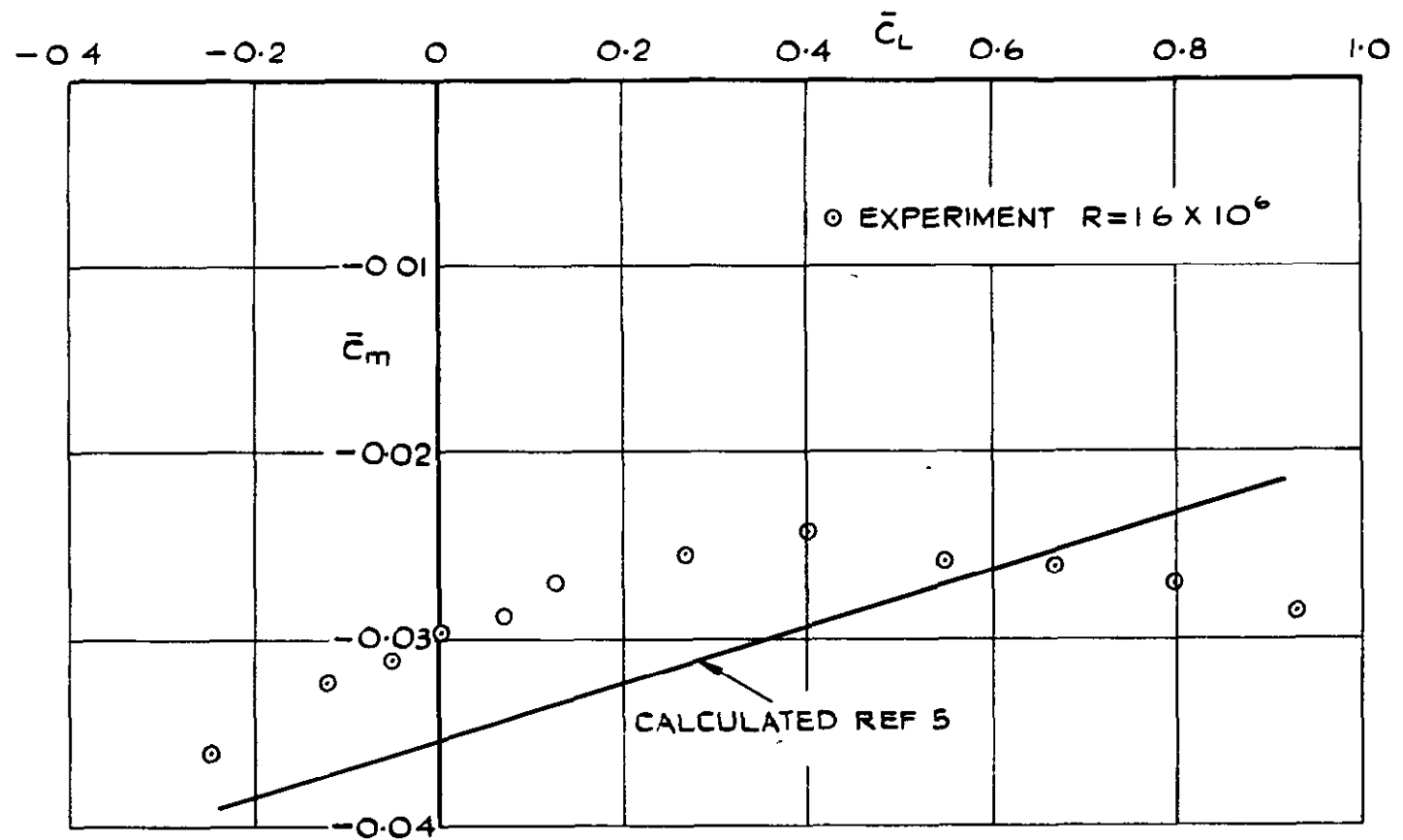


FIG. 25 PITCHING MOMENT v LIFT, WING BF/1

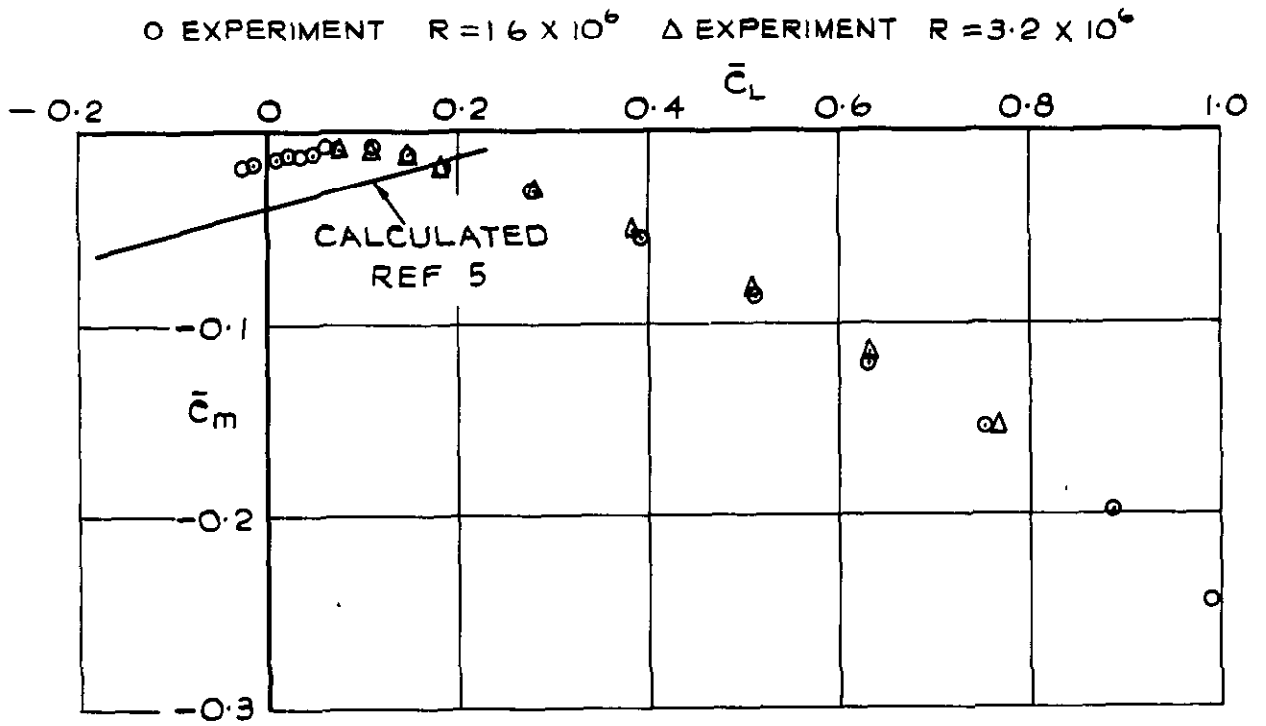


FIG. 26 PITCHING MOMENT v LIFT, WING BF/5

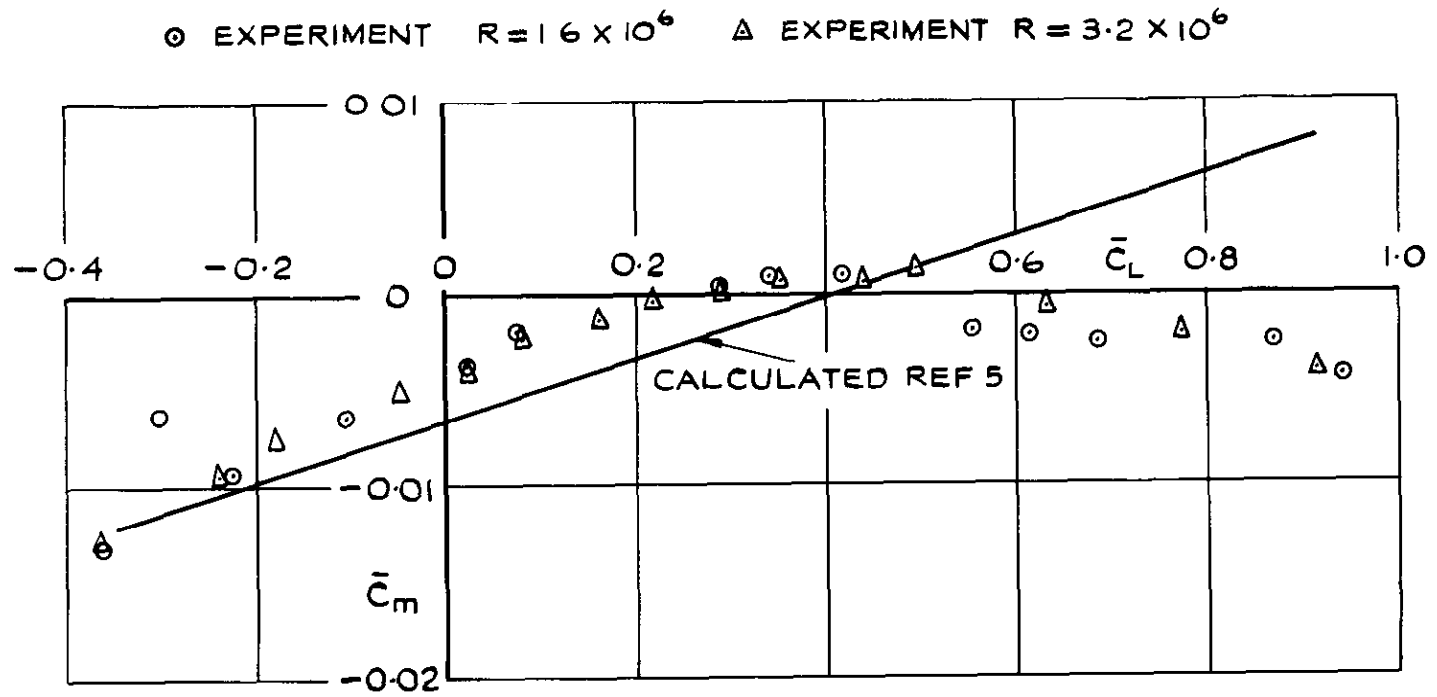


FIG. 27 PITCHING MOMENT v LIFT, WING CF/I

⊙ EXPERIMENT  $R=16 \times 10^6$      $\Delta$  EXPERIMENT  $R=32 \times 10^6$

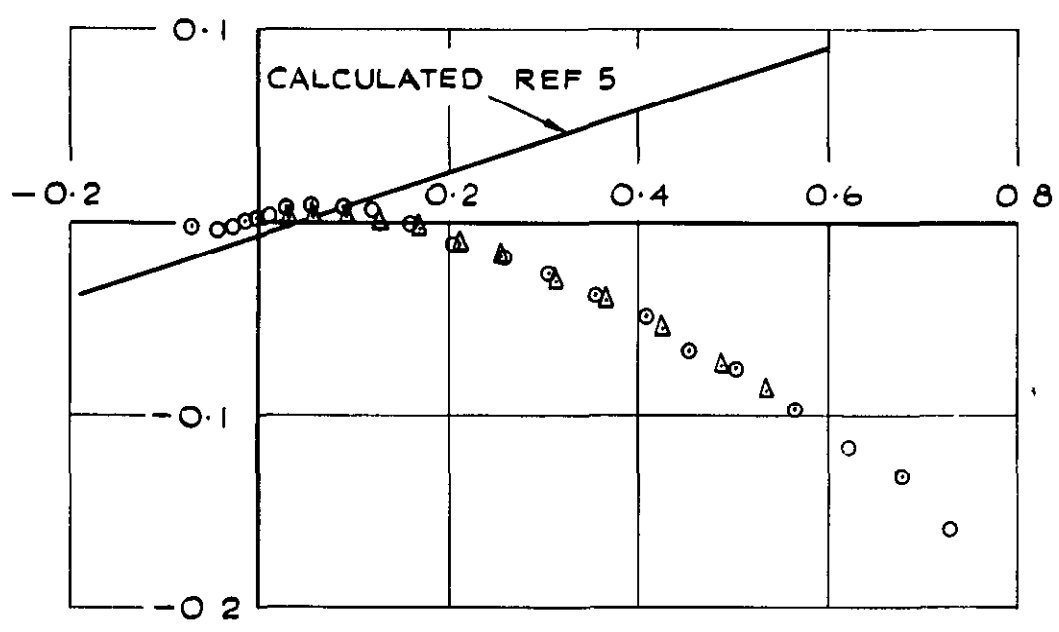


FIG.28 PITCHING MOMENT v LIFT, WING CF/5



A.R.C. C.P. No. 916  
October 1965

Brebner, G. G.  
Wyatt, L. A.  
Ilott, Gladys P.

533.693.6 :  
533.6.048.2 :  
533.6.048.1 :  
533.6.013.12/13 :  
533.6.013.152 :  
532.526.3

LOW SPEED WIND TUNNEL TESTS ON A SERIES OF RECTANGULAR  
WINGS OF VARYING ASPECT RATIO AND AEROFOIL SECTION

To provide experimental evidence on the loading and pressure distribution of low aspect ratio wings and on the variation of aerofoil section characteristics with aspect ratio, wind tunnel tests were done on a series of rectangular wings with aspect ratios varying from 4.0 to 0.5 and three different aerofoil sections. Two of the sections were cambered and all had the RAE 101 thickness distribution,  $t/c = 0.10$ . The tests comprised balance measurements of lift, drag and pitching moment, pressure measurements at the centre section (which have been integrated to obtain local forces and moments) and boundary layer transition observations.

(over)

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(over)

A limited analysis has been done of the local and total forces and moments, comparisons being made with the methods of Kúchemann and Weber for calculating load and pressure distribution. The experimental pressure distributions offer scope for considerably more analysis.

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